| A | | | NTERIOR REC'D: 6/04/20 | 120 | FORM APPROVED OMB NO. 1004-0137 Expires: January 31, 2018 |
|--|---|---|---|--|--|
| | SUNDRY | UREAU OF LAND MANA NOTICES AND REPO | RTS ON WELLS | 5. Lease Se NMNM | rial No. |
| Do aba | not use the ndoned we | is form for proposals to II. Use form 3160-3 (AP | drill or to re-enter an D) for such proposals. | 6. If Indian | , Allottee or Tribe Name |
| 1997 | SUBMIT IN | TRIPLICATE - Other ins | tructions on page 2 | | r CA/Agreement, Name and/or No. 70965X |
| 1. Type of Well | | | | 8. Well Nan | ne and No. RANCH UNIT DI 1A BS3-7E 218H |
| 2. Name of Operator | s Well Oth | | KELLY KARDOS | 9. API Wel | ENNIS 904H |
| XTO PERMIAN C | PERATING | | os@xtoenergy.com | 30-015 | -45617 |
| 3a. Address 6401 HOLIDAY H MIDLAND, TX 79 | 9707 | | 3b. Phone No. (include area code) Ph: 432-620-4374 | WILDC LOS M | nd Pool or Exploratory Area AT BONE SPRING EDANOS WOLFCAMP |
| | - | C., R., M., or Survey Description | | | or Parish, State |
| Sec 21 T22S R30 |)E Mer NMP | SENW 1480FNL 2560F | ₩L1608FNL 2575FEL | EDDY | COUNTY, NM |
| 12. CHE | CK THE AI | PPROPRIATE BOX(ES) | TO INDICATE NATURE O | F NOTICE, REPORT, | OR OTHER DATA |
| TYPE OF SUBMI | ISSION | | TYPE OF | ACTION | |
| Notice of Intent | | □ Acidize | Deepen | Production (Start/Re | esume) 🔲 Water Shut-Off |
| | | □ Alter Casing | Hydraulic Fracturing | □ Reclamation | U Well Integrity |
| □ Subsequent Repo | ort | Casing Repair | □ New Construction | □ Recomplete | Other Change to Original A |
| □ Final Abandonm | ent Notice | □ Change Plans | □ Plug and Abandon | Temporarily Abando | on PD |
| | | Convert to Injection | □ Plug Back | □ Water Disposal | |
| testing has been comp determined that the sit | leted. Final Alter is ready for f | bandonment Notices must be fi inal inspection. | sults in a multiple completion or reco led only after all requirements, includ nake the following changes to | ing reclamation, have been o | |
| | | | | | |
| | design per t | he attached drilling prog | am. | | |
| Casing & cement | • . | | ram. E 218H to <mark>James Ranch Unit</mark> E | 01 1A Ennis 904H. | |
| Casing & cement Change name from | m James Ra | | 218H to James Ranch Unit I | 0I 1A Ennis 904H. | |
| Casing & cement Change name from Change the formation | m James Ra ation from W | anch Unit DI 1A BS3E-7E ildcat Bone Spring to Los | 218H to James Ranch Unit I | | |
| Casing & cement Change name from Change the forma Change SHL from Change BHL from | m James Ra ation from W 1480FNL & 1990FSL & | anch Unit DI 1A BS3E-7E ildcat Bone Spring to Los 2560FWL to 1608FNL | 218H to James Ranch Unit L Medanos Wolfcamp. 2575FEL. No Surface Distu 590FWL | | |
| Casing & cement Change name from Change the format Change SHL from Change BHL from Sarface | m James Ra ation from W 1480FNL & 990FSL & Soci | anch Unit DI 1A BS3E-7E ildcat Bone Spring to Los 2560FWL to 1608FNL 2440FWL to 990FSL & 2 6-3-20 Sol | E 218H to James Ranch Unit E s Medanos Wolfcamp. & 2575FEL. No Surface Distu 590FWL ne COA'S SR | bance | |
| Casing & cement Change name from Change the forma Change SHL from Change BHL from Sar face PLIO2120 - AN | m James Ra ation from W 1480FNL & 990FSL & <i>3000</i> | anch Unit DI 1A BS3E-7E ildcat Bone Spring to Los 2560FWL to 1608FNL \sim 2440FWL to 990FSL & 2 6 - 3 - 20 Say 240 Say | 218H to James Ranch Unit L Medanos Wolfcamp. 2575FEL. No Surface Distu 590FWL | bance | sting attached. |
| Casing & cement Change name from Change the format Change SHL from Change BHL from Sarface | m James Ra ation from W 1480FNL & 990FSL & <i>3000</i> | anch Unit DI 1A BS3E-7E ildcat Bone Spring to Los 2560FWL to 1608FNL $=$ 2440FWL to 990FSL & 2 6 - 3 - 20 Sav Homosoft Add true and forfect. Electronic Submission # For XTO PERMI | E 218H to James Ranch Unit E s Medanos Wolfcamp. & 2575FEL. No Surface Distur 590FWL me COA'S SR <u>chanal COAs Mgan</u> 516025 verified by the BLM Wel AN OPERATING LLC, sent to ti | bance ding Shell He Information System te Carlsbad | <u>Sting attached</u> . |
| Casing & cement Change name from Change the forma Change SHL from Change BHL from Sar face PLIO2120 - AN | m James Ra ation from W 1480FNL & 990FSL & 990FSL & All O he foregoing is | anch Unit DI 1A BS3E-7E ildcat Bone Spring to Los 2560FWL to 1608FNL 2440FWL to 990FSL & 2 6-3-20 Sav Hore and forect Electronic Submission # For XTO PERMI Committed to AFMSS for | E 218H to James Ranch Unit E s Medanos Wolfcamp. & 2575FEL. No Surface Distu 590FWL me COA'S SR <u>chanal COAs Myan</u> 516025 verified by the BLM Wel AN OPERATING LLC, sent to th r processing by PRISCILLA PEI | bance ding Shell He Information System te Carlsbad | |
| Casing & cement Change name from Change the forma Change SHL from Change BHL from Sarface <u>PLIOLIDE - AN</u> 14. Thereby certify that t | m James Ra ation from W 1480FNL & 990FSL & 990FSL & All O he foregoing is | anch Unit DI 1A BS3E-7E ildcat Bone Spring to Los 2560FWL to 1608FNL 2440FWL to 990FSL & 2 6-3-20 Sav Ho Add true and optect Electronic Submission # For XTO PERMI Committed to AFMSS for ARDOS | E 218H to James Ranch Unit E s Medanos Wolfcamp. & 2575FEL. No Surface Distu 590FWL me COA'S SR <u>chanal COAs Myan</u> 516025 verified by the BLM Wel AN OPERATING LLC, sent to th r processing by PRISCILLA PEI | bance Linformation System Te Carlsbad REZ on 05/21/2020 () ATORY COORDINATO | |
| Casing & cement Change name from Change the forma Change SHL from Change BHL from Sarface OLIOLICO - AN 14. Thereby certify that the Name (<i>Printed/Typed</i>) | m James Ra ation from W 1480FNL & 990FSL & 2 411 O he foregoing is KELLY KA | anch Unit DI 1A BS3E-7E ildcat Bone Spring to Los 2560FWL to 1608FNL a 2440FWL to 990FSL & 2 6 - 3 - 20 Sov 40 Sov 40 Submission # For XTO PERMI Committed to AFMSS for RDOS | 218H to James Ranch Unit E s Medanos Wolfcamp. & 2575FEL. No Surface Distur 590FWL me COA'S SR <u>chonal COAs Mann</u> 516025 verified by the BLM Wel AN OPERATING LLC, sent to th r processing by PRISCILLA PEI Title REGUL | bance <u>Shell Ha</u> Information System The Carlsbad REZ on 05/21/2020 () ATORY COORDINATO 020 | |
| Casing & cement Change name from Change the forma Change SHL from Change BHL from Sarface OLIOLICO - AN 14. Thereby certify that the Name (<i>Printed/Typed</i>) | m James Ra ation from W 1480FNL & 990FSL & 2 411 O he foregoing is KELLY KA | anch Unit DI 1A BS3E-7E ildcat Bone Spring to Los 2560FWL to 1608FNL a 2440FWL to 990FSL & 2 6 - 3 - 20 Sov 40 Sov 40 Submission # For XTO PERMI Committed to AFMSS for RDOS | 218H to James Ranch Unit I s Medanos Wolfcamp. & 2575FEL. No Surface Distur 590FWL me COA'S SR <u>chanol COAs regan</u> 516025 verified by the BLM Wel AN OPERATING LLC, sent to th r processing by PRISCILLA PEI Title REGUL/ Date 05/20/20 | bance ding Shell Ha Information System the Carlsbad REZ on 05/21/2020 () ATORY COORDINATO D20 DFFICE USE | DR UZJUN |
| Casing & cement Change name from Change the forma Change SHL from Change BHL from Sarface Octo2120 - AN 14. Thereby certify that t Name (Printed/Typed) Signature | m James Ra ation from W 1480FNL & 990FSL & 411 O he foregoing is KELLY KA (Electronic S | anch Unit DI 1A BS3E-7E ildcat Bone Spring to Los 2560FWL to 1608FNL of 2440FWL to 990FSL & 2 6-3-20 Say 100 100 100 100 100 100 100 10 | 218H to James Ranch Unit I s Medanos Wolfcamp. & 2575FEL. No Surface Distur 590FWL me COA'S SR <u>chonal COAs Manager</u> 516025 verified by the BEM Wel AN OPERATING LLC, sent to th r processing by PRISCILLA PEI Title REGUL Date 05/20/20 OR FEDERAL OR STATE C | bance <u>Shell Ha</u> Information System The Carlsbad REZ on 05/21/2020 () ATORY COORDINATO 020 | DR DR Date |
| Casing & cement Change name from Change the forma Change SHL from Change BHL from Sarface <u>Octo2120 - AN</u> 14. Thereby certify that t Name (<i>Printed/Typed</i>) Signature Approved By Conditions of approval, if a certify that the applicant ho which would entitle the app Title 18 U.S.C. Section 100 | m James Ra ation from W 1480FNL & 990FSL & <u>All O</u> he foregoing is KELLY KA (Electropic (Electropic solution) (Electropic) | anch Unit DI 1A BS3E-7E ildcat Bone Spring to Los 2560FWL to 1608FNL of 2440FWL to 990FSL & 2 6-3-20 Save 40 Save Add true and offect. Electronic Submission # For XTO PERMI Committed to AFMSS for RDOS ubmission) THIS SPACE FO d. Approval of this notice does hitable title to those rights in the tot operations thereon. U.S.C. Section 1212, make it a | 218H to James Ranch Unit I Medanos Wolfcamp. 2575FEL. No Surface Distur- 590FWL Me COA'S SR <u>Anol Cons regar</u> 516025 verified by the BLM Wel AN OPERATING LLC, sent to th r processing by PRISCILLA PER Title REGULA Date 05/20/20 OR FEDERAL OR STATE O Title AFM | bance ding Shell Ha Information System The Carlsbad REZ on 05/21/2020 () ATORY COORDINATO D20 DFFICE USE - PESOUPCE MMPG 2000 | DR B Date Date Date |

