

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
 Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special		Test Date									
Company Amoco Production Company		Connection									
Pool Bravo Dome Carbon Dioxide Gas Unit-640 Acre Area		Formation									
Completion Date 12-1-85	Total Depth 2425	Plug Back TD 2350	Elevation 4663								
Csq. Size 7	Wt. 20	Set At 2425	Perforations: From 2228 To 2282								
Thq. Size 3-1/2	Wt. 9.3	Set At 2067	Perforations: From To								
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single		Packer Set At 2036	Unit BDCDGU								
Producing Thru Tubing	Reservoir Temp. °F 90	Mean Annual Temp. °F 50	Baro. Press. - P _a 12.25								
L 2255	H 2255	C _g 1.529	% CO ₂ 100								
		% N ₂ 0	% H ₂ S 0								
		Prover	Meter Run 4.0								
			Taps Flange								
FLOW DATA											
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	TUBING DATA		CASING DATA		Duration of Flow
							Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
1.	4.026 x 2.500			182.1	4.5	47	281				
2.	4.026 x 2.500			151.2	4	48	194.35	47			1.5
3.	4.026 x 2.500			124.7	4	48	163.45	48			1.5
4.	4.026 x 2.500			98.7	6	48	136.95	48			1.5
5.						48	110.95	48			1.5
RATE OF FLOW CALCULATIONS											
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd				
1.											
2.							580				
3.							631				
4.							699				
5.							852				
NO.	P _f	Temp. °R	T _f	Z	Gas Liquid Hydrocarbon Ratio _____ Mcl/bbl. A.P.I. Gravity of Liquid Hydrocarbons _____ Deg. Specific Gravity Separator Gas 1.529 Specific Gravity Flowing Fluid _____ Critical Pressure 1072 P.S.I.A. Critical Temperature 496 R						
1.											
2.											
3.											
4.											
5.											
P _c 293.2 P _c ² 85,966					(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.16$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.15$						
NO.	P _f ²	P _w	P _w ²	P _c ² - P _w ²							
1.		194		48.330							
2.		163		59.397							
3.		136		67.470							
4.		110		73.866							
5.											
AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 978$											
Absolute Open Flow 978 Mcfd @ 15.025 Angle of Slope θ _____ Slope, n .91											
Remarks:											
Approved by Commission:		Conducted By:		Calculated By: Don Kimble							
				Checked By:							