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appropriate district office.
See Rule 401 & Rule 1122

State of New Mexico
Energy Minerals and Natural Resources
Oil Conservation Division
2040 South Pacheco
Santa Fe, NM 87505

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Form C-122
Revised October, 1999

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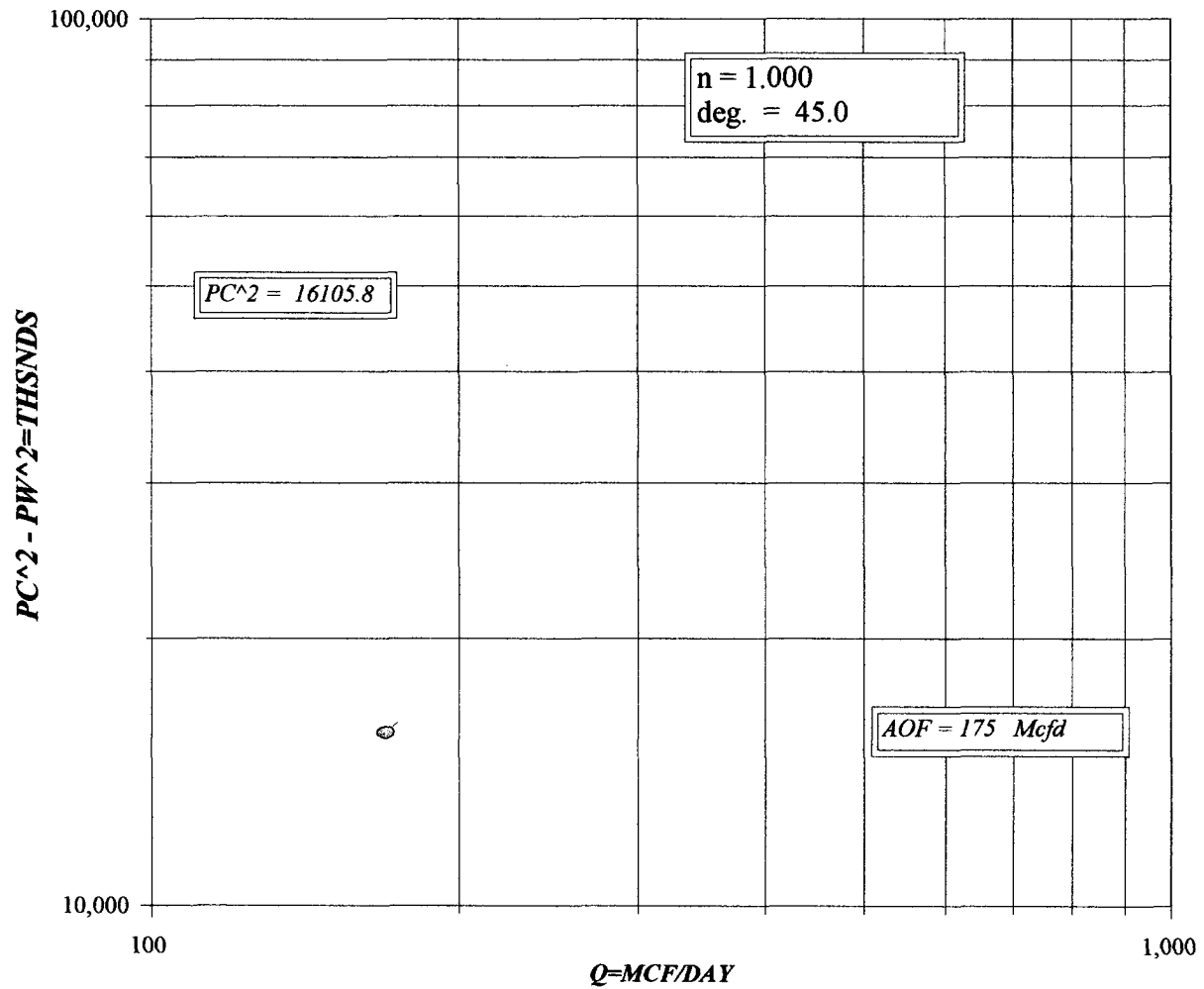
ODD-ANTEGIA

