

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special		Test Date 7-10-87	
Company Amoco Production Company		Connection	
Pool Bravo Dome		Formation Tubb	
Completion Date 4-14-74		Total Depth 2558	Plug Back TD 2509
		Elevation 4741	Farm or Lease Name
Csg. Size 4.50	Wt. 9.5	d 4.1	Set At 2558
Perforations: From 2245	To 2357		Well No. 2034-111H
Perforations: From	To		Unit H
Sec. 11	Twp. 20	Rge. 34	
Type Well - Single - Brdenhead - G.C. or G.O. Multiple Single		Packer Set At 2178	County Union
Producing Thru Tubing	Reservoir Temp. °F 90	Mean Annual Temp. °F 50	Baro. Press. - P _g 12.25
State New Mexico			
L	H	Cg	% CO ₂ 100
			% N ₂ 0
			% H ₂ S. 0
Prover		Meter Run 4.0	Taps Flange

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
1.	4.026	x	1.50	200	33	61	190	61	0		24 hrs
2.	4.026	x	1.50	211	25	61	134	61	0		24 hrs
3.	4.026	x	1.50	226	17	62	213	62	0		24 hrs
4.	4.026	x	1.50	242	10	62	161	62	0		24 hrs
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor FL	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1.							796
2.							670
3.							599
4.							486
5.							

NO.	P _f	Temp. °R	T _f	Z	Gas Liquid Hydrocarbon Ratio	Mcf/bbl.
1.					0	
2.						
3.						
4.						
5.						

A.P.L. Gravity of Liquid Hydrocarbons _____ Deg. Specific Gravity Separator Gas 1.529 Specific Gravity Flowing Fluid XXXXX Critical Pressure 1072 P.S.I.A. Critical Temperature 496 R			
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P _c 293.25 P _c ² 85,995 (1) $\frac{P_c^2}{P_c^2 - P_w^2} = 2.1003$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.7548$ AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1397$	<table border="1" style="width:100%; border-collapse: collapse;"> <tr> <th>NO.</th> <th>P_w</th> <th>P_w²</th> <th>P_c² - P_w²</th> </tr> <tr> <td>1</td> <td>212.25</td> <td>45,050</td> <td>40,945</td> </tr> <tr> <td>2</td> <td>223.25</td> <td>49,840</td> <td>36,155</td> </tr> <tr> <td>3</td> <td>238.25</td> <td>56,763</td> <td>29,232</td> </tr> <tr> <td>4</td> <td>254.25</td> <td>64,643</td> <td>21,352</td> </tr> <tr> <td>5</td> <td></td> <td></td> <td></td> </tr> </table>	NO.	P _w	P _w ²	P _c ² - P _w ²	1	212.25	45,050	40,945	2	223.25	49,840	36,155	3	238.25	56,763	29,232	4	254.25	64,643	21,352	5			
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Absolute Open Flow 1397 Mcfd @ 15.025	Angle of Slope @ 37.1548	Slope, n 0.7578
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Remarks: Test was run from a low flowing tubing pressure to a high flowing tubing pressure to minimize liquid loading effects.

Approved by Commission:	Conducted By: RANDY MAHANNAH	Calculated By: RICHARD ROETH	Checked By:
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BDCD GU No. 2034 111H

