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See Rule 401 & Rule 1122

State of New Mexico
Energy Minerals and Natural Resources
Oil Conservation Division
2040 South Pacheco
Santa Fe, NM 87505

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Form C-122
Revised October, 1999

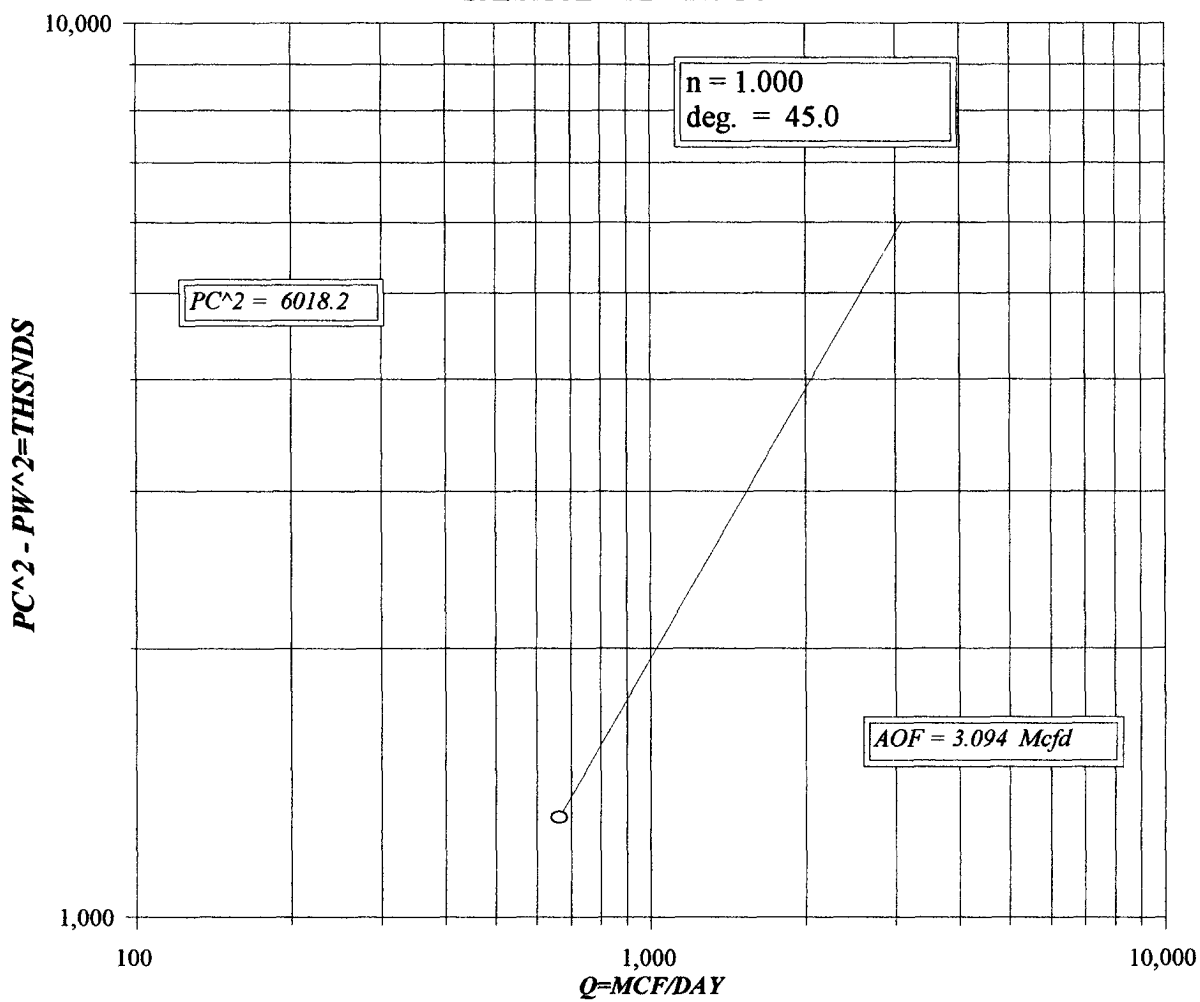
DEC - 9 2004

OLD ARTESIA 30-015-33416

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Operator MEWBOURNE OIL				Lease or Unit Name SALADAR 32 FEE COM						
Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 9/27/2004		Well No. 1		
Completion Date 9/3/2004		Total Depth 11621		Plug Back TD 11361		Elevation 3198 GL		Unit Ltr - Sec - TWP - Rge O 32 20S 26E		
Csg. Size 5 1/2	Wt. 17#	d 4.615	Set At 11621	Perforations: From: 11231 To: 11242				County EDDY		
Tbg. Size 2 7/8	Wt. 6.5	d 2.441	Set At 10519	Perforations: From: To:				Pool BURTON FLAT MORROW		
Type Well-Single-Bradenhead-G.G. or G.O. Multiple SINGLE				Packer Set At 10506				Formation MORROW		
Producing Thru TUBING		Reservoir Temp. 181		Mean Annual Temp. 60		Baro. Press.-P _a 13.2		Connection SALES		
L 10506	H 10506	Gg 0.61	%CO ₂ 0.806	%N ₂ 0.27	%H ₂ S N/A	Prover N/A	Meter Run 3.067	Taps FLG		
FLOW DATA				TUBING DATA				CASING DATA		
No.	Prover Line Size	Orifice x Size	Press p.s.i.g.	Diff. h _w	Temp.	Press p.s.i.g.	Temp.	Press p.s.i.g.	Temp.	
SI						2440		PKR		
1	3.067 X 1.375		188	2	86	2160		"		
2										
3										
4										
5										
RATE OF FLOW CALCULATIONS										
No.	COEFFICIENT (24 Hour)		$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress Factor F _{pv}	Rate of Flow Q, Mcfd		
1								665		
2										
3	TOTAL		FLOW	METER						
4										
5										
No.	P _r	Temp. R	T _r	Z	Gas Liquid Hydrocarbon Ratio				DRY GAS Mcf bbl.	
1					A.P. I. Gravity of Liquid Hydrocarbons				DRY Deg.	
2	TOTAL	FLOW	METER		Specific Gravity Separator Gas				.610 XXXXXXXX	
3					Specific Gravity Flowing Fluid				XXXXXX N/A	
4					Critical Pressure				674 P.S.I.A. N/A P.S.I.A.	
5					Critical Temperature				358 R. N/A R	
P _c 2453.2 P _{c2} 6018.2					$(1) \quad \frac{P_c^2}{P_c^2 - P_w^2} = \frac{4.653}{\quad}$ $AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \frac{\quad}{3.094}$ $(2) \quad \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \frac{4.653}{\quad}$					
No.	P _t ²	P _w	P _w ²	P _c ² - P _w ²						
1		2173.7	4724.8	1293.4						
2										
3										
4										
5										
Absolute Open Flow					3,094	Mcf @ 15.025	Angle of Slope (°):	45	Slope, n:	1.000
