

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test: <input checked="" type="checkbox"/> Initial <input type="checkbox"/> Annual <input type="checkbox"/> Special				Test Date: 5-24-85							
Company: Amoco Production Company			Connection:								
Pool: Bravo Dome Carbon Dioxide Gas Unit 640-acre area			Formation: Tubb		Unit: BDCDGU						
Completion Date: 11-30-85		Total Depth: 2740'	Plug Back TD: 2616'	Elevation: 4551" GL	Farm or Lease Name:						
Csg. Size: 7"	Wt.: 20#	Set At: 2740'	Perforations: From 2153' To 2254'		Well No.: 1834 141G						
Tbg. Size: 2-7/8"	Wt.: 6.5	Set At: 2358'	Perforations: From To		Unit: G Sec: 14 Twp: 18 Rge: 35						
Type Well - Single - Bradenhead - G.G. or G.O. Multiple: Single				Packer Set At: 2327'	County: Union						
Producing Thru Tubing		Reservoir Temp. *F: 96 @ 2204'	Mean Annual Temp. *F: 50	Baro. Press. - P _a : 12.2	State: New Mexico						
L: 2204'	H: 2204'	G _g : 1.529	% CO ₂ : 100	% N ₂ : 0	% H ₂ S: 0						
Prover:		Meter Run: 4.0"		Taps: Flange							
FLOW DATA											
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. *F	TUBING DATA		CASING DATA		Duration of Flow
							Press. p.s.i.g.	Temp. *F	Press. p.s.i.g.	Temp. *F	
SI							329				
1.	4.026 x 2.25			200	38	53	212.2	50			24 hrs
2.	4.026 x 2.25			215	33	54	227.2	50			24 hrs
3.	4.026 x 2.25			247	22	56	259.2	50			24 hrs
4.	4.026 x 2.25			273	15	57	285.2	50			24 hrs
5.											
RATE OF FLOW CALCULATIONS											
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd				
1							1956				
2							1886				
3							1648				
4							1433				
5											
NO.	P _r	Temp. *R	T _r	Z	Gas Liquid Hydrocarbon Ratio: 0 Mcf/bbl.						
1					A.P.I. Gravity of Liquid Hydrocarbons: 0 Deg.						
2					Specific Gravity Separator Gas: 1.529		XXXXXXXXXX				
3					Specific Gravity Flowing Fluid: XXXXX						
4					Critical Pressure: 1072 P.S.I.A.		P.S.I.A.				
5					Critical Temperature: 547 R		R				
P _c 341.2 P _c ² 116.417											
NO.	F _t ²	P _w	P _w ²	P _c ² - P _w ²	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.63$						
1		212.2		71.389	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.24$						
2		227.2		64.798							
3		259.2		49.232							
4		285.2		35.078	AOF = C $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2426$						
5											
Absolute Open Flow: 2426 Mcfd @ 15.025					Angle of Slope θ :		Slope, n: .44				
Remarks:											
Approved by Commission:		Conducted By:		Calculated By: D. D. Kimble		Checked By:					

1834 1416

46 7200

LOGARITHMIC 2 x 2 CYCLES
KEUFFEL & ESSER CO. MADE IN U.S.A.

AOF = 2426

2 2 1 2 2

$$Q = MCF$$

