

NEW MEXICO OIL CONSERVATION COMMISSION  
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122  
Revised 9-1-65

Type Test <input checked="" type="checkbox"/> Initial <input type="checkbox"/> Annual <input type="checkbox"/> Special			Test Date 9-10-85								
Company Amoco Production Company			Connection								
Pool Bravo Dome Carbon Dioxide Gas Unit-640 acre area			Formation Tubb								
Completion Date 10/28/85		Total Depth 2775	Plug Back TD 2700	Elevation 4773	Unit BDCDGU						
Csq. Size 7	Wt. 20	d	Set At 2778	Perforations: From 2425 To 2515	Well No. 1833 031G						
Tbg. Size 3-1/2"	Wt. 9.3	d	Set At 2324	Perforations: From To	Unit Sec. Twp. Rge. G 3 18 33						
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single			Packer Set At 2293	County Harding							
Producing Thru Tubing		Reservoir Temp. °F 90 @ 2470	Mean Annual Temp. °F 50	Baro. Press. - P <sub>a</sub> 12.2	State New Mexico						
L 2470	H 2470	G <sub>g</sub> 1.529	% CO <sub>2</sub> 100	% N <sub>2</sub> 0	% H <sub>2</sub> S 0						
FLOW DATA			TUBING DATA		CASING DATA						
Prover	Meter Run 4.0	Taps Flange									
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h <sub>w</sub>	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration of Flow
SI							350				
1.	4.026 x 1.75			195	25	64	195	50			24 hrs.
2.	4.026 x 1.75			211	27	64	211	50			24 hrs.
3.	4.026 x 1.75			231	19	63	231	50			24 hrs.
4.	4.026 x 1.75			246	14	63	246	50			24 hrs.
5.											
RATE OF FLOW CALCULATIONS											
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P <sub>m</sub>	Flow Temp. Factor Ft.	Gravity Factor F <sub>g</sub>	Super Compress. Factor, F <sub>pv</sub>	Rate of Flow Q, Mcfd				
1							879				
2							818				
3							729				
4							703				
5											
NO.	P <sub>r</sub>	Temp. °R	T <sub>r</sub>	Z	Gas Liquid Hydrocarbon Ratio <u>0</u> Mcf/bbl.						
1					A.P.I. Gravity of Liquid Hydrocarbons <u>0</u> Deg.						
2					Specific Gravity Separator Gas <u>1.529</u> X X X X X X X X						
3					Specific Gravity Flowing Fluid <u>X X X X X</u>						
4					Critical Pressure <u>1072</u> P.S.I.A. P.S.I.A.						
5					Critical Temperature <u>547</u> R R						
P <sub>r</sub> <u>362.2</u> P <sub>w</sub> <u>131.189</u>											
NO.	P <sub>r</sub> <sup>2</sup>	P <sub>w</sub>	P <sub>w</sub> <sup>2</sup>	P <sub>r</sub> <sup>2</sup> - P <sub>w</sub> <sup>2</sup>	(1) $\frac{P_r^2}{P_r^2 - P_w^2} = 1.49$ (2) $\left[ \frac{P_r^2}{P_r^2 - P_w^2} \right]^n = 1.33$						
1		207.2		88.257	AOF = Q $\left[ \frac{P_r^2}{P_r^2 - P_w^2} \right]^n = 1165$						
2		223.2		81.370							
3		243.2		72.043							
4		258.2		64.522							
5											
Absolute Open Flow <u>1165</u> Mcfd @ 15.025					Angle of Slope $\theta$ _____			Slope, n <u>.71</u>			
Remarks: _____											
Approved By Commission:			Conducted By:			Calculated By: D. D. KIMBLE			Checked By:		