Remarks: NO LIQUID MADE DURING TEST.										
Approved By Division:			Conducted By:		Calculated By:		Checked By:			
			PRO WELL TESTING		MERV BUECKER		BM			

MEWBOURNE OIL
SALADAR "32" FEE COM #1



COMPANY : MEWBORNE OIL LEASE : SALADAR 32 FEE COWELL NO. : 1
UNIT : O SECTION : ,32 TOWNSHIP : ,20S
L : 10506 H : 10506 L/H : 1 G/GMIX : 0.610
%CO2 : 0.806 %N2 : 0.27 H2S : DATE : ,9/27/04
d : 2 7/8 Fr : 0.0070195 GH : 6408.7 RANGE : ,28E

VOL 1 : 665 PSIA 1 : 2173.2 RESV.TEMP 179.1
VOL 2 : PSIA 2 :
VOL 3 : PSIA 3 : SHUT-IN PR = 2453.2
VOL 4 : PSIA 4 :

PCR : 674
TCR : 358

Pc = 2453.2 Pc2 = 6018.2
Pt2 = 4722.8 Pw = 2173.7
0.0 #DIV/0!
0.0 #DIV/0!
0.0 #DIV/0!

Pc2-Pw2= 1293.4 Pw2 = 4724.8
#DIV/0! #DIV/0!
#DIV/0! #DIV/0!
#DIV/0! #DIV/0!

n = 1.000

Pc2/(Pc2-Pw2) = 4.653
#DIV/0!
#DIV/0!
#DIV/0!

[Pc2/Pc2-Pw2]n = 4.653
#DIV/0!
#DIV/0!

AOF= Q 3.094
#DIV/0!
#DIV/0!
#DIV/0!

LINE		RATE 1		RATE 2		RATE 3		RATE 4	
		1ST	2ND	1ST	2ND	1ST	2ND	1ST	2ND
1	QM	0.665	0.665	0.000	0.000	0.000	0.000	0.000	0.000
2	TW	534	534	534	534	534	534	534	534
3	Ts	639.1	639.1	639.1	639.1	639.1	639.1	639.1	639.1
4	T	586.5	586.5	586.5	586.5	586.5	586.5	586.5	586.5
	PR (est)	3.22		0.00		0.00		0.00	
5	Z(est)	0.820	0.819	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
6	TZ	481.0	480.6	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
7	GH/TZ	13.323	13.336	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
8	eS	1.648	1.649	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
9	I-e-S	0.393	0.394	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
10	Pt	2173.2	2173.2	0.0	0.0	0.0	0.0	0.0	0.0
11	Pt2 /1000	4722.8	4722.8	0.0	0.0	0.0	0.0	0.0	0.0
12	Fr	0.0070195	0.0070195	0.0070195	0.0070195	0.0070195	0.0070195	0.0070195	0.0070195
13	Fc=FrTZ	3.376	3.373	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
14	FcQm	2.25	2.24	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
15	L/H(FcQm)2	5.0	5.0	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
16	Fw	1.9825183	1.9802354	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
17	Pw2	4724.8	4724.8	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
18	Ps2	7786.9	7790.6	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
19	Ps	2790.5	2791.2	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
20	P	2481.9	2482.2	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
21	Pr	3.68	3.68	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
22	Tr	1.64	1.64	1.64	1.64	1.64	1.64	1.64	1.64
23	Z	0.819	0.819	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!

FORM C122-D