

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
 Revised 9-1-65

Type Test <input checked="" type="checkbox"/> Initial <input type="checkbox"/> Annual <input type="checkbox"/> Special			Test Date 9-24-85								
Company Amoco Production Company			Connection								
Pool Bravo Dome Carbon Dioxide Gas Formation			Unit BDCDGU								
Completion Date 3-14-84		Total Depth 2570	Plug Back TD 2500	Elevation 4733							
Csg. Size 7	Wt. 20	d	Set At 2277	Perforations: From 2106 To 2359							
Thq. Size 3.5	Wt. 9.3	d	Set At 2086	Perforations: From To							
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single			Packer Set At 2024		County Union						
Producing Thru Tubing		Reservoir Temp. °F 90 # 2233	Mean Annual Temp. °F 50	Baro. Press. - P _a							
L 2233	H 2233	G _g 1.529	% CO ₂ 100	% N ₂ 0	% H ₂ S 0						
Prover			Meter Run 4.0	Taps Flange							
FLOW DATA											
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. hw'	Temp. °F	TUBING DATA		CASING DATA		Duration of Flow
							Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI							337				
1.	4.026 x 2.50			195	56	55	195	50			24 hr.
2.	" "			217	40	56	217	"			"
3.	" "			226	34	57	226	"			"
4.	" "			255	18	58	255	"			"
5.											
RATE OF FLOW CALCULATIONS											
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd				
1.							2925				
2.							2616				
3.							2183				
4.							1995				
5.											
NO.	R _t	Temp. °R	T _f	Z	Gas Liquid Hydrocarbon Ratio _____ 0 _____ Mcf/bbl.						
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ 0 _____ Deg.						
2.					Specific Gravity Separator Gas _____ 1.529 _____	XXXXXXXXXX					
3.					Specific Gravity Flowing Fluid _____ XXXXX _____						
4.					Critical Pressure _____ 1072 _____ P.S.I.A.	P.S.I.A.					
5.					Critical Temperature _____ 547 _____ R	R					
P _c 349.2		P _w 121.941									
NO.	P _i ²	P _w	P _w ²	P _c ² - P _w ²	(1) $\frac{P_c^2}{P_w^2 - P_w^2} = 1.54$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.45$					
1.		207.2		79.009							
2.		229.2		69.408							
3.		238.2		65.201							
4.		267.2		50.545							
5.											
Absolute Open Flow _____ 4248 _____ Mcfd @ 15.025				Angle of Slope Θ _____		Slope, n _____ .86					
Remarks: _____											
Approved By Commission:		Conducted By:		Calculated By: D. D. Kimble		Checked By:					