100

Additional data for EC transaction #516025 that would not fit on the form

32. Additional remarks, continued

XTO requests the following variances:

Approval to utilize a spudder rig to pre-set surface casing per the attached Description of Operations.

Batch drill this well if necessary. In doing so, XTO will set each casing string and ensure that the well is cemented properly and the well is static. With floats holding, no pressure on the csg annulus, and the installation of a 10K TA cap as per GE recommendations, XTO will contact the BLM to skid the rig to drill the remaining wells on the pad. Once surface and intermediate strings are all completed, XTO will begin drilling the production hole on each of the wells.

ONLY test broken pressure seals on the BOP equipment per the attached procedure.

Attachments: C102 & Supplement Casing/Cement Design Multibowl Diagram Directional Plan Spudder Rig Description of Operations BOP Variance Procedure

Conditions of Approval James Ranch Unit DI 1A Ennis 904H 30-015-45617

BOP Break Testing Variance (Note: Shell testing is not approved for any portion of the hole with a MASP of 5000 psi or greater)

- While in transfer between wells, the BOPE shall be secured by the hydraulic carrier or cradle.
- Any well control event while drilling require notification to the BLM Petroleum
- Engineer prior to the commencement of any BOP Break Testing operations.

A full BOP test is required prior to drilling the first deep intermediate hole section. If any subsequent hole interval is deeper than the first, a full BOP test will be required.

District I

1625 N. French Dr., Hobbs, NM 88240 Phone: (575) 393-6161 Fax: (575) 393-0720 District II 811 S. First St., Artesia, NM 88210 Phone: (575) 748-1283 Fax: (575) 748-9720 District III 1000 Rio Brazos Road, Aztec, NM 87410 Phone: (505) 334-6178 Fax: (505) 334-6170 District IV 1220 S. St. Francis Dr., Santa Fe, NM 87505 Phone: (505) 476-3460 Fax: (505) 476-3462

State of New Mexico Energy, Minerals & Natural Resources Department **OIL CONSERVATION DIVISION** 1220 South St. Francis Dr. Santa Fe, NM 87505

EMNRD-OCD ARTESIA

Form C-102

REC'D: 6/04/2020 Revised August 1, 2011 Submit one copy to appropriate

District Office

AMENDED REPORT

WELL LOCATION AND ACREAGE DEDICATION PLAT

| 1 | API Number | r | | ² Pool Code | | | ³ Pool Na | ³ Pool Name | | | | | | |
|--------------------------------------|-------------------------|--------------------------|-------------------|------------------------|---------------------------------------|-------------------------|----------------------|------------------------|----------------------------------|--|--|--|--|--|
| | 30-015- 4 | 15617 | 96597 | | LOS | LOS MEDANOS; WOLFCAMP | | | | | | | | |
| ⁴ Property 328259 | Code | | | JAM | ⁵ Property IES RANCH UI | Name NIT DI 1A ENNIS | | 6, | Well Number 904H | | | | | |
| ⁷ OGRID 37307 | | | | | | | | | ⁹ Elevation 3,160' | | | | | |
| | | | | • • • • • • • • • • | ¹⁰ Surface | Location | | | | | | | | |
| UL or lot no. | Section | Township | Range | Lot Idn | Feet from the | e North/South line | Feet from the | East/West line | County | | | | | |
| G | 21 | 22S | 30E | | 1,608 | NORTH | 2,575 | EAST | EDDY | | | | | |
| | | | ¹¹ Bot | tom Hole | e Location I | f Different From | n Surface | | | | | | | |
| UL or lot no. | Section | Township | Range | Lot Idn | Feet from the | e North/South line | Feet from the | East/West line | County | | | | | |
| Ν | 23 | 22S | 30E | | 990 | SOUTH | 2,590 | WEST | EDDY | | | | | |
| ¹² Dedicated Acres 320 | s ¹³ Joint o | r Infill ¹⁴ C | onsolidation (| Code ¹⁵ Ord | ier No. | | | | | | | | | |

No allowable will be assigned to this completion until all interests have been consolidated or a non-standard unit has been approved by the division.