30-015-33580

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Operator MEWBOURNE OIL					Lease or Unit Name JUSTICE FED COM							
Type Test ☒ Initial ☐ Annual ☐ Special							Test Date 9/09/04		Well No. 1			
Completion Date 9/9/2004			Total Depth 11870			Plug Back TD 11740			Elevation 3194 GL		Unit Ltr - Sec - TWP - Rge C 1 21S 27E	
Csg. Size 5 1/2		Wt. 17		d 4.8		Set At 11870		Perforations: From: 11386 To: 11490		County EDDY		
Tbg. Size 2 7/8		Wt. 6.5		d 2.441		Set At 11133		Perforations: From: 11997 To: 12196		Pool BURTON FLAT		
Type Well-Single-Bradenhead-G.G. or G.O. Multiple SINGLE							Packer Set At 11114			Formation MORROW		
Producing Thru TUBING			Reservoir Temp. 181		Mean Annual Temp. 60		Baro. Press.-P _a 13.2			Connection SALES		
L 11133		H 11133		Gg 0.617		%CO ₂ 3.224		%N ₂ 1.08		%H ₂ S N/A		
				Prover N/A		Meter Run 3.067		Taps FLG				
FLOW DATA						TUBING DATA			CASING DATA			
No.	Prover Line Size	Orifice x Size	Press p.s.i.g.	Diff. h _w	Temp.	Press p.s.i.g.	Temp.	Press p.s.i.g.	Temp.	Duration of Flow		
SI						4013.2		PKR		24 HRS		
1	3 X	1.125	85	12	45	554		"		24 HRS		
2												
3												
4												
5												
RATE OF FLOW CALCULATIONS												
No.	COEFFICIENT (24 Hour)		$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress Factor F _{pv}	Rate of Flow Q, Mcfd				
1								170				
2												
3	TOTAL		FLOW	METER								
4												
5												
No.	P _r	Temp. R	T _r	Z	Gas Liquid Hydrocarbon Ratio DRY GAS Mcf bbl.							
1					A.P. I. Gravity of Liquid Hydrocarbons DRY Deg.							
2	TOTAL	FLOW	METER		Specific Gravity Separator Gas 0.617 XXXXXXXX							
3					Specific Gravity Flowing Fluid XXXXX N/A							
4					Critical Pressure 682 P.S.I.A. N/A P.S.I.A.							
5					Critical Temperature 350 R. N/A R							
P _c 4013.2 P _{c2} 16105.8					(1) $P_c^2 = 1.028$ $\frac{P_c^2 - P_w^2}{P_c^2 - P_w^2}$ AOF = Q (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.028$ $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 0.175$							
No.	P _t ²	P _w	P _w ²	P _c ² - P _w ²								
1		567.5	322.1	15673.7								
2												
3												
4												
Absolute Open Flow 2.286 Mcfd @ 15.025 Angle of Slope (°) 45 Slope, n 1.000												
Remarks: NO LIQUID MADE DURING TEST.												
Approved By Division:				Conducted By: MEWBOURNE OIL				Calculated By: MERV BUECKER				
								Checked By: BM				

MEWBOURNE OIL
JUSTICE FED COM #1



COMPANY : MEWBOUF OIL		LEASE : JUSTIFIED.COM		WELL NO. : 1		Pc = 4013.2		Pc2 = 16105.8	
UNIT : C		SECTION : 1		TOWNSHIP : 21					
L : 11133		H : 11133		L/H : 1		G/GMIX : 0.617		Pt2 = 321.7	
%CO2 : 3.224		%N2 : 1.083		H2S : 0.0		DATE : 9-9-04		Pw = 567.5	
d : 2.441		Fr : 0.010763		GH : 6869.1		RANGE : 27		0.0	
								0.0	
								0.0	
VOL 1 : 170		PSIA 1 : 567.2		RESV.TEMP : 185.3		Pc2-Pw2 = 15673.7		Pw2 = 322.1	
VOL 2 :		PSIA 2 :				#DIV/0!		#DIV/0!	
VOL 3 :		PSIA 3 :		SHUT-IN PR = 4013.2		#DIV/0!		#DIV/0!	
VOL 4 :		PSIA 4 :				#DIV/0!		#DIV/0!	
		PCR : 682				n = 1.000			
		TCR : 350							
LINE		RATE 1		RATE 2		RATE 3		RATE 4	
		1ST		2ND		1ST		2ND	
1	QM	0.170	0.170	0.000	0.000	0.000	0.000	0.000	0.000
2	TW	534	534	534	534	534	534	534	534
3	Ts	645.3	645.3	645.3	645.3	645.3	645.3	645.3	645.3
4	T	589.7	589.7	589.7	589.7	589.7	589.7	589.7	589.7
	PR (est)	0.83	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5	Z(est)	0.923	0.916	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
6	TZ	544.2	540.4	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
7	GH/TZ	12.622	12.712	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
8	eS	1.605	1.611	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
9	I-e-S	0.377	0.379	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
10	Pt	567.2	567.2	0.0	0.0	0.0	0.0	0.0	0.0
11	Pt2 /1000	321.7	321.7	0.0	0.0	0.0	0.0	0.0	0.0
12	Fr	0.010763	0.010763	0.010763	0.010763	0.010763	0.010763	0.010763	0.010763
13	Fc=FrTZ	5.857	5.816	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
14	FcQm	1.00	0.99	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
15	L/H(FcQm)	1.0	1.0	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
16	Fw	0.373867	0.370671	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
17	Pw2	322.1	322.1	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
18	Ps2	517.1	518.8	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
19	Ps	719.1	720.3	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
20	P	643.1	643.7	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
21	Pr	0.94	0.94	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
22	Tr	1.68	1.68	1.68	1.68	1.68	1.68	1.68	1.68
23	Z	0.916	0.916	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
								FORM C122-D	