Submit in duplicate to appropriate district office.
See Rule 401 & Rule 1122

State of New Mexico
Energy Minerals and Natural Resources
Oil Conservation Division
2040 South Pacheco
Santa Fe, NM 87505

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Form C-122
Revised October, 1999

30-015-33222

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Operator: MEWBOURNE OIL		Lease or Unit Name: DINERO 20 FED	
Type Test: ☑ Initial ☐ Annual ☐ Special		Test Date:	Well No.: 1
Completion Date:	Total Depth: 12650	Plug Back TD: 12567	Elevation: 3065 GL
Unit Ltr - Sec - TWP - Rge: P 20 22S 28E			
Csg. Size: 5 1/2 / Wt.: 20# / d: 4.778 / Set At: 12650	Perforations: From: 12410 To: 12420	County: EDDY	
Tbg. Size: 2 7/8 / Wt.: 6.5 / d: 2.441 / Set At: 11911	Perforations: From: 11997 To: 12196	Pool: DUBLIN RANCH	
Type Well-Single-Bradenhead-G.G. or G.O. Multiple: SINGLE	Packer Set At: 11897	Formation: MORROW	
Producing Thru: TUBING	Reservoir Temp.: 181	Mean Annual Temp.: 60	Baro. Press.-P_a: 13.2
Connection: SALES			

L	H	Gg	%CO_2	%N_2	%H_2S	Prover	Meter Run	Taps
10506	10506	0.61	0.806	0.27	N/A	N/A	3.067	FLG

	FLOW DATA				TUBING DATA		CASING DATA		
No.	Prover Line Size x Orifice Size	Press p.s.i.g.	Diff. h_w	Temp.	Press p.s.i.g.	Temp.	Press p.s.i.g.	Temp.	Duration of Flow
SI					1996		PKR		24 HRS
1	3.067 X 1.375	552	91.16	86	700		"		24 HRS
2									
3									
4									
5									

RATE OF FLOW CALCULATIONS

No.	COEFFICIENT (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor F_g	Super Compress Factor F pv	Rate of Flow Q. Mcfd
1							1966
2							
3	TOTAL	FLOW	METER				
4							
5							

No.	P_r	Temp. R	T_r	Z
1				
2	TOTAL	FLOW	METER	
3				
4				
5				

Gas Liquid Hydrocarbon Ratio	DRY GAS		Mcf bbl.
A.P. I. Gravity of Liquid Hydrocarbons	DRY		Deg.
Specific Gravity Separator Gas	0.574		XXXXXXX
Specific Gravity Flowing Fluid	XXXXX		N/A
Critical Pressure	675 P.S.I.A.	N/A	P.S.I.A.
Critical Temperature	342 R.	N/A	R

P_c 2009.2 P_c^2 4036.9

No.	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1		751.7	508.7	3471.8
2				
3				
4				
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} =$ 1.163 (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n =$ 1.163

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n =$ 2.286

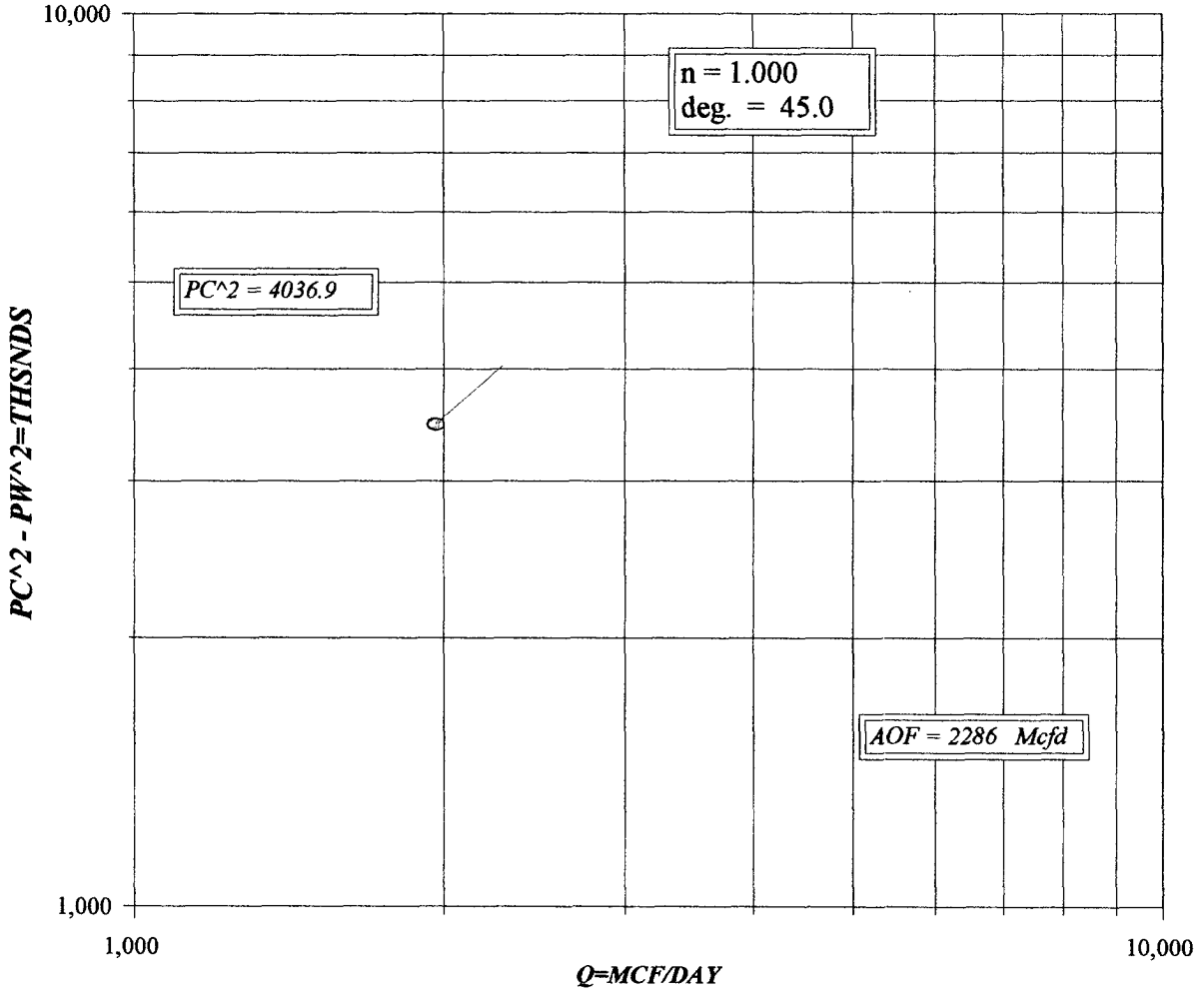
Absolute Open Flow	2.286	Mcfd @ 15.025	Angle of Slope ():	45	Slope, n: 1.000

