

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
 Revised 9-1-65

Type Test: ☒ Initial ☐ Annual ☐ Special		Test Date: 6-20-87	
Company: Amoco Production Company		Connection:	
Pool: Bravo Dome		Formation: Tubb	
Completion Date: 12-30-80		Total Depth: 2558'	Plug Back TD: 2490'
		Elevation: 4780'	Farm or Lease Name:
Csg. Size: 5.50	Wt. 14#	d 4.9	Set At 2558
Tub. Size: 2.875	Wt. 6.5#	d 2.441	Set At 2131'
Type Well - Single - Bradenhead - G.G. or G.O. Multiple		Packer Set At 2125'	Well No. 1934-101J
Producing Thru Tubing		Reservoir Temp. °F 90	Mean Annual Temp. °F 50
		Baro. Press. - P _a 12.25	Unit Sec. Twp. Rge. J 10 19 34
L H Gg		% CO ₂ 100	% N ₂ 0
		% H ₂ S. 0	Prover
		Meter Run 4.0	Taps Flange

FLOW DATA					TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	
1.	4.026 x 2.50			192	26	58	192	58	24 hrs
2.	4.026 x 2.50			200	22	59	201	59	24 hrs
3.	4.026 x 2.50			211	17	60	211	60	24 hrs
4.	4.026 x 2.50			224	14	60	224	60	24 hrs
5.									24 hrs

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1.							
2.							2041
3.							1895
4.							1750
5.							1610

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio 0	Mcf/bbl.
1.					A.P.I. Gravity of Liquid Hydrocarbons	
2.					Specific Gravity Separator Gas 1.529	Deg.
3.					Specific Gravity Flowing Fluid X X X X X	X X X X X X X X X
4.					Critical Pressure 1072	P.S.I.A.
5.					Critical Temperature 496	P.S.I.A.

F _c 318.25 P _c ² 101.283						
NO.	F _c ²	P _w	P _w ²	P _c ² - P _w ²	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.7004$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.6997$
1.		204.25	41,718	59,565		
2.		213.25	45,475	55,807		
3.		223.25	49,840	51,442		
4.		236.25	55,841	45,496		
5.						

Absolute Open Flow 3469 Mcfd @ 15.025			Angle of Slope @ 44.9771	Slope, n 0.9992
Remarks: Test was run from a low flowing tubing pressure to a high flowing tubing pressure to minimize liquid loading effects.				
Approved By Commission:		Conducted By: RANDY MAHANNAH	Calculated By: RICHARD ROETH	Checked By: