

NEW MEXICO OIL CONSERVATION COMMISSION  
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122  
Revised 9-1-65

Type Test: <input checked="" type="checkbox"/> Initial <input type="checkbox"/> Annual <input type="checkbox"/> Special				Test Date: 8-10-87							
Company: Amoco Production Company			Connection:								
Pool: Bravo Dome		Formation: Tubb		Unit: BDCDGU							
Completion Date: 4-8-81		Total Depth: 2565	Plug Back TD: 2618	Elevation: 4667	Farm or Lease Name:						
Csg. Size: 5.50	Wl.: 14#	d: 5.012	Set At: 2618	Perforations: From 2283 To 2324							
Perforations: From 2283 To 2324	Well No.: 2035-181F	Unit: F	Sec: 18	Twp: 20	Rge: 35						
Type Well - Single - Brdenhead - G.C. or G.O. Multiple: Single			Packer Set At: 2199		County: Union						
Producing Thru Tubing	Reservoir Temp. °F: 90	Mean Annual Temp. °F: 50	Baro. Press. - P <sub>g</sub> : 12.25		State: New Mexico						
L:	H:	G <sub>g</sub> :	% CO <sub>2</sub> : 100	% N <sub>2</sub> : 0	% H <sub>2</sub> S: 0						
Prover:	Meter Run: 4.0	Taps: Flange									
FLOW DATA			TUBING DATA		CASING DATA						
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h <sub>w</sub>	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration of Flow
1.	4.026 x 1.125			212	7	50	212	50	0		24 hr.
2.	4.026 x 1.125			187	12	54	187	54	0		1 hr.
3.	4.026 x 1.125			165	14	54	165	54	0		1 hr.
4.	4.026 x 1.125			140	16	55	140	55	0		1 hr.
5.											
RATE OF FLOW CALCULATIONS											
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P <sub>m</sub>	Flow Temp. Factor Ft.	Gravity Factor F <sub>g</sub>	Super Compress. Factor, F <sub>pv</sub>	Rate of Flow Q, Mc/d				
1.							197				
2.							244				
3.							250				
4.							254				
5.											
NO.	F <sub>t</sub>	Temp. °R	T <sub>f</sub>	Z	Gas Liquid Hydrocarbon Ratio 0 Mc/d/bbl.						
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.						
2.					Specific Gravity Separator Gas 1.529 X X X X X X X X X						
3.					Specific Gravity Flowing Fluid X X X X X						
4.					Critical Pressure 1072 P.S.I.A. P.S.I.A.						
5.					Critical Temperature 496 R R						
F <sub>c</sub> 284.25	F <sub>c</sub> <sup>2</sup> 80798										
NO.	F <sub>t</sub> <sup>2</sup>	P <sub>w</sub>	P <sub>w</sub> <sup>2</sup>	P <sub>c</sub> <sup>2</sup> - P <sub>w</sub> <sup>2</sup>	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 2.6482$		(2) $\left[ \frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2.1057$				
1.		224.25	50288	30510							
2.		199.25	39701	41097							
3.		177.25	31418	49380							
4.		152.25	23180	57618							
5.					AOF = Q $\left[ \frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 415$						
Absolute Open Flow 415 Mc/d @ 15.025				Angle of Slope @ 37.40				Slope, n 0.7646			
Remarks: Low production rates and small amounts of liquid production caused erratic plotting on log - log plot.											
Approved by Commission:			Conducted By: RANDY MAHANNAH			Calculated By: RICHARD ROETH			Checked By:		