

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
 Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 5-15-85	
Company Amoco Production Company				Connection			
Pool Bravo Dome Carbon Dioxide Gas Unit 640-acre area				Formation Tubb		Unit BDCDGU	
Completion Date 12-19-81		Total Depth 2910'		Plug Back TD 2864'		Elevation 4605' GL	
Csg. Size 5-1/2"	Wt. 14#	d	Set At 2903'	Perforations: From 2393' To 2450'		Well No. 1835 311K	
Tbg. Size 2-7/8"	Wt. 6.5#	d	Set At 2229'	Perforations: From To		Unit Sec. Twp. Rge. K 31 18 35	
Type Well - Single - Brdenhead - G.G. or G.O. Multiple Single				Packer Set At 2342'		County Union	
Producing Thru Tubing		Reservoir Temp. °F 97° @ 2422'		Mean Annual Temp. °F 50		Baro. Press. - P _a 12.2	
L 2422'		H 2422'	Gg 1.529	% CO ₂ 100	% N ₂ 0	% H ₂ S 0	Prover Meter Run 4.0" Taps Flange

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	
SI							363			
1.	4.026 x 1.75			223	39	56	235.2	50		
2.	4.026 x 1.75			247	27	57	259.2	50		
3.	4.026 x 1.75			261	20	59	273.2	50		
4.	4.026 x 1.75			272	17	59	284.2	50		
5.										

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1							1217
2							1061
3							964
4							877
5							

NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.					Specific Gravity Separator Gas _____ X X X X X X X X
3.					Specific Gravity Flowing Fluid _____ X X X X X
4.					Critical Pressure _____ 1072 P.S.I.A. _____ P.S.I.A.
5.					Critical Temperature _____ 547 R _____ R

P _c 375.2	P _c ² 140.775			
NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²
1		235.2		85.456
2		259.2		73.590
3		273.2		66.137
4		284.2		60.005
5				

$$(1) \frac{P_c^2}{P_c^2 - P_w^2} = 1.647$$

$$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1936$$

$$(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.59$$

Absolute Open Flow	1936	Mcf/d @ 15.025	Angle of Slope θ	Slope, n .93
Remarks:				
Approved By Commission:	Conducted By:	Calculated By:	Checked By:	
		D. D. Kimble		