NEW MEXICO OIL CONSERVATION COMMISSION

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test: [X] Initial [ ] Annual [ ] Special				Test Date: 7-4-87	
Company: Amoco Production Company		Connection:			
Pool: Bravo Dome		Formation: Tubb			Unit: BDCDGU
Completion Date: 1-11-81	Total Depth: 2450	Plug Back TD: 2364	Elevation: 4690		Farm or Lease Name:
Csg. Size: 5.50 / Wt.: 14 / d: 4.90	Set At: 2450	Perforations: From 2120 To 2330			Well No.: 1935-061G
Tbg. Size: 2.875 / Wt.: 6.5 / d: 2.441	Set At: 2112	Perforations: From To			Unit: G / Sec.: 6 / Twp.: 19 / Rge.: 35
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: Single		Packer Set At: 2074			County: Union
Producing Thru: Tubing	Reservoir Temp. °F: 90	Mean Annual Temp. °F: 50	Baro. Press. – P_a: 12.25		State: New Mexico
L	H	Gg	% CO_2: 100	% N_2: 0	% H_2S: 0
Prover	Meter Run: 4.0	Taps: Flange			

FLOW DATA / TUBING DATA / CASING DATA

NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	Tubing Press. p.s.i.g.	Tubing Temp. °F	Casing Press. p.s.i.g.	Casing Temp. °F	Duration of Flow
SI							298		0		24 hrs
1.	4.026	x	2.375	190	31	53	192	53	0		24 hrs
2.	4.026	x	2.375	203	25	54	204	54	0		24 hrs
3.	4.026	x	2.375	225	15	56	227	56	0		24 hrs
4.	4.026	x	2.375	238	11	55	240	55	0		24 hrs
5.											

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1							
2.							1952
3.							1834
4.							1574
5.							1325

NO.	P_t	Temp. °R	T_t	Z
1.				
2.				
3.				
4.				
5.				

Gas Liquid Hydrocarbon Ratio: 0 Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons: Deg.
Specific Gravity Separator Gas: 1.529 XXXXXXXXX
Specific Gravity Flowing Fluid: XXXXX
Critical Pressure: 1072 P.S.I.A. P.S.I.A.
Critical Temperature: 496 R R

P_c 310.25 P_c^2 96,255

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1		202.25	40.905	55,350
2		215.25	46,332	49,922
3		237.25	56,287	39,967
4		250.25	62,625	33,630
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.7390$

(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1.4416$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 2814$

Absolute Open Flow: 2814 Mcfd @ 15.025
Angle of Slope θ: 33.4647
Slope, n: 0.6610

Remarks: Test was run from a low flowing tubing pressure to a high flowing tubing pressure to minimize liquid loading effects.

Approved by Commission:	Conducted By:	Calculated By:	Checked By:
	RANDY MAHANNAH	RICHARD ROETH	