

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
 Revised 9-1-65

Type Test <input checked="" type="checkbox"/> Initial <input type="checkbox"/> Annual <input type="checkbox"/> Special				Test Date 7-4-87								
Company Amoco Production Company			Connection									
Pool Bravo Dome			Formation Tubb		Unit BDCDGU							
Completion Date 1-12-81		Total Depth 2650		Plug Back TD 2587	Elevation 4792							
Csq. Size 5.50	Wt. 14	d 4.9	Set At 2650	Perforations: From 2220 To 2438								
Tq. Size 2.875	Wt. 6.5	d 2.441	Set At 2170	Perforations: From To								
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single				Packer Set At 2170								
Producing Thru Tubing		Reservoir Temp. °F 90	Mean Annual Temp. °F 50	Baro. Press. - P _g 12.25								
L	H	G _g	% CO ₂ 100	% N ₂ 0	% H ₂ S. 0							
				Prover	Meter Run 4.0							
				Taps Flange								
FLOW DATA			TUBING DATA		CASING DATA							
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration of Flow	
SI							295		0		24 hrs	
1.	4.026	x	2.50	191	32	57	192	57	0		24 hrs	
2.	4.026	x	2.50	200	28	58	200	58	0		24 hrs	
3.	4.026	x	2.50	212	22	60	212	60	0		24 hrs	
4.	4.026	x	2.50	225	16	59	225	59	0		24 hrs	
5.												
RATE OF FLOW CALCULATIONS												
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor FL	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mc/d					
1.							2273					
2.							2188					
3.							2032					
4.							1748					
5.												
NO.	P _f	Temp. °R	T _f	Z	Gas Liquid Hydrocarbon Ratio 0 Mc/d/bbl.							
1.					A.P.L. Gravity of Liquid Hydrocarbons _____ Deg.							
2.					Specific Gravity Separator Gas 1.529 XXXXXXXXXX							
3.					Specific Gravity Flowing Fluid XXXXXX							
4.					Critical Pressure 1072 P.S.I.A. _____ P.S.I.A.							
5.					Critical Temperature 496 _____ R _____ R							
P _c 307.25 P _c ² 94,402												
NO.	P _f ²	P _w	P _w ²	P _c ² - P _w ²	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.7918$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.4451$							
1		204.25	41,718	52,685	AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 3285$							
2		212.25	45,050	49,352								
3		224.25	50,288	44,114								
4		237.25	56,288	38,115								
5												
Absolute Open Flow		3285			Mcd @ 15.025		Angle of Slope @		32.2620		Slope, n	0.6312
Remarks: Test was run from a low flowing tubing pressure to a high flowing tubing pressure to minimize liquid loading effects.												
Approved by Commission:			Conducted By: RANDY MAHANNAH			Calculated By: RICHARD ROETH			Checked By:			