| B SEC. 22 SEC. 123 C 2,575 ⁺ CRD A2 = 167:17'57 ⁺ CRD A2 = 80'5'3'1 ⁺ SEC. 24 FHORZ. DIST.=2,745.53 ⁺ CRD A2 = 80'5'3'1 ⁺ SEC. 24 SEC. 21 FT.P. CRD A2 = 167'17'57 ⁺ CRD A2 = 80'5'3'1 ⁺ SEC. SEC. 21 FT.P. CRD A2 = 80'5'3'1 ⁺ SEC. SEC. SEC. 23 G SEC. | 16 | SEC. 16 | | SEC. T22S | 15 R30E | | SEC. | 14 | SEC. 13 | 17 OPERATOR CERTIFICATION I hereby certify that the information contained herein is true and complete |
|--|-------------|--|---------|-------------------------------------|--------------------|---------------------------------|------------|---------------------------|---|---|
| CRID AZ,=167/17/57' CRID AZ,=467/17/57' CRID AZ,=467/17/57' SEC. SEC. 21 F,T,P, F,T,P,P, F,T,P,P,P,P,P,P,P,P,P,P,P,P,P,P,P,P,P,P, | i 1 1 | ,800 ,S.H.L. | | | SEC. 22 | 1 | SEC. 2 | 3 | | |
| SEC. 21 F.T.P. C.S.BU. Sec. 23 Sec. 23 Sec. 27 Sec. 28 Sec. 27 Sec. 28 Sec. 27 Sec. 28 Sec. 28 Sec. 28 Sec. 27 Sec. 28 Sec. 28 Sec. 25 SHL (NAD23 NME) LTP (NAD23 NME) LTP (NAD27 NME) LTP (NAD27 NME) Sec. 28 Sec. 27 Sec. 28 Sec. 28 Sec. 28 Sec. 28 Sec. 28 Sec. 27 Sec. 28 Sec. 27 Sec. 28 Sec. 28 Sec. 29 Sec. 28 Sec. 29 Sec. 28 Sec. 29 Sec. 28 Sec. 29 Sec. 29 <td></td> <td>2,57</td> <td></td> <td>GRID AZ.=167 HORIZ. DIST.=2</td> <td>17'57" ,745.63'</td> <td></td> <td></td> <td></td> <td></td> <td>location pursuant to a contract with an owner of such a mineral or working</td> | | 2,57 | | GRID AZ.=167 HORIZ. DIST.=2 | 17'57" ,745.63' | | | | | location pursuant to a contract with an owner of such a mineral or working |
| SEC. 28 B SEC. 27 SEC. 26 SEC. 27 SEC. 28 SEC. 28 SEC. 25 SEC. 26 SEC. 27 23 27 23 27 23 27 23 27 23 27 23 27 | SEC. 2 | | .PH | | | | | | - <u>-</u> | Kelly Kardos 5-20-20 |
| SEC. 28 SEC. 27 SEC. 26 Printed Name SHL (NAD83 NME) LTP (NAD83 NME) SHL (NAD27 NME) SHL (NAD27 NME) Printed Name kelly_kardos@xtoenergy.com Y = 502,458.6 Y = 499,798.8 Y = 502,397.9 Y = 499,738.2 Y = 648,732.3 LAT. = 32.370368 'N LAT. = 32.37041 'N <td< td=""><td>i</td><td></td><td>80'-</td><td> </td><td></td><td></td><td>V 1</td><td>-</td><td></td><td></td></td<> | i | | 80'- | | | | V 1 | - | | |
| SHL (NADDS NME) LIP (NADDZ NME) LIP (NADDZ NME) LIP (NADDZ NME) Y = 502,458.6 Y = 499,798.8 Y = 502,458.6 Y = 499,788.2 X = 679,450.4 X = 689,914.0 X = 638,268.8 X = 648,732.3 LAT. = 32.30308 *N LAT. = 32.373098 *N LAT. = 32.373098 *N LAT. = 32.372975 *N LONG. = 103.852079 *W LONG. = 103.85404 *W LONG. = 103.85168 *W I*SURVEYOR CERTIFICATION Y = 499,780.2 Y = 499,798.9 Y = 499,719.5 Y = 499,738.3 X = 648,782.3 X = 680,054.0 X = 638,964.0 X = 638,872.3 X = 648,782.3 I hereby certify that the well location shown on this LONG. = 103.884016 *W LONG. = 103.8851917 *W LONG. = 103.885192 *W LONG. = 103.885192 *W LONG. = 103.885142 *W CORNER COORDINATES (NAD83 NME) CORNER COORDINATES (NAD27 NME) A - Y = 498,733.7 N X = 643,522.1 R Mathefees A - Y = 498,793.4 N X = 663,037.5 E B - Y = 498,737.2 N X = 643,522.8 E O Y = 498,737.2 N X = 643,522.8 E O Y = 498,737.2 N X = 643,522.8 E Signatue and Seal of Professional Surveyor: O 21-0220 D - Y = 498,804.6 N X = 669,737.3 F E C - Y = 498,737.4 N X = 6638,747.5 N | SEC. | | ľ | SEC. | 27 | SEC. 2 | 26 006 000 | 200 | | |
| $ \begin{array}{c} Y = 502,458.6 & Y = 499,798.8 & Y = 502,397.9 & Y = 499,738.2 \\ X = 679,450.4 & X = 689,914.0 & X = 638,368.8 & X = 648,732.3 \\ LAT = 32.380534 *N & LAT = 32.373098 *N & LAT = 32.386440 *W & LONG = 103.851586 *W \\ IONG = 103.852079 *W & LONG = 103.852079 *W & LONG = 103.852079 *W \\ IONG = 103.852079 *W & LONG = 103.852079 *W & LONG = 103.851586 *W \\ Y = 499,798.0.2 & Y = 499,798.9 & Y = 499,719.5 & Y = 499,738.3 \\ X = 680,054.0 & X = 689,964.0 & X = 638,967.2 & X = 648,782.3 \\ LAT = 32.373058 *N & LAT = 32.373088 *N & LAT = 32.373041 *N & LAT = 32.372975 *N \\ LONG = 103.884015 *W & LONG = 103.851917 *W & LONG = 103.85322 *W & LONG = 103.851424 *W \\ \hline & CORNER COORDINATES (NADB3 NME) & CORNER COORDINATES (NADB3 NME) \\ A - Y = 498,793.8 N & X = 668,737.5 E & A - Y = 498,732.7 N & X = 648,872.2 8 E \\ D - Y = 498,797.8 N & X = 668,737.5 E & A - Y = 498,732.7 N & X = 643,522.8 E \\ D - Y = 498,797.8 N & X = 668,737.7 E & D - Y = 498,737.2 N & X = 643,522.8 E \\ D - Y = 498,809.0 N & X = 669,051.3 E & E - Y = 498,737.2 N & X = 643,522.8 E \\ D - Y = 498,809.0 N & X = 669,051.3 E & E - Y = 498,737.2 N & X = 643,522.8 E \\ D - Y = 498,809.0 N & X = 669,051.3 E & E - Y = 498,737.2 N & X = 648,669.7 E \\ F - Y = 498,809.0 N & X = 669,051.3 E & E - Y = 498,748.5 N & X = 648,669.7 E \\ F - Y = 498,809.0 N & X = 669,051.3 E & E - Y = 498,748.5 N & X = 648,669.7 E \\ F - Y = 498,809.0 N & X = 669,051.3 E & E - Y = 498,748.5 N & X = 648,669.7 E \\ F - Y = 498,809.0 N & X = 669,051.3 E & E - Y = 498,748.5 N & X = 648,669.7 E \\ F - Y = 498,809.0 N & X = 669,051.3 E & E - Y = 498,748.5 N & X = 648,669.7 E \\ F - Y = 500,111.7 N & X = 682,032.9 E & H - Y = 500,065.0 N & X = 643,521.1 E \\ I - Y = 500,117.1 N & X = 688,774.1 E & J - Y = 500,065.2 N & X = 648,870.9 E \\ MARK DILLON HARP 2376 & MARK $ | SHI (| NAD83 NMF) | | AD83 NME) | SHL (NAD2 | 7 NME) | | ITP (NAD27) | | |
| $ \begin{array}{c} X = 679,450.4 & X = 689,914.0 & X = 632,268.8 & X = 648,732.3 \\ LAT. = 32.380534 *N & LAT. = 32.373098 *N & LAT. = 32.380411 *N & LAT. = 32.372975 *N \\ LONG. = 103.8853935 *W & LONG. = 103.85279 *W & LONG. = 103.88540 *W & LONG. = 103.88586 *W \\ \hline \end{tabular} FTP (NAD33 NME) & FTP (NAD27 NME) & BHL (NAD27 NME) \\ Y = 499,780.2 & Y = 499,798.9 & Y = 499,715.5 & Y = 499,738.3 \\ X = 680,054.0 & X = 689,964.0 & X = 638,872.3 & X = 648,782.3 \\ LAT. = 32.373165 *N & LAT. = 32.373098 *N & LAT. = 32.373041 *N & LAT. = 32.372975 *N \\ LONG. = 103.884016 *W & LONG. = 103.881016 *W & LONG. = 103.881542 *W & CORRECOORDINATES (NAD27 NME) \\ \hline \end{tabular} OCRNER COORDINATES (NAD33 NME) & CORRECOORDINATES (NAD27 NME) \\ \hline \end{tabular} OCRNER COORDINATES (NAD33 NME) & CORRECOORDINATES (NAD27 NME) \\ \hline \end{tabular} OCRNER COORDINATES (NAD33 NME) & CORRECOORDINATES (NAD27 NME) \\ \hline \end{tabular} OCRNER COORDINATES (NAD33 NME) & CORRECOORDINATES (NAD27 NME) \\ \hline \end{tabular} OCRNER COORDINATES (NAD33 NME) & CORRECOORDINATES (NAD27 NME) \\ \hline \end{tabular} OCRNER COORDINATES (NAD33 NME) & CORRECOORDINATES (NAD27 NME) \\ \hline \end{tabular} OCRNER COORDINATES (NAD33 NME) & CORRECOORDINATES (NAD37 NME) & ORNE COORDINATES (NAD37 NME) & ORNE C$ | | on an office and an other course . | | | | | | | | E-mail Address |
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| LONG. = 103.8520/3 *W LONG. = 103.8510/3 *W LONG. = 103.8510/3 *W PTP (NAD27 NME) BHL (NAD27 NME) I hereby certify that the well location shown on this Y = 499,780.2 Y = 499,798.9 Y = 499,719.5 Y = 499,738.3 X = 648,782.3 X = 648,782.3 X = 648,782.3 X = 648,782.3 N data N data thereby certify that the well location shown on this plat was plotted from field notes of actual surveys made by me or under my supervision, and that the same is true and correct to the best of my belief. 04-21-2020 Date of Survey 04-21-2020 Date of Survey Signatue and Seal of Professional Surveyor: 23786 Y 23786 Y 23786 Y 23786 Y 23786 Y Y Y Y Y Y Y Y Y Y Y Y Y Y Y Y Y | LAT. = | 32.380534 °N | LAT. = | 32.373098 °N | LAT. = 32 | .380411 °N | LA | T. = 32.3729 | 75 °N | 18 SUDVEVOD CEDTIEICATION |
| $\begin{array}{c c c c c c c c c c c c c c c c c c c $ | LONG. = | 103.885935 °W | LONG. = | 103.852079 °W | LONG. = 103 | .885440 °W | LON | G. = 103.8515 | 86 °W | |
| $ \begin{array}{cccccccccccccccccccccccccccccccccccc$ | FTP (I | NAD83 NME) | BHL (M | NAD83 NME) | FTP (NAD2 | 7 NME) | | BHL (NAD27 | NME) | I hereby certify that the well location shown on this |
