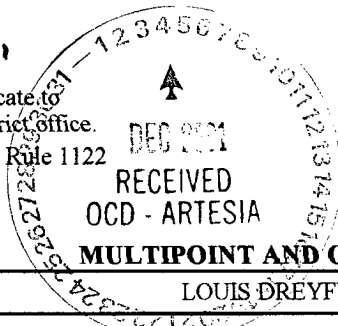


Submit in duplicate to appropriate district office.
See Rule 401 & Rule 1122



State of New Mexico
Energy Minerals and Natural Resources
Oil Conservation Division
2040 South Pacheco
Santa Fe, NM 87505

30-015-21757
Form C-122
Revised October, 1999
CONFIDENTIAL

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Operator LOUIS DREYFUS /					Lease or Unit Name SARAGOSA "10" STATE				
Type Test ☒ Initial ☐ Annual ☐ Special					Test Date 9/11/01		Well No. 1		
Completion Date 9/11/01		Total Depth 12000		Plug Back TD 11866		Elevation		Unit Ltr - Sec - TWP - Rge A 10 23S 26E	
Csg. Size 4 1/2	Wt. 13.5	d 3.92	Set At 12000		Perforations: From: 11634 To: 11714		County EDDY		
Tbg. Size 2 3/8	Wt. 4.7	d 1.995	Set At 11595		Perforations: From: To:		Pool 5 Canisbad Morrow		
Type Well-Single-Bradenhead-G.G. or G.O. Multiple SINGLE					Packer Set At 11527		Formation MORROW		
Producing Thru Tubing		Reservoir Temp. °F 189.9		Mean Annual Temp. °F 60		Baro. Press. -P _a 13.2		Connection AIR	
L 11595	H 11595	Gg 0.744	%CO ₂ 17.74	%N ₂ 1.22	%H ₂ S N/A	Prover N/A	Meter Run 4.026	Taps FLG	

FLOW DATA				TUBING DATA				CASING DATA		Duration of Flow
No.	Prover Line Size	Orifice Size	Press p.s.i.g.	Diff. h _w	Temp. °F	Press p.s.i.g.	Temp. °F	Press p.s.i.g.	Temp. °F	
SI						2580	N/A	PKR	N/A	
1	4.026 X .750		150	2	68	2550				1 HR
2	4.026 X .750		150	10	68	2480				1 HR
3	4.026 X .750		190	19	68	2190				1 HR
4	4.026 X .750		180	36	68	1780				1 HR
5										

RATE OF FLOW CALCULATIONS							
No.	COEFFICIENT (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress Factor F _{pv}	Rate of Flow Q. Mcfd
1	2.661	18	163.2	0.9924	1.159	1.042	57
2	2.661	40.4	163.2	0.9924	1.159	1.042	128
3	2.661	62.1	203.2	0.9924	1.159	1.042	198
4	2.661	83.4	193.2	0.9924	1.159	1.042	265
5							

No.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	N/A	Mcf bbl.
1	0.71	528	1.41	0.921	A.P. I. Gravity of Liquid Hydrocarbons	N/A	Deg.
2	0.71	528	1.41	0.921	Specific Gravity Separator Gas	0.744	XXXXXXX
3	0.71	528	1.41	0.921	Specific Gravity Flowing Fluid	XXXXX	
4	0.71	528	1.41	0.921	Critical Pressure	743	P.S.I.A.
5					Critical Temperature	372	R.

