NEW MEXICO OIL CONSERVATION COMMSSION

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test: [X] Initial [ ] Annual [ ] Special — Test Date: 4-9-85

Company: Amoco Production Company	Connection:		
Pool: Bravo Dome Carbon Dioxide Unit - 640 acre area	Formation: Tubb		Unit: BDCDGU
Completion Date: 11-17-83	Total Depth: 2672	Plug Back TD: 2520	Elevation: 4822
Farm or Lease Name:			
Csg. Size: 7 / Wt.: 20 / d: / Set At: 2672	Perforations: From 2320 To 2450		Well No.: 2034 031G
Tbg. Size: 3.5 / Wt.: 9.3 / d: / Set At: 2314	Perforations: From To		Unit: G / Sec.: 03 / Twp.: 20 / Rge.: 34
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: Single	Packer Set At: 2283		County: Union
Producing Thru: Tubing	Reservoir Temp. °F: 90° @	Mean Annual Temp. °F: 50	Baro. Press. – P_a: 12.2
			State: New Mexico

L	H	Gg	% CO_2	% N_2	% H_2S	Prover	Meter Run	Taps
2385	2385	1.529	100	0	0		4.0	Flange

NO.	FLOW DATA: Prover Line Size X Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	TUBING DATA: Press. p.s.i.g.	Temp. °F	CASING DATA: Press. p.s.i.g.	Temp. °F	Duration of Flow
SI					307				
1.	4.026 x 1.875	218	50	60	230.2	50			24 hr.
2.	4.026 x 1.875	238	31	61	250.2	50			24 hr.
3.	4.026 x 1.875	263	15	60	265.2	50			24 hr.
4.	4.026 x 1.875	284	7	60	296.2	50			24 hr.
5.									

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1							
2							1500
3							1258
4							1100
5							626

NO.	P_t	Temp. °R	T_r	Z
1				
2				
3				
4				
5				

Gas Liquid Hydrocarbon Ratio 0 Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons 0 Deg.
Specific Gravity Separator Gas 1.529 XXXXXXXXX
Specific Gravity Flowing Fluid XXXXX
Critical Pressure 1072 P.S.I.A. ____ P.S.I.A.
Critical Temperature 547 R ____ R

P_c 319.2 P_c^2 101.889

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1		230.2		48.897
2		250.2		39.289
3		265.2		31.558
4		296.2		14.154
5				

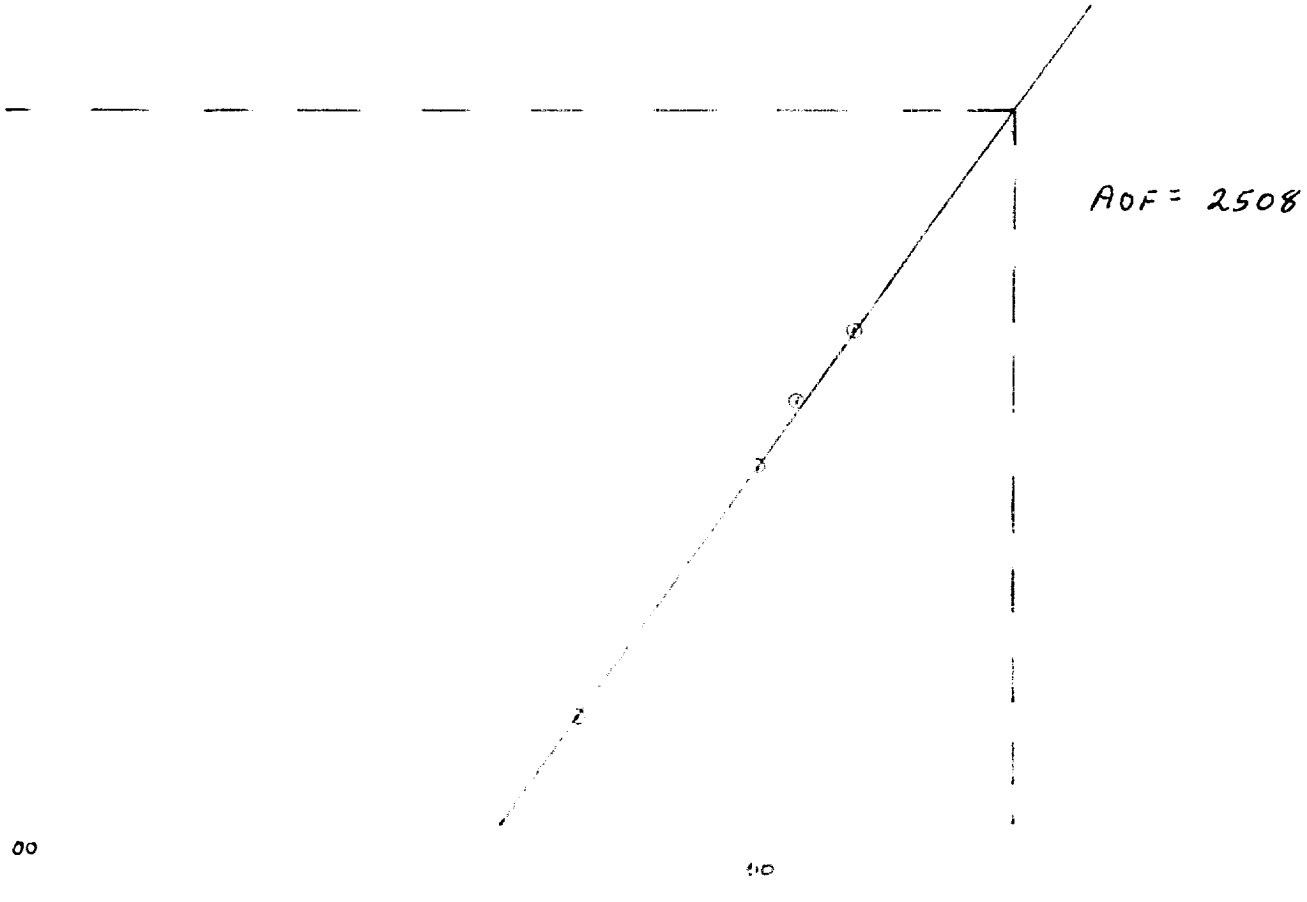
(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 2.08$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1.67$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 2508$

Absolute Open Flow 2508 Mcfd @ 15.025 Angle of Slope θ ____ Slope, n .70

Remarks:

Approved By Commission:	Conducted By:	Calculated By:	Checked By:
		D. D. Kimble	


AOF = 2508
$P_c^2 - P_w^2$
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