MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test: [X] Initial [ ] Annual [ ] Special			Test Date: 6-26-87	
Company: Amoco Production Company		Connection:		
Pool: Bravo Dome		Formation: Tubb		Unit: BDCDGU
Completion Date: 1-26-84	Total Depth: 2615'	Plug Back TD: 2183'	Elevation: 4505'	Farm or Lease Name:
Csg. Size: 7.0 / Wt.: 20 / d: 6.331 / Set At: 2615		Perforations: From 2046 To 2206		Well No.: 1935-351G
Tbg. Size: 3.5 / Wt.: 9.5 / d: 3.000 / Set At: 2015		Perforations: From To		Unit: G / Sec.: 35 / Twp.: 19 / Rge.: 35
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: Single		Packer Set At: 2015		County: Union
Producing Thru: Tubing	Reservoir Temp. °F: 90	Mean Annual Temp. °F: 50	Baro. Press. – P_a: 12.25	State: New Mexico

L	H	Gg	% CO_2	% N_2	% H_2S	Prover	Meter Run	Taps
			100	0	0		4.0	Flange

	FLOW DATA				TUBING DATA		CASING DATA		
NO.	Prover Line Size X Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration of Flow
SI					281		0		24 hrs
1.	4.026 x 2.00	231	35	61	229	61	0		24 hrs
2.	4.026 x 2.00	237	28	61	235	61	0		24 hrs
3.	4.026 x 2.00	246	13	61	243	61	0		24 hrs
4.	4.026 x 2.00	255	4	60	252	60	0		24 hrs
5.									

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1							
2.							1595
3.							1423
4.							1036
5.							731

NO.	P_t	Temp. °R	T_f	Z
1.				
2.				
3.				
4.				
5.				

Gas Liquid Hydrocarbon Ratio 0 Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons ____ Deg.
Specific Gravity Separator Gas 1.529 XXXXXXXXX
Specific Gravity Flowing Fluid XXXXX
Critical Pressure 1072 P.S.I.A. ____ P.S.I.A.
Critical Temperature 496 R ____ R

P_c 293.25 P_c^2 85,995

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1		241.25	58,201	27,794
2		247.25	61,132	24,863
3		255.25	65,152	20,843
4		264.25	69,828	16,167
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 3.0940$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 3.0139$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 4807$

Absolute Open Flow 4807 Mcfd @ 15.025 | Angle of Slope θ 44.32 | Slope, n .9768

Remarks: Test was run from a low flowing tubing pressure to a high flowing tubing pressure to minimize liquid loading effects.

Approved by Commission:	Conducted By:	Calculated By:	Checked By:
	RANDY MAHANNAH	RICHARD ROETH	