P _c 2593.2		P _{c2} 6724.7	
No.	P _t ²	P _w	P _w ²
1	6570	2563.2	6570.1
2	6216	2493.3	6216.7
3	4854.1	2203.5	4855.5
4	3215.6	1793.9	3218.9
5			

(1) $P_c^2 = 1.918$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.383$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 367$

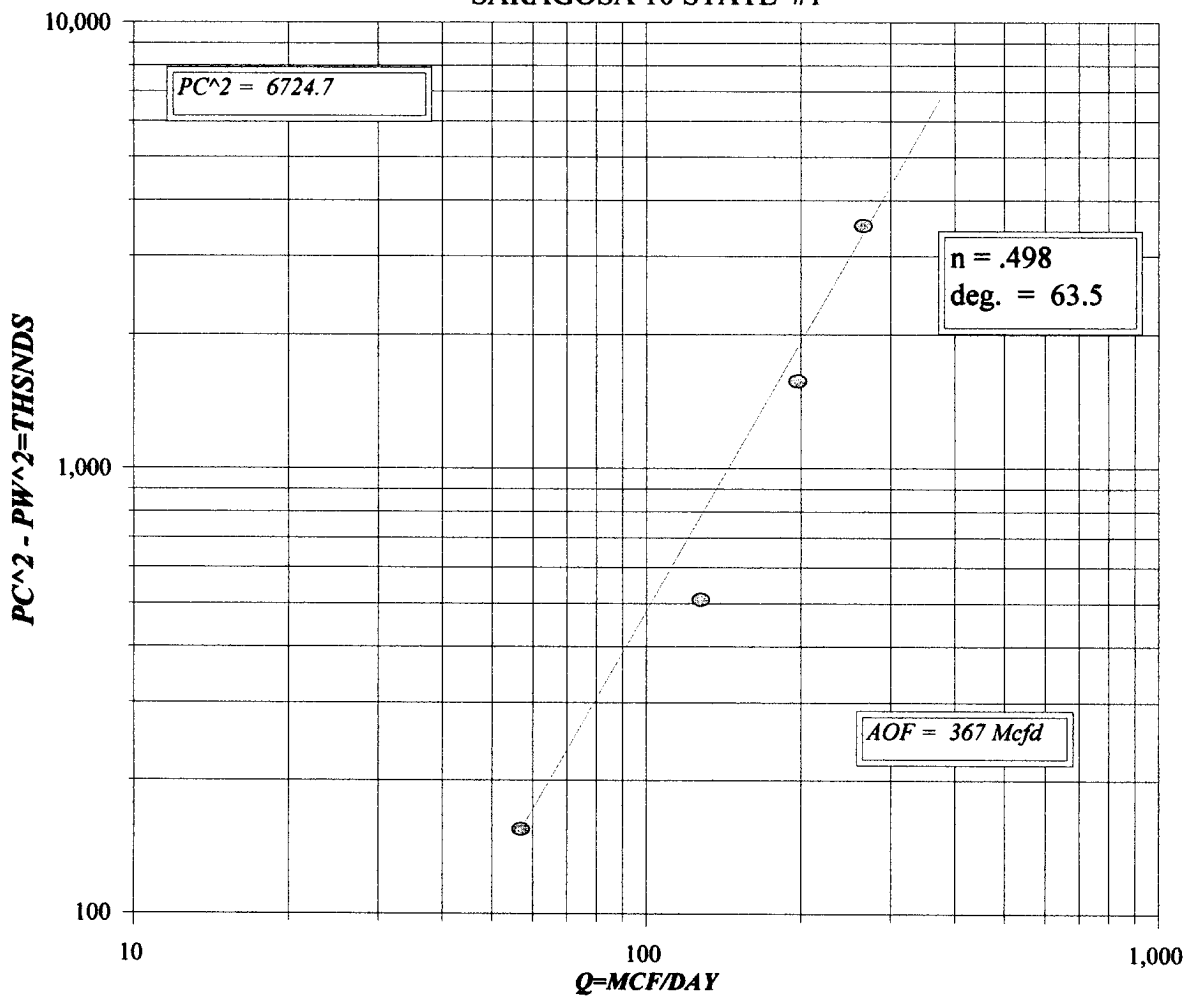
Absolute Open Flow	367	Mcf @ 15.025	Angle of Slope (°):	63.5	Slope n:	0.498
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Remarks: * NO LIQUID MADE DURING TEST.

