NEW MEXICO OIL CONSERVATION COMMSSION

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test: [X] Initial [ ] Annual [ ] Special				Test Date: 6-20-87	
Company: Amoco Production Company			Connection		
Pool: Bravo Dome			Formation: Tubb		Unit: BDCDGU
Completion Date: 12-30-80	Total Depth: 2530'		Plug Back TD: 2390'	Elevation: 4720'	Farm or Lease Name
Csg. Size: 5.50 / Wt.: 14# / d: 4.90 / Set At: 2530'			Perforations: From 2142' To 2354'		Well No.: 1934-111G
Tbg. Size: 2.875 / Wt.: 6.5 / d: 2.441 / Set At: 2125			Perforations: From To		Unit: G / Sec.: 11 / Twp.: 19 / Rge.: 34
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: Single			Packer Set At: 2096'		County: Union
Producing Thru: Tubing	Reservoir Temp. °F: 90	Mean Annual Temp. °F: 50	Baro. Press. – P_a: 12.25		State: New Mexico
L	H	Gg	% CO_2: 100	% N_2: 0	% H_2S: 0
Prover			Meter Run: 4.0	Taps: Flange	

FLOW DATA

NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	TUBING DATA Press. p.s.i.g.	TUBING DATA Temp. °F	CASING DATA Press. p.s.i.g.	CASING DATA Temp. °F	Duration of Flow
SI							290				
1.	4.026	X	2.50	195	24	59	196	59	0		24 hrs
2.	4.026	X	2.50	201	22	59	202	59	0		24 hrs
3.	4.026	X	2.50	212	17	60	212	60	0		24 hrs
4.	4.026	X	2.50	225	12	60	225	60	0		24 hrs
5.											

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1							
2.							2050
3.							1905
4.							1726
5.							1542

NO.	P_t	Temp. °R	T_r	Z
1.				
2.				
3.				
4.				
5.				

Gas Liquid Hydrocarbon Ratio 0 Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons ____ Deg.
Specific Gravity Separator Gas 1.529 XXXXXXXXX
Specific Gravity Flowing Fluid XXXXX
Critical Pressure 1072 P.S.I.A. ____ P.S.I.A.
Critical Temperature 496 R ____ R

F_c 302.25 P_c^2 91.355

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1		208.25	43.368	47.987
2		214.25	45.903	45.452
3		224.25	50.288	41.067
4		237.25	56.287	35.067
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.9037$

(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1.9037$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 3902$

Absolute Open Flow 3902 Mcfd @ 15.025 | Angle of Slope θ 45 | Slope, n 1.0

Remarks: Test was run from a low flowing tubing pressure to a high flowing tubing pressure to minimize liquid loading effects.

Approved by Commission:	Conducted By:	Calculated By:	Checked By:
	RANDY MAHANNAH	RICHARD ROETH	