

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test <input checked="" type="checkbox"/> Initial <input type="checkbox"/> Annual <input type="checkbox"/> Special		Test Date 4-29-85													
Company Amoco Production Company		Connection													
Pool Carbon Dioxide Gas Bravo Dome Unit 40 Acre Area		Formation Tubb													
Completion Date 11/29/82		Total Depth 2482	Flug Back TD 2392												
		Elevation 4778	Farm or Lease Name												
Csg. Size 5" liner	Wt. 12.83	Set At 2482	Perforations: From 2182 To 2384												
Inq. Size 3.5	Wt. 9.3	Set At 2197	Perforations: From To												
Type Well - Single - Brazenhead - G.G. or G.O. Multiple Single		Packer Set At 2147	Unit BDCDGU												
Producing Thru Tubing	Reservoir Temp. *F 90 @ 2283	Mean Annual Temp. *F 50	Baro. Press. - P _a 12.5												
L 2283	H 2283	G _g 1.529	% CO ₂ 100												
		% N ₂ 0	% H ₂ S 0												
		Prover	Meter Run 4.0												
			Taps Flange												
FLOW DATA															
TUBING DATA															
CASING DATA															
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. hw	Temp. *F	Press. p.s.i.g.	Temp. *F	Press. p.s.i.g.	Temp. *F	Duration of Flow				
1.	4.026 x		2.125	277	18	60	315	50			24 hr				
2.	4.026 x		2.125	255	17	60	281	50			24 hr				
3.	4.026 x		2.125	236	31	60	259	50			24 hr				
4.	4.026 x		2.125	216	46	59	241	50			24 hr				
5.							221	50			24 hr				
RATE OF FLOW CALCULATIONS															
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd								
1.							905								
2.							1331								
3.							1681								
4.							1955								
5.															
NO.	P _r	Temp. *R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.										
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.										
2.					Specific Gravity Separator Gas 1.529 X X X X X X X X X										
3.					Specific Gravity Flowing Fluid X X X X X										
4.					Critical Pressure 1072 P.S.I.A.										
5.					Critical Temperature 547 P.S.I.A.										
P _c 327.2 P _c ² 107,060															
NO.	P _w	P _w ²	P _r ² - P _w ²	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 2.032$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.809$											
1.	293.2		21,094	ACF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 3536$											
2.	271.2		33,510												
3.	253.2		42,950												
4.	233.2		52,678												
5.															
Absolute Open Flow 3536		Mcf @ 15.025			Angle of Slope θ			Slope, n .836							
Remarks:															
Approved by Commission:				Conducted By:				Calculated By: D. R. White				Checked By:			