| LAT. = 32.373165 *N LAT. = 32.373098 *N LAT. = 32.373041 *N LAT. = 32.372975 *N LONG. = 103.851917 *W LONG. = 103.851917 *W LONG. = 103.83522 *W LONG. = 103.851424 *W CORNER COORDINATES (NAD27 NME) A - Y = $498,789.0$ N, X = $679,354.8$ E A - Y = $498,728.3$ N, X = $638,173.1$ E B - Y = $498,793.4$ N, X = $682,037.5$ E B - Y = $498,737.2$ N, X = $640,855.8$ E C - Y = $498,797.8$ N, X = $684,704.4$ E C - Y = $498,737.2$ N, X = $640,855.8$ E D - Y = $498,804.6$ N, X = $687,373.7$ E D - Y = $498,744.1$ N, X = $646,192.0$ E E - Y = $498,804.6$ N, X = $690,051.3$ E E - Y = $498,748.5$ N, X = $643,669.7$ E F - Y = $498,748.5$ N, X = $643,869.7$ E F - Y = $498,748.5$ N, X = $643,869.7$ E F - Y = $498,748.5$ N, X = $643,869.7$ E F - Y = $498,748.5$ N, X = $643,869.7$ E F - Y = $498,748.5$ N, X = $643,869.7$ E F - Y = $498,748.5$ N, X = $643,869.7$ E F - Y = $498,748.5$ N, X = $643,869.7$ E F - Y = $498,748.5$ N, X = $643,869.7$ E F - Y = $498,748.5$ N, X = $643,869.7$ E F - Y = $498,748.5$ N, X = $643,869.7$ E F - Y = $500,011.7$ N, X = $682,032.9$ E H - Y = $500,051.0$ N, X = $643,851.2$ E F - Y = $498,748.5$ N, X = $643,869.7$ E F - Y = $500,011.7$ N, X = $684,702.7$ E I - Y = $500,056.5$ N, X = $643,521.1$ E J - Y = $500,052.0$ N, X = $643,521.1$ E J - Y = $500,052.6$ N, X = $643,521.1$ E J - Y = $500,052.6$ N, X = $643,521.1$ E K - Y = $500,052.6$ N, X = $643,521.1$ E K - Y = $500,052.6$ E K - Y = $500,063.2$ N, X = $643,870.9$ E MARK DILLON HARP 23786 | Y = | 499,780.2 | Y = | 499,798.9 | Y = 49 | 9,719.5 | | Y = 499,738 | .3 | plat was plotted from field notes of actual surveys |
| LA1. = 32.37305 N LA1. = 32.37305 N LA1. = 32.37305 N LA1. = 32.37305 N LA1. = 32.37304 N LA1. = S2.37304 N <td< td=""><td>X =</td><td>680,054.0</td><td>X =</td><td>689,964.0</td><td>X = 63</td><td>38,872.3</td><td></td><td>X = 648,782</td><td>.3</td><td></td></td<> | X = | 680,054.0 | X = | 689,964.0 | X = 63 | 38,872.3 | | X = 648,782 | .3 | |
| CORNER COORDINATES (NAD23 NME)CORNER COORDINATES (NAD27 NME) $A - Y = 498,789.0 N$ $X = 679,354.8 E$ $A - Y = 498,728.3 N$ $X = 638,173.1 E$ $B - Y = 498,793.4 N$ $X = 682,037.5 E$ $B - Y = 498,728.3 N$ $X = 638,173.1 E$ $C - Y = 498,797.8 N$ $X = 682,037.5 E$ $B - Y = 498,737.2 N$ $X = 640,855.8 E$ $C - Y = 498,804.6 N$ $X = 687,373.7 E$ $D - Y = 498,748.5 N$ $X = 643,522.8 E$ $D - Y = 498,809.0 N$ $X = 690,051.3 E$ $E - Y = 498,748.5 N$ $X = 643,659.7 E$ $F - Y = 498,814.5 N$ $X = 692,729.2 E$ $F - Y = 498,748.5 N$ $X = 633,169.7 E$ $G - Y = 500,108.0 N$ $X = 679,351.4 E$ $G - Y = 500,051.0 N$ $X = 633,169.7 E$ $H - Y = 500,111.7 N$ $X = 682,032.9 E$ $H - Y = 500,051.0 N$ $X = 643,521.1 E$ $J - Y = 500,112.7 N$ $X = 687,374.1 E$ $J - Y = 500,063.2 N$ $X = 643,870.9 E$ $K - Y = 500,128.8 N$ $X = 690,052.6 E$ $K - Y = 500,068.3 N$ $X = 648,870.9 E$ | LAT. = | 32.373165 °N | | | | | | | | made by me or under my supervision, and that the |
| E - Y = 498,809.0 N , X = 690,051.3 E E - Y = 498,748.5 N , X = 648,869.7 E F - Y = 498,814.5 N , X = 692,729.2 E F - Y = 498,754.0 N , X = 651,547.5 E G - Y = 500,108.0 N , X = 679,351.4 E G - Y = 500,047.2 N , X = 638,169.7 E H - Y = 500,111.7 N , X = 682,032.9 E H - Y = 500,051.0 N , X = 640,851.2 E I - Y = 500,117.1 N , X = 684,702.7 E I - Y = 500,056.5 N , X = 643,521.1 E J - Y = 500,123.7 N , X = 687,374.1 E J - Y = 500,063.2 N , X = 646,192.4 E K - Y = 500,128.8 N , X = 690,052.6 E K - Y = 500,068.3 N , X = 648,870.9 E MARK DILLON HARP 23786 | LONG. = | 103.884016 °W | LONG. = | 103.851917 °W | LONG. = 103 | .883522 °W | LON | G. = 103.8514 | 24 °W | same is true and correct to the best of my belief. |
| E - Y = 498,809.0 N , X = 690,051.3 E E - Y = 498,748.5 N , X = 648,869.7 E F - Y = 498,814.5 N , X = 692,729.2 E F - Y = 498,754.0 N , X = 651,547.5 E G - Y = 500,108.0 N , X = 679,351.4 E G - Y = 500,047.2 N , X = 638,169.7 E H - Y = 500,111.7 N , X = 682,032.9 E H - Y = 500,051.0 N , X = 640,851.2 E I - Y = 500,117.1 N , X = 684,702.7 E I - Y = 500,056.5 N , X = 643,521.1 E J - Y = 500,123.7 N , X = 687,374.1 E J - Y = 500,063.2 N , X = 646,192.4 E K - Y = 500,128.8 N , X = 690,052.6 E K - Y = 500,068.3 N , X = 648,870.9 E MARK DILLON HARP 23786 | | | | | | | RDINATES (| | | |
| E - Y = 498,809.0 N , X = 690,051.3 E E - Y = 498,748.5 N , X = 648,869.7 E F - Y = 498,814.5 N , X = 692,729.2 E F - Y = 498,754.0 N , X = 651,547.5 E G - Y = 500,108.0 N , X = 679,351.4 E G - Y = 500,047.2 N , X = 638,169.7 E H - Y = 500,111.7 N , X = 682,032.9 E H - Y = 500,051.0 N , X = 640,851.2 E I - Y = 500,117.1 N , X = 684,702.7 E I - Y = 500,056.5 N , X = 643,521.1 E J - Y = 500,123.7 N , X = 687,374.1 E J - Y = 500,063.2 N , X = 646,192.4 E K - Y = 500,128.8 N , X = 690,052.6 E K - Y = 500,068.3 N , X = 648,870.9 E MARK DILLON HARP 23786 | | | | | | | , | | | 04-21-2020 |
| E - Y = 498,809.0 N , X = 690,051.3 E E - Y = 498,748.5 N , X = 648,869.7 E F - Y = 498,814.5 N , X = 692,729.2 E F - Y = 498,754.0 N , X = 651,547.5 E G - Y = 500,108.0 N , X = 679,351.4 E G - Y = 500,047.2 N , X = 638,169.7 E H - Y = 500,111.7 N , X = 682,032.9 E H - Y = 500,051.0 N , X = 640,851.2 E I - Y = 500,117.1 N , X = 684,702.7 E I - Y = 500,056.5 N , X = 643,521.1 E J - Y = 500,123.7 N , X = 687,374.1 E J - Y = 500,063.2 N , X = 646,192.4 E K - Y = 500,128.8 N , X = 690,052.6 E K - Y = 500,068.3 N , X = 648,870.9 E MARK DILLON HARP 23786 | | | | | | | , | | | Date of Survey |
| E - Y = 498,809.0 N , X = 690,051.3 E E - Y = 498,748.5 N , X = 648,869.7 E F - Y = 498,814.5 N , X = 692,729.2 E F - Y = 498,754.0 N , X = 651,547.5 E G - Y = 500,108.0 N , X = 679,351.4 E G - Y = 500,047.2 N , X = 638,169.7 E H - Y = 500,111.7 N , X = 682,032.9 E H - Y = 500,051.0 N , X = 640,851.2 E I - Y = 500,117.1 N , X = 684,702.7 E I - Y = 500,056.5 N , X = 643,521.1 E J - Y = 500,123.7 N , X = 687,374.1 E J - Y = 500,063.2 N , X = 646,192.4 E K - Y = 500,128.8 N , X = 690,052.6 E K - Y = 500,068.3 N , X = 648,870.9 E MARK DILLON HARP 23786 | | | | | | | , | | | Signatue and Seal of |
| F - Y = 498,814.5 N , X = 630,713 E E - Y = 498,754.0 N , X = 640,603.1 E 23786 G - Y = 500,108.0 N , X = 651,547.5 E , X = 651,547.5 E , X = 631,617. E , X = 631,617. E , X = 631,617. E , X = 633,169.7 E , X = 633,169.7 E , X = 633,169.7 E , X = 640,851.2 E , X = , X = 640,851.2 E , X = , X = 643,521.1 E , X = , X = 643,521.1 E , X = , X = 643,521.1 E , X = , X = 646,192.4 E , X = , X = 646,192.4 E , X = , X = 648,870.9 E , X = , Mark Dillon Harp 23786 , Mark Dillon Harp 23786 , X = </td <td></td> <td>in the second second</td> <td></td> <td>and the second second second second</td> <td></td> <td></td> <td>,</td> <td>and the second states of</td> <td></td> <td></td> | | in the second | | and the second second second second | | | , | and the second states of | | |
| G - Y = 500,108.0 N X = 679,351.4 E G - Y = 500,047.2 N X = 638,169.7 E H - Y = 500,111.7 N X = 682,032.9 E H - Y = 500,051.0 N X = 640,851.2 E I - Y = 500,117.1 N X = 684,702.7 E I - Y = 500,056.5 N X = 643,521.1 E J - Y = 500,123.7 N X = 687,374.1 E J - Y = 500,063.2 N X = 646,192.4 E K - Y = 500,128.8 N X = 690,052.6 E K - Y = 500,068.3 N X = 648,870.9 E | | and the second | | a second Disaster second states of | | | , | Marine Contraction Marine | and the second | |
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| | | | | | | and a start of the start of the | | | NG FES | 5 |
| | | | X = | | | | , | | | NU YOA |
| | J - Y = | | X = | 687,374.1 E | J - Y = 50 | 0,063.2 N | , | X = 646,192 | .4 E | ESSIQUE CUR |
| L-Y = 500,134.4 N , X = 692,730.7 E L-Y = 500,073.9 N , X = 651,549.1 E Certificate Number LM 2020030722 | K - Y = | 500,128.8 N , | X = | 690,052.6 E | Ķ - Y = 50 | 0,068.3 N | , | X = 648,870 | .9 E | MARK DILLON HARP 23786 |
| | L - Y = | 500,134.4 N , | X = | 692,730.7 E | L-Y= 50 | 0,073.9 N | , | X = 651,549 | .1 E | Certificate Number LM 202003072 |

