Submit in duplicate to appropriate district office.
See Rule 401 & Rule 1122

State of New Mexico
Energy Minerals and Natural Resources
Oil Conservation Division
2040 South Pacheco
Santa Fe, NM 87505

30-015-33496

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SEP 16 2004
OCD-ARTESIA

Revised October, 1999

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Operator: MEWBOURNE OIL		Lease or Unit Name: BURTON FLAT "5" FED	
Type Test: ☑ Initial ☐ Annual ☐ Special		Test Date: 8/1/04	Well No.: 5
Completion Date: 7/24/04	Total Depth: 11289	Plug Back TD: 11207	Elevation: 3339 GL
Unit Ltr - Sec - TWP - Rge: C 5 20S 28E			
Csg. Size: 5 1/2 / Wt.: 17 / d: 4.892 / Set At: 11290	Perforations: From: 11028 To: 11034	County: EDDY	
Tbg. Size: 2 7/8 / Wt.: 6.5 / d: 2.441 / Set At: 11034	Perforations: From: To:	Pool: ANGLE RANCH MORROW	
Type Well-Single-Bradenhead-G.G. or G.O. Multiple: SINGLE	Packer Set At: 10957	Formation: MORROW	
Producing Thru: TUBING	Reservoir Temp.: 181	Mean Annual Temp.: 60	Baro. Press.-P_a: 13.2	Connection: SALES

L	H	Gg	%CO_2	%N_2	%H_2S	Prover	Meter Run	Taps
11032	11032	0.641	2.017	1.236			3.067	FLG

	FLOW DATA				TUBING DATA		CASING DATA		
No.	Prover Line Size x Orifice Size	Press p.s.i.g.	Diff. h_w	Temp.	Press p.s.i.g.	Temp.	Press p.s.i.g.	Temp.	Duration of Flow
SI					2973.2				
1	3.067 X 1.000	500	9.6	69	2750				24 HRS.
2									
3									
4									
5									

RATE OF FLOW CALCULATIONS

No.	COEFFICIENT (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor F_g	Super Compress Factor F pv	Rate of Flow Q. Mcfd
1							484
2	TOTAL	FLOW	METER				
3							
4							
5							

No.	P_r	Temp. R	T_r	Z
1				
2				
3	TOTAL	FLOW	METER	
4				
5				

Gas Liquid Hydrocarbon Ratio	N/A	Mcf bbl.
A.P. I. Gravity of Liquid Hydrocarbons	N/A	Deg.
Specific Gravity Separator Gas	0.59	XXXXXXX
Specific Gravity Flowing Fluid	XXXXX	
Critical Pressure	675 P.S.I.A.	P.S.I.A.
Critical Temperature	350 R.	R

P_c 2973.2 P_c2 8839.9

No.	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1		2763.8	7638.4	1201.5
2				
3				
4				
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} =$ 7.357 (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n =$ 7.357

$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n =$ 3.561

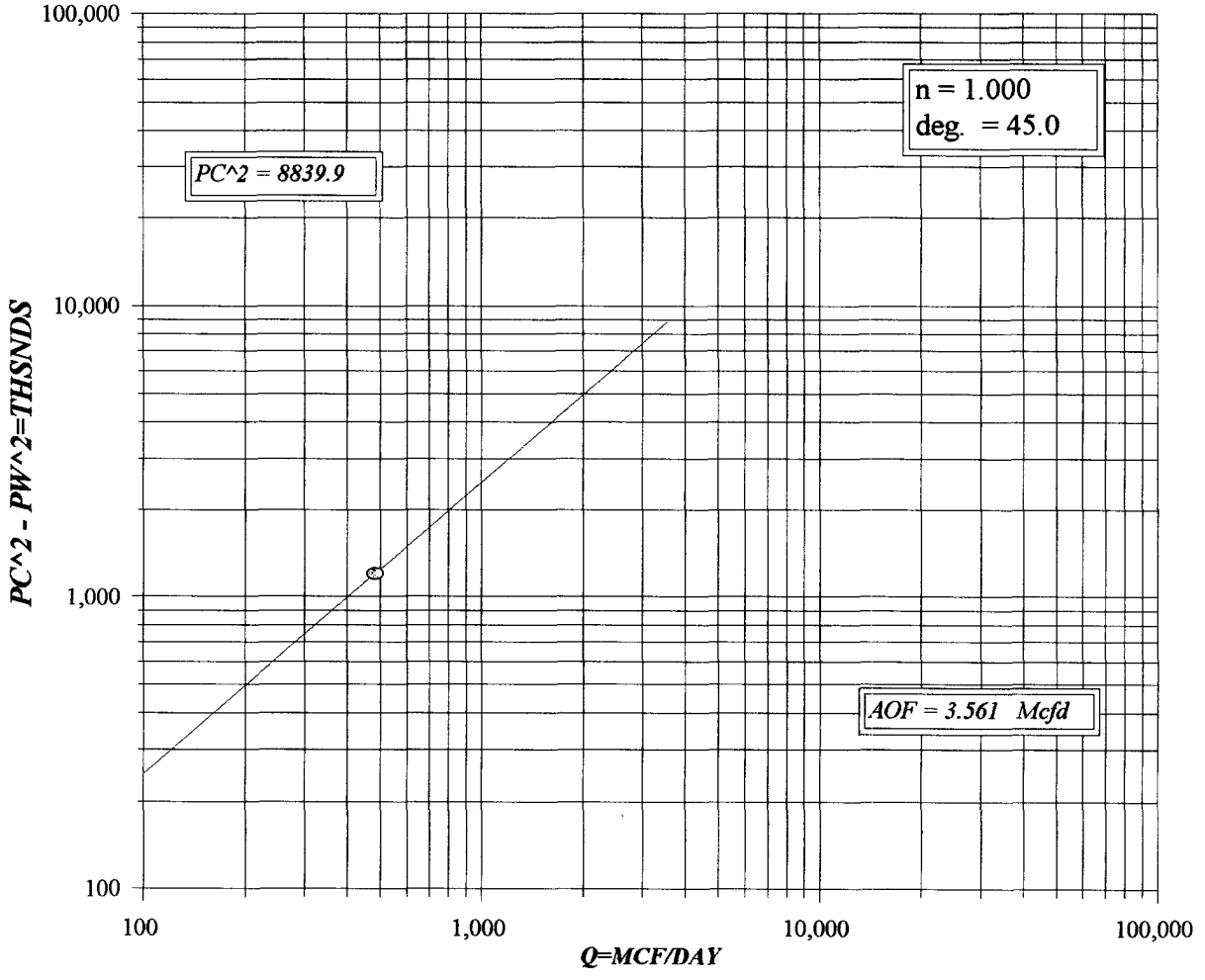
Absolute Open Flow	3.561	Mcfd @ 15.025	Angle of Slope ():	45	Slope n: 1