Approved By Division:	Conducted By: PRO WELL TESTING	Calculated By: MERV BUECKER	Checked By: BM
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LOUIS DREYFUS
SARAGOSA 10 STATE #1



COMPANY :LOUIS DREYFUS LEASE :SARAGOSA 10 ST. WELL NO. : 1
UNIT :A SECTION :10 TOWNSHIP :23S
L : 11595 H : 11595 L/H : 1 G/GMIX : 0.744
%CO2 : 17.74 %N2 : 1.22 H2S : DATE :9/11/01
d : 1.995 Fr :0.018231 GH : 8626.7 RANGE :26E

VOL 1 : 57 PSIA 1 : 2563.2 RESV.TEMP 189.9
VOL 2 : 128 PSIA 2 : 2493.2
VOL 3 : 198 PSIA 3 : 2203.2 SHUT-IN PR= 2593.2
VOL 4 : 265 PSIA 4 : 1793.2

PCR : 743
TCR : 372

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LINE	RATE 1		RATE 2		RATE 3		RATE 4	
	1ST	2ND	1ST	2ND	1ST	2ND	1ST	2ND
1 QM	0.057	0.057	0.128	0.128	0.198	0.198	0.265	0.265
2 TW	534	534	534	534	534	534	534	534
3 Ts	650.0	650.0	650.0	650.0	650.0	650.0	650.0	650.0
4 T	592.0	592.0	592.0	592.0	592.0	592.0	592.0	592.0
PR (est)	3.45		3.36		2.97		2.41	
5 Z(est)	0.799	0.805	0.799	0.803	0.804	0.799	0.819	0.805
6 TZ	473.0	476.5	473.2	475.4	475.8	473.0	484.8	476.7
7 GH/TZ	18.238	18.104	18.230	18.146	18.130	18.238	17.794	18.098
8 eS	1.982	1.972	1.981	1.975	1.974	1.982	1.949	1.971
9 l-e-S	0.495	0.493	0.495	0.494	0.493	0.495	0.487	0.493
10 Pt	2563.2	2563.2	2493.2	2493.2	2203.2	2203.2	1793.2	1793.2
11 Pt2 /1000	6570.0	6570.0	6216.0	6216.0	4854.1	4854.1	3215.6	3215.6
12 Fr	0.018231	0.018231	0.018231	0.018231	0.018231	0.018231	0.018231	0.018231
13 Fc=FrTZ	8.624	8.687	8.627	8.667	8.675	8.624	8.839	8.690
14 FcQm	0.49	0.50	1.10	1.11	1.72	1.71	2.34	2.30
15 L/H(FcQm)	0.2	0.2	1.2	1.2	3.0	2.9	5.5	5.3
16 Fw	0.119688	0.120836	0.603876	0.607520	1.455421	1.444191	2.671117	2.6129987
17 Pw2	6570.1	6570.1	6216.7	6216.7	4855.5	4855.5	3218.2	3218.2
18 Ps2	13019.4	12954.6	12315.6	12276.9	9582.9	9621.9	6272.1	6343.9
19 Ps	3608.2	3599.2	3509.4	3503.8	3095.6	3101.9	2504.4	2518.7
20 P	3085.7	3081.2	3001.3	2998.5	2649.4	2652.6	2148.8	2156.0
21 Pr	4.15	4.15	4.04	4.04	3.57	3.57	2.89	2.90
22 Tr	1.59	1.59	1.59	1.59	1.59	1.59	1.59	1.59
23 Z	0.805	0.805	0.803	0.803	0.799	0.799	0.805	0.805

Pc = 2593.2 Pc2 = 6724.7 *
Pt2 = 6570.0 Pw = 2563.2 *
6216.0 2493.3 *
4854.1 2203.5 *
3215.6 1793.9 *

Pc2-Pw2= 154.6 Pw2 = 6570.1 *
508.0 6216.7 *
1869.2 4855.5 *
3506.5 3218.2 *

n = 0.498

Pc2/(Pc2-Pw2) = 43.505
13.237
3.598
1.918

[Pc2/Pc2-Pw2]n = 6.546
3.619
1.892
1.383

AOF= Q 0.373
0.463
0.375
0.367

FORM C122-D