RWP 6/12/2020

P:\PROJECTS\2020\2020030722-XTO-JRU_DI_1A_ENNIS_904H-EDDY\DWG\2020030722-XTO-JAMES_RANCH_UNIT_DI_1A_ENNIS_904H_C-102_04-20-2020.dwg

| Intent × As Drilled | | |
|----------------------------|------------------------------|-------------|
| Operator Name: | Property Name: | Well Number |
| XTO PERMIAN OPERATING, LLC | JAMES RANCH UNIT DI 1A ENNIS | 904H |

Kick Off Point (KOP)

| UL G | Section 21 | Township 22S | Range 30E | Lot | Feet 1608 | From N/S NORTH | Feet 2575 | From E/W EAST | County EDDY |
|-------------|--------------------------|-----------------|--------------|-----|--------------|-------------------|--------------|------------------|----------------|
| Latitu 32.3 | ^{ude} 380534 | | | | Longitude | 5935 | | | NAD 83 |

First Take Point (FTP)

| UL | Section | Township | Range | Lot | Feet | From N/S | Feet | From E/W | County |
|-------------|--------------------------|----------|-------|-----|-----------|----------|------|----------|-----------|
| O | 21 | 22S | 30E | | 990 | SOUTH | 1980 | EAST | EDDY |
| Latitu 32.3 | ^{ide} 373165 | i | | | Longitude | 4016 | | | NAD 83 |

Last Take Point (LTP)

| UL | Section | Township | Range | Lot | Feet | From N/S | Feet | From E/W | County |
|-------------|--------------------------|----------|-------|-----|----------|-------------------------|------|----------|-----------|
| N | 23 | 22S | 30E | | 990 | SOUTH | 2540 | WEST | EDDY |
| Latitu 32.3 | ^{ide} 373098 | 3 | | | Longitur | ^{de} 852079 | | | NAD 83 |

Is this well the defining well for the Horizontal Spacing Unit?

