

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special		Test Date 7-11-87	
Company Amoco Production Company		Connection	
Pool Bravo Dome		Formation Tubb	
Completion Date 4-16-81		Total Depth 2648	Plug Back TD 2500
Elevation 4810		Farm or Lease Name	
Csg. Size 5.50	Wt. 14	d 4.9	Set At 2598
Perforations From 2265	To 2440		Well No. 2034-101J
Tag. Size 2.875	Wt. 6.5	d 2.441	Set At 2249
Perforations From		To	
Type well - Single - Bradenhead - G.G. or G.O. Multiple Single		Packer Set At 2210	Unit BDCDGU
Producing Thru Tubing		Reservoir Temp. °F 90	Mean Annual Temp. °F 50
Baro. Press. - P _g 12.25		State New Mexico	
L	H	Gg	% CO ₂ 100
			% N ₂ 0
			% H ₂ S. 0
Prover		Meter Run 4.0	Taps Flange

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
1.	4.026	x	2.375	189	26	60	186	60	0		24 hrs
2.	4.026	x	2.375	199	22	61	199	61	0		24 hrs
3.	4.026	x	2.375	210	16	62	218	62	0		24 hrs
4.	4.026	x	2.375	226	10	62	227	62	0		24 hrs
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor FL	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mscf
1.							1836
2.							1720
3.							1507
4.							1210
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	Mcf/bbl.
1.					0	
2.						
3.						
4.						
5.						

A.P.L. Gravity of Liquid Hydrocarbons		Specific Gravity Separator Gas 1.529		XXXXXXX	
Specific Gravity Flowing Fluid		XXXXX		XXXXXXX	
Critical Pressure 1072		P.S.I.A.		P.S.I.A.	
Critical Temperature 496		R		R	

P _c 306.25	P _w 93.789	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.7213$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.5091$
NO 1	P _r 198.25	P _w 39,303	P _c ² - P _w ² 54,486
2	211.25	44,626	49,162
3	230.25	53,015	40,774
4	239.25	57,240	36,548
5			

Absolute Open Flow 2770		Mscf @ 15.025	Angle of Slope @ 37.1548	Slope, n 0.8208
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Remarks: Test was run from a low flowing tubing pressure to a high flowing tubing pressure to minimize liquid loading effects.

Approved by Commission:	Conducted By: RANDY MAHANNAH	Calculated By: RICHARD ROETH	Checked By:
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