Remarks: * NO LIQUID MADE DURING TEST.

Approved By Division:	Conducted By:	Calculated By:	Checked By:
	PRO WELL TESTING	MERV BUECKER	BM

MEWBOURNE OIL CO.

BURTON FLAT "5" FED #5



C122D FORM IMPORTED FROM SYMPHONY ON 9-9-01

COMPANY :	MEWBOURNE OIL CO.		LEASE :	BURTON FLAT "5" FED WELL NO. :		5					
UNIT :	C		SECTION :	5		TOWNSHIP :	20S				
L :	11034	H :	11034	L/H :	1	G/GMIX :	0.590				
%CO2 :	0.901	%N2 :	0.93	H2S :			DATE :	8/1/04			
d :	2.441	Fr :	0.010763	GH :	8197.0		RANGE :	28E			
VOL 1 :	484	PSIA 1 :	2763.2			RESV.TEMP	181.0				
VOL 2 :		PSIA 2 :									
VOL 3 :		PSIA 3 :				SHUT-IN PRES =	2973.2				
VOL 4 :		PSIA 4 :									
			PCR :	675							
			TCR :	350							

LINE		RATE 1		RATE 2		RATE 3		RATE 4	
		1ST	2ND	1ST	2ND	1ST	2ND	1ST	2ND
1	QM	0.484	0.484	0.000	0.000	0.000	0.000	0.000	0.000
2	TW	534	534	534	534	534	534	534	534
3	Ts	641.0	641.0	641.0	641.0	641.0	641.0	641.0	641.0
4	T	587.5	587.5	587.5	587.5	587.5	587.5	587.5	587.5
	PR (est)	4.09		0.00		0.00		0.00	
5	Z(est)	0.838	0.854	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
6	TZ	492.6	501.7	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
7	GH/TZ	16.641	16.339	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
8	eS	1.866	1.845	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
9	I-e-S	0.464	0.458	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
10	Pt	2763.2	2763.2	0.0	0.0	0.0	0.0	0.0	0.0
11	Pt2 /1000	7635.3	7635.3	0.0	0.0	0.0	0.0	0.0	0.0
12	Fr	0.010763	0.010763	0.010763	0.010763	0.010763	0.010763	0.010763	0.010763
13	Fc=FrTZ	5.302	5.400	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
14	FcQm	2.57	2.61	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
15	L/H(FcQm)2	6.6	6.8	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
16	Fw	3.0565572	3.1290376	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
17	Pw2	7638.3	7638.4	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
18	Ps2	14256.6	14095.9	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
19	Ps	3775.8	3754.5	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
20	P	3269.5	3258.8	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
21	Pr	4.84	4.83	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
22	Tr	1.68	1.68	1.68	1.68	1.68	1.68	1.68	1.68
23	Z	0.854	0.854	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!

Pc =	2973.2	Pc2 =	8839.9
Pt2 =	7635.3	Pw =	2763.8
	0.0		#DIV/0!
	0.0		#DIV/0!
	0.0		#DIV/0!
Pc2-Pw2=	1201.5	Pw2 =	7638.4
	#DIV/0!		#DIV/0!
	#DIV/0!		#DIV/0!
	#DIV/0!		#DIV/0!
n =	1.000		
Pc2/(Pc2-Pw2) =	7.357		
	#DIV/0!		
	#DIV/0!		
	#DIV/0!		
[Pc2/Pc2-Pw2]n =	7.357		
	#DIV/0!		
	#DIV/0!		
	#DIV/0!		
AOF= Q	3.561		
	#DIV/0!		
	#DIV/0!		
	#DIV/0!		

FORM C122-D