Is this well an infill well?

Y

If infill is yes please provide API if available, Operator Name and well number for Defining well for Horizontal Spacing Unit.

| API # 30-015-45611 Operator Name: | | Property Name: | Well Number |
|---|--------------|------------------------------|---------------|
| XTO PERMIAN OPE | ERATING, LLC | JAMES RANCH UNIT DI 1A ENNIS | 115H |
| | | | KZ 06/29/2018 |

James Ranch Unit DI 1A Ennis 904H Projected TD: 20965' MD / 10656' TVD SHL: 1608' FNL & 2575' FEL , Section 21, T22S, R30E BHL: 990' FSL & 2590' FWL , Section 23, T22S, R30E Eddy County, NM

Casing Design

The surface fresh water sands will be protected by setting 16" inch casing @ 488' (25' above the salt) and circulating cement back to surface. The salt will be isolated by setting 11-3/4" inch casing at 3328' and circulating cement to surface. The second intermediate will isolate from the solt down to the next casing seat by setting 8-5/8" inch casing at 9883' and cemented 200' into the 11-3/4" inch casing. A 7-7/8" inch curve and lateral hole will be drilled to MD/TD and 5-1/2 inch casing will be set at TD and cemented back up to 2nd intermediate (estimated TOC 9383 feet) per Potash regulations.

| Hole Size | Depth | OD Csg | Weight | Collar | Grade | New/Used | SF Burst | SF Collapse | SF Tension |
|-----------|-------------|---------|--------|--------|---------|----------|----------|-------------|------------|
| 20" | 0' - 488' | 16" | 75 | втс | J-55 | New | 2.77 | 5.75 | 40.07 |
| 14-3/4" | 0' - 3328' | 11-3/4″ | 47 | втс | J-55 | New | 1.13 | 1.57 | 4.96 |
| 10-5/8″ | 0' - 9883' | 8-5/8″ | 32 | втс | HCL-80 | New | 1.10 | 1.38 | 2.17 |
| 7-7/8" | 0' - 20965' | 5-1/2″ | 20 | C7S | CYP-110 | New | 1.20 | 1.45 | 2.25 |

· XTO requests to not utilize centralizers in the curve and lateral

16" Collapse analyzed using 75% evacuation. Casing to be filled while running.

11-3/4" Collapse analyzed using 50% evacuation based on regional experience.

8-5/8" Collapse analyzed using 33% evacuation based on regional experience.

-5-1/2" Tension calculated using vertical hanging weight plus the lateral weight multiplied by a friction factor of 0.35 • Test on 2M Annular & Casing will be limited to 70% burst of the casing or 1500 psi, whichever is less

WELLHEAD:

Temporary Wellhead 16" SOW bottom x 16-3/4" 3M top flange

Permanent Wellhead – GE RSH Multibowl System A. Starting Head: 13-5/8" 10M top flange x 11-3/4" SOW bottom

B. Tubing Head: 13-5/8" 10M bottom flange x 7-1/16" 15M top flange

Wellhead will be installed by manufacturer's representatives. Manufacturer will monitor welding process to ensure appropriate temperature of seal.

Operator will test the 8-5/8" casing per BLM Onshore Order 2

Wellhead manufacturer representative may not be present for BOP test plug installation

Cement Program

Surface Casing:

Tail: 560 sxs Halcem-C + 2% CaCl (mixed at 14.8 ppg, 1.35 ft3/sx, 6.39 gal/sx water) Compressives: 12-hr = 900 psi 24 hr = 1500 psi

*Two additional 1" top out jobs will be attempted after the surface cement job. If the top of cement is not affected by the two top out jobs, ~10-20 ppb gravel will be added on the backside of the 1" to attempt to get cement to surface.

1st Intermediate Casing:

Lead: 1880 sxs EconoCem-HLTRRC (mixed at 12.9 ppg, 1.39 ft3/sx, 10.13 gal/sx water) Tail: 190 sxs Halcem-C + 2% CaCl (mixed at 14.8 ppg, 1.35 ft3/sx, 6.39 gal/sx water) Compressives: 12-hr = 900 psi 24 hr = 1500 psi

2nd Intermediate Casing: ECP/DV Tool to be set at 3428'

1st Stage:

Lead: 1180 sxs Halcem-C + 2% CaCl (mixed at 12.9 ppg, 2.11 ft3/sx, 9.61 gal/sx water) Tail: 170 sxs Halcem-C + 2% CaCl (mixed at 14.8 ppg, 1.2 ft3/sx, 6.39 gal/sx water) Compressives: 12-hr = 900 psi 24 hr = 1500 psi

2nd Stage:

Lead: 30 sxs Halcem-C + 2% CaCl (mixed at 12.9 ppg, 2.16 ft3/sx, 9.61 gal/sx water) Tail: 150 sxs Halcem-C + 2% CaCl (mixed at 14.8 ppg, 1.33 ft3/sx, 6.39 gal/sx water) Compressives: 12-hr = 900 psi 24 hr = 1500 psi

Production Casing:

Lead: 160 sxs NeoCem (mixed at 10.5 ppg, 1.14 ft3/sx, 12.26 gal/sx water) Top of Cement: Tail: 2120 sxs VersaCem (mixed at 13.2 ppg, 1.14 ft3/sx, 8.38 gal/sx water) Top of Cement: 1375 psi Compressives: 12-hr = 24 hr = 2285

Mud Circulation Program

| INTERVAL | Hole Size | Mud Type | MW (ppg) | Viscosity (sec/qt) | Fluid Loss (cc) |
|-----------------|-----------|--------------------------|-------------|-----------------------|--------------------|
| 0' - 488' | 20" | FW/Native | 8.4-8.8 | 35-40 | NC |
| 488' - 3328' | 14-3/4" | Brine | 9.8-10.2 | 30-32 | NC |
| 3328' to 9883' | 10-5/8″ | FW / Cut Brine | 8.7-9.4 | 30-32 | NC |
| 9883' to 20965' | 7-7/8" | Cut Brine / ` Polymer | 9.8 - 10.1 | 29-32 | NC - 20 |

DRILLING PLAN: BLM COMPLIANCE (Supplement to BLM 3160-3)

XTO Energy Inc. James Ranch Unit DI 1A Ennis 904H Projected TD: 20965' MD / 10656' TVD SHL: 1608' FNL & 2575' FEL , Section 21, T22S, R30E BHL: 990' FSL & 2590' FWL , Section 23, T22S, R30E Eddy County, NM

1. Geologic Name of Surface Formation

Α.

