

NEW MEXICO OIL CONSERVATION COMMISSION MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test: ☒ Initial ☐ Annual ☐ Special		Test Date: 8-12-85	
Company: Amoco Production Company		Connection:	
Pool: Bravo Dome Carbon Dioxide Gas Unit 640 Acre Area		Formation: Tubb	
Completion Date: 12-30-83		Total Depth: 2911	Plug Back TD: 2800
		Elevation: 4832	
Csg. Size: 7	Wt.: 20	Set At: 2911	Perforations: From 2552 To 2632
Tbg. Size: 3.5	Wt.: 9.3	Set At: 2528	Perforations: From To
Type Well - Single - Bradenhead - G.G. or G.O. Multiple			
Single		Packer Set At: 2487	Well No.: 1834 071G
Producing Thru: Tubing		Reservoir Temp. °F: 90 @ 2592	Mean Annual Temp. °F: 50
		Baro. Press. - P _a : 12.2	Unit: G
			Sec.: 7
			Twp.: 18
			Rge.: 34
			County: Union
			State: New Mexico
L: 2592	H: 2592	Gg: 1.529	% CO ₂ : 100
		% N ₂ : 0	% H ₂ S: 0
		Prover: 4.0	Meter Run: 4.0
		Taps: Flange	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
1.	4.026 x 2.5			185	42	61	320				
2.	4.026 x 2.5			199	33	60	185	50			24 hr
3.	4.026 x 2.5			217	27	61	199	50			24 hr
4.	4.026 x 2.5			239	18	61	217	50			24 hr
5.							239	50			24 hr

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1.							2549
2.							2355
3.							2227
4.							1947
5.							

NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1.					0	0	1.529	X X X X X X X X	1072	547
2.										
3.										
4.										
5.										

P _c : 332.2	P _w : 110.357		
NO.	P _t ²	P _w ²	P _t ² - P _w ²
1.	197.2		71.469
2.	211.2		65.751
3.	229.2		57.824
4.	251.2		47.255
5.			

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.54$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 3380$

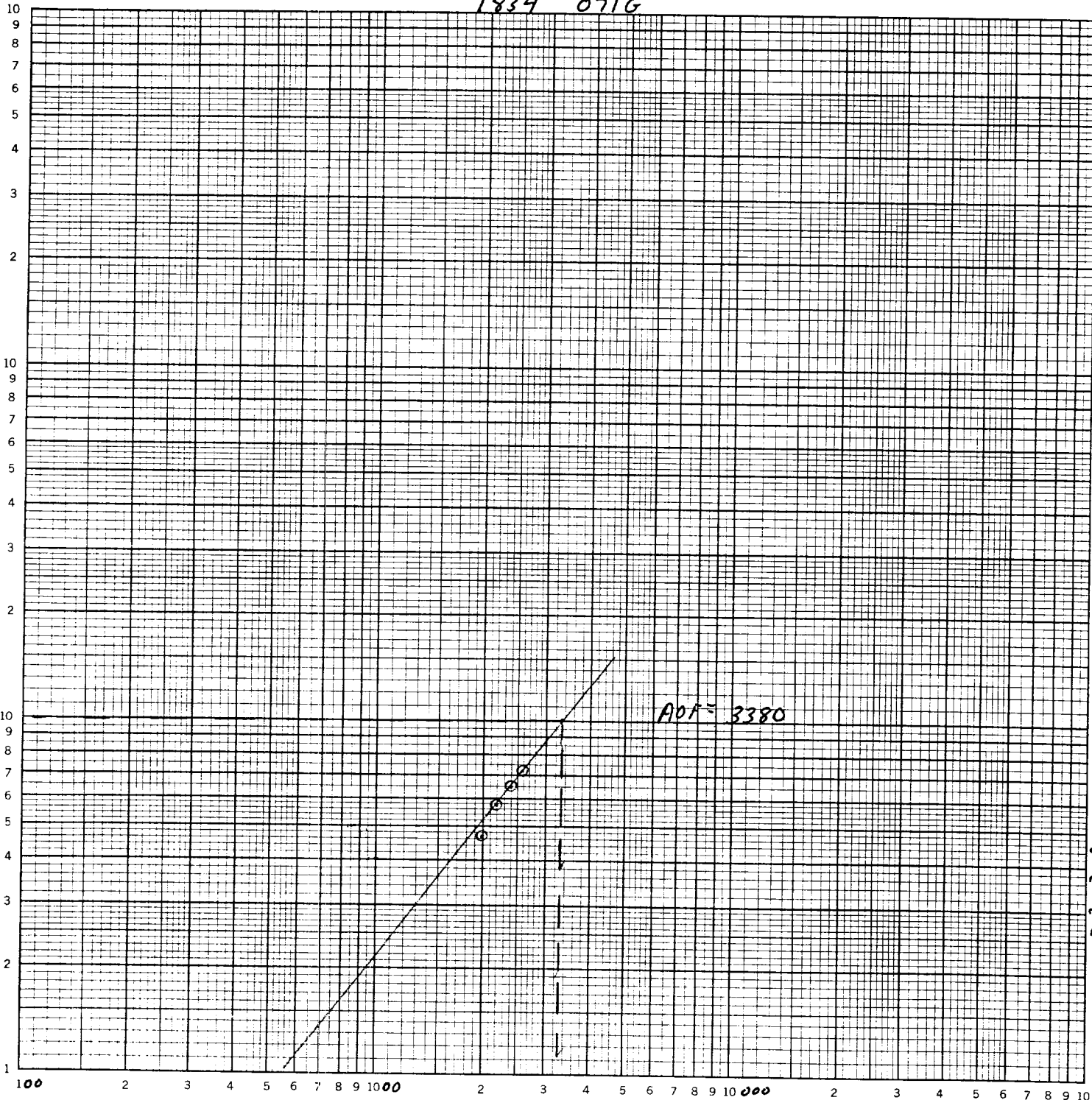
(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.33$

Absolute Open Flow: 3380	Mcfd @ 15.025	Angle of Slope θ	Slope, n: .65
Remarks:			

Approved By Commission:	Conducted By:	Calculated By: D. D. Kimble	Checked By:
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46 7400

1834 0716



Q = MCF