Remarks: NO LIQUID MADE DURING TEST.

Approved By Division:	Conducted By:	Calculated By:	Checked By:
	MEWBOURNE OIL	MERV BUECKER	BM

MEWBOURNE OIL

DINERO 20 FED #1



C122D FORM IMPORTED FROM SYMPHONY ON 9-9-01

COMPANY :	MEWBOURNE OIL		LEASE	: DINERO 20 FED	WELL NO.	:	1		Pc =	2009.2	Pc2 =	4036.9
UNIT :	P		SECTION	: ,20	TOWNSHIP	:	,22S					
L :	11911	H :	11911	L/H :	1	G/GMIX	:	0.574	Pt2 =	508.7	Pw =	751.7
%CO2 :	1.239	%N2 :	,,180	H2S :			DATE	:		0.0		#DIV/0!
d :	2.441	Fr :	0.010763	GH :	8197.0		RANGE	: ,28E		0.0		#DIV/0!
										0.0		#DIV/0!
VOL 1 :	1966	PSIA 1 :	713.2			RESV.TEMP		193.0	Pc2-Pw2=	3471.8	Pw2 =	565.1
VOL 2 :		PSIA 2 :								#DIV/0!		#DIV/0!
VOL 3 :		PSIA 3 :				SHUT-IN PRI =		2009.2		#DIV/0!		#DIV/0!
VOL 4 :		PSIA 4 :								#DIV/0!		#DIV/0!
				PCR :	675					n =	1.000	
				TCR :	342							
									Pc2/(Pc2-Pw2) =		1.163	
											#DIV/0!	
											#DIV/0!	

LINE		RATE 1		RATE 2		RATE 3		RATE 4	
		`1ST	`2ND	`1ST	``2ND	`1ST	`2ND	`1ST	`2ND
1	QM	1.966	1.966	0.000	0.000	0.000	0.000	0.000	0.000
2	TW	534	534	534	534	534	534	534	534
3	Ts	653.0	653.0	653.0	653.0	653.0	653.0	653.0	653.0
4	T	593.5	593.5	593.5	593.5	593.5	593.5	593.5	593.5
	PR (est)	1.06		0.00		0.00		0.00	
5	Z(est)	0.917	0.907	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
6	TZ	544.1	538.1	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
7	GH/TZ	15.065	15.232	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
8	eS	1.759	1.770	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
9	I-e-S	0.432	0.435	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
10	Pt	713.2	713.2	0.0	0.0	0.0	0.0	0.0	0.0
11	Pt2 /1000	508.7	508.7	0.0	0.0	0.0	0.0	0.0	0.0
12	Fr	0.010763	0.010763	0.010763	0.010763	0.010763	0.010763	0.010763	0.010763
13	Fc=FrTZ	5.856	5.792	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
14	FcQm	11.51	11.39	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
15	L/H(FcQm)2	132.6	129.7	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
16	Fw	57.21437	56.42496	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
17	Pw2	565.9	565.1	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
18	Ps2	995.5	1000.4	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
19	Ps	997.8	1000.2	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
20	P	855.5	856.7	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
21	Pr	1.27	1.27	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
22	Tr	1.74	1.74	1.74	1.74	1.74	1.74	1.74	1.74
23	Z	0.907	0.907	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!

[Pc2/Pc2-Pw2]n =		1.163	
		#DIV/0!	
		#DIV/0!	
		#DIV/0!	
	AOF= Q	2.286	
		#DIV/0!	
		#DIV/0!	
		#DIV/0!	

FORM C122-D