

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special		Test Date 7-10-87	
Company Amoco Production Company		Connection	
Pool Bravo Dome		Formation Tubb	
Completion Date 3-27-81		Total Depth 2671	Plug Back TD 2523
Elevation 4810		Unit BDCDGU	
Csg. Size 5.50	Wt. 14	d 4.9	Set At 2671
Perforations: From 2236	To 2493		Well No. 2034-091G
Tub. Size 2.875	Wt. 6.5	d 2.441	Set At 2223
Perforations: From	To		Unit G
Type Well - Single - Bradenhead - G.G. or G.O. Multiple		Packer Set At 2187	Sec. 9
Producing Thru Tubing		Reservoir Temp. °F 90	Mean Annual Temp. °F 50
Baro. Press. - P _g 12.25		State New Mexico	
L	H	G _g	% CO ₂ 100
			% N ₂ 0
			% H ₂ S. 0
Prover		Meter Run 4.0	Taps Flange

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
1.	4.026	x	1.875	194	32	62	194	62	0		24 hrs
2.	4.026	x	1.875	204	25	62	201	62	0		24 hrs
3.	4.026	x	1.875	230	9	63	228	63	0		24 hrs
4.	4.026	x	1.875	258	1	63	255	63	0		24 hrs
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _L	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mscf/d
1.							
2.							
3.							
4.							
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	Mcf/bbl.
1.					0	
2.						
3.						
4.						
5.						

A.P.I. Gravity of Liquid Hydrocarbons _____ Mcl/bbl. Specific Gravity Separator Gas <u>1.529</u> _____ Deg. Specific Gravity Flowing Fluid <u>X X X X X</u> _____ Critical Pressure <u>1072</u> _____ P.S.I.A. Critical Temperature <u>496</u> _____ P.S.I.A.			
P _c <u>288.25</u> P _c ² <u>83,088</u>			

NO.	F _r ²	P _w	P _w ²	P _c ² - P _w ²
1.		206.25	42,539	40,549
2.		213.25	45,475	37,612
3.		240.25	57,720	25,367
4.		267.25	71,422	11,665
5.				

$$(1) \frac{P_c^2}{P_c^2 - P_w^2} = \frac{2.0491}{2.0491 - 2.0491} = 2.0491$$

$$(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \frac{2.0491}{2.0491 - 2.0491} = 2.0491$$

$$Q = \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2584$$

Absolute Open Flow	2584	Mcf/d @ 15.025	Angle of Slope @	45	Slope, n	1.0
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Remarks: Test was run from a low flowing tubing pressure to a high flowing tubing pressure to minimize liquid loading effects.

Approved by Commission:	Conducted By: RANDY MAHANNAH	Calculated By: RICHARD ROETH	Checked By:
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