OIL CONSERVATION COMMSSION

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test: [X] Initial [ ] Annual [ ] Special				Test Date: 6-26-87	
Company: Amoco Production Company			Connection		
Pool: Bravo Dome			Formation: Tubb		Unit: BDCDGU
Completion Date: 4-29-81	Total Depth: 2802		Plug Back TD: 2761	Elevation: 4542	Farm or Lease Name
Csg. Size: 5.50 / Wt.: 14 / d: 4.9	Set At: 2802		Perforations: From 2141 To 2188		Well No.: 1935-111G
Tbg. Size: 2.875 / Wt.: 6.5 / d: 2.441	Set At: 2138		Perforations: From To		Unit: G / Sec.: 11 / Twp.: 19 / Rge.: 35
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: Single			Packer Set At: 2100		County: Union
Producing Thru: Tubing	Reservoir Temp. °F: 90	Mean Annual Temp. °F: 50	Baro. Press. – P_a: 12.25		State: New Mexico
L	H	Gg	% CO_2: 100	% N_2: 0	% H_2S: 0
Prover		Meter Run: 4.0		Taps: Flange	

FLOW DATA

NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	TUBING DATA Press. p.s.i.g.	TUBING DATA Temp. °F	CASING DATA Press. p.s.i.g.	CASING DATA Temp. °F	Duration of Flow
SI							275		0		24 hrs
1.	4.026	x	1.50	218	31	60	219	60	0		24 hrs
2.	4.026	x	1.50	228	26	62	228	62	0		24 hrs
3.	4.026	x	1.50	243	15	61	244	61	0		24 hrs
4.	4.026	x	1.50	259	1	60	258	60	0		24 hrs
5.											

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1							778
2.							736
3.							563
4.							245
5.							

NO.	P_t	Temp. °R	T_t	Z
1.				
2.				
3.				
4.				
5.				

Gas Liquid Hydrocarbon Ratio: 0 Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons: Deg.
Specific Gravity Separator Gas: 1.529 XXXXXXXXX
Specific Gravity Flowing Fluid: XXXXX
Critical Pressure: 1072 P.S.I.A. P.S.I.A.
Critical Temperature: 496 R R

P_c 287.25 P_c^2 82,512

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1		230.25	53,015	29,496
2		240.25	57,720	24,792
3		255.25	65.152	17.359
4		271.25	73,576	8,935
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 2.7974$

(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 2.7054$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 2104$

Absolute Open Flow: 2104 Mcfd @ 15.025 | Angle of Slope θ: 44.0537 | Slope, n: 0.9675

Remarks: Test was run from a low flowing tubing pressure to a high flowing tubing pressure to minimize liquid loading effects.

Approved by Commission:	Conducted By:	Calculated By:	Checked By:
	RANDY MAHANNAH	RICHARD ROETH	