Quaternary

2. Estimated Tops of Geological Markers & Depths of Anticipated Fresh Water, Oil or Gas

| Formation | Well Depth (TVD) | Water/Oil/Gas |
|----------------------|------------------|---------------|
| Rustler | 143' | Water |
| Top of Salt | 513' | Water |
| Base of Salt | 3278' | Water |
| Delaware | 3530' | Water |
| Bone Spring Lime | 7383' | Water |
| 1st Bone Spring Ss | 8300' | Water/Oil/Gas |
| 2nd Bone Spring Ss | 8908' | Water/Oil/Gas |
| 3rd Bone Spring Carb | 9591' | Water/Oil/Gas |
| 3rd Bone Spring Ss | 10314' | Water/Oil/Gas |
| Target/Land Curve | 10656' | Water/Oil/Gas |

*** Hydrocarbons @ Brushy Canyon

*** Groundwater depth 40' (per NM State Engineers Office).

No other formations are expected to yield oil, gas or fresh water in measurable volumes. The surface fresh water sands will be protected by setting 16" inch casing @ 488' (25' above the salt) and circulating cement back to surface. The salt will be isolated by setting 11-3/4" inch casing at 3328' and circulating cement to surface. The second intermediate will isolate from the salt down to the next casing seat by setting 8-5/8" inch casing at 9883' and cemented 200' into the 11-3/4" inch casing. A 7-7/8" inch curve and lateral hole will be drilled to MD/TD and 5-1/2 inch casing will be set at TD and cemented back up to 2nd intermediate (estimated TOC 9383 feet) per Potash regulations.

Casing Design

| Hole Size | Depth | OD Csg | Weight | Collar | Grade | New/Used | SF Burst | SF Collapse | SF Tension |
|-----------|-------------|---------|--------|--------|---------|----------|-------------|----------------|---------------|
| 20" | 0' – 488' | 16" | 75 | BTC | J-55 | New | 2.77 | 5.75 | 40.07 |
| 14-3/4" | 0' – 3328' | 11-3/4" | 47 | BTC | J-55 | New | 1.13 | 1.57 | 4.96 |
| 10-5/8" | 0' – 9883' | 8-5/8" | 32 | BTC | HCL-80 | New | 1.10 | 1.38 | 2.17 |
| 7-7/8" | 0' – 20965' | 5-1/2" | 20 | C7S | CYP-110 | New | 1.20 | 1.45 | 2.25 |

· XTO requests to not utilize centralizers in the curve and lateral

· 16" Collapse analyzed using 75% evacuation. Casing to be filled while running.

· 11-3/4" Collapse analyzed using 50% evacuation based on regional experience.

· 8-5/8" Collapse analyzed using 33% evacuation based on regional experience.

· 5-1/2" Tension calculated using vertical hanging weight plus the lateral weight multiplied by a friction factor of 0.35

• Test on 2M Annular & Casing will be limited to 70% burst of the casing or 1500 psi, whichever is less

Wellhead:

Temporary Wellhead

- · 16" SOW bottom x 16-3/4" 3M top flange
- Permanent Wellhead GE RSH Multibowl System
- A. Starting Head: 13-5/8" 10M top flange x 11-3/4" SOW bottom

B. Tubing Head: 13-5/8" 10M bottom flange x 7-1/16" 15M top flange

- · Wellhead will be installed by manufacturer's representatives.
 - · Manufacturer will monitor welding process to ensure appropriate temperature of seal.
 - · Operator will test the 8-5/8" casing per BLM Onshore Order 2
 - · Wellhead Manufacturer representative will not be present for BOP test plug installation

4. Cement Program

Surface Casing: 16", 75 New J-55, BTC casing to be set at +/- 488'

Tail: 560 sxs Halcem-C + 2% CaCl (mixed at 14.8 ppg, 1.35 ft3/sx, 6.39 gal/sx water) Compressives: 12-hr = 900 psi 24 hr = 1500 psi Top of Cement: Surface Two additional 1" top out jobs will be attempted after the surface cement job. If the top of cement is not affected by the two top out jobs, ~10-20 ppb gravel will be added on the backside of the 1" to attempt to get cement to surface. 1st Intermediate Casing: 11-3/4", 47 New J-55, BTC casing to be set at +/- 3328' Lead: 1880 sxs EconoCem-HLTRRC (mixed at 12.9 ppg, 1.39 ft3/sx, 10.13 gal/sx water) Tail: 190 sxs Halcem-C + 2% CaCl (mixed at 14.8 ppg, 1.35 ft3/sx, 6.39 gal/sx water) Compressives: 12-hr = 900 psi 24 hr = 1500 psi Top of Cement: Surface 2nd Intermediate Casing: 8-5/8", 32 New HCL-80, BTC casing to be set at +/- 9883' ECP/DV Tool to be set at 3428' 1st Stage Lead: 1180 sxs Halcem-C + 2% CaCl (mixed at 12.9 ppg, 2.11 ft3/sx, 9.61 gal/sx water) Tail: 170 sxs Halcem-C + 2% CaCl (mixed at 14.8 ppg, 1.2 ft3/sx, 6.39 gal/sx water) Compressives: 12-hr = 900 psi 24 hr = 1500 psi 2nd Stage Lead: 30 sxs Halcem-C + 2% CaCl (mixed at 12.9 ppg, 2.16 ft3/sx, 9.61 gal/sx water) Tail: 150 sxs Halcem-C + 2% CaCl (mixed at 14.8 ppg, 1.33 ft3/sx, 6.39 gal/sx water) Compressives: 12-hr = 900 psi 24 hr = 1500 psi Top of Cement: 200' inside previous casing shoe

Production Casing: 5-1/2", 20 New CYP-110, C7S casing to be set at +/- 20965"

Lead: 160 sxs NeoCem (mixed at 10.5 ppg, 1.14 ft3/sx, 12.26 gal/sx water) Top of Cement: Compressives: 12-hr = 1375 psi 24 hr = 2285 psi

5. Pressure Control Equipment

The blow out preventer equipment (BOP) on surface casing temporary wellhead will consist of a 21-1/4" minimum 2M Hydril. MASP should not exceed 1016 psi.

Once the permanent WH is installed on the 11-3/4" casing, the blow out preventer equipment (BOP) will consist of a 13-5/8" minimum 5M Hydril and a 13-5/8" minimum 5M Double Ram BOP. MASP should not exceed 3252 psi.In any instance where 10M BOP is required by BLM, XTO requests a variance to utilize 5M annular with 10M ram preventers (a common BOP configuration, which allows use of 10M rams in unlikely event that pressures exceed 5M).

All BOP testing will be done by an independent service company. Annular pressure tests will be limited to 50% of the working pressure. When nippling up on the 11-3/4", 5M bradenhead and flange, the BOP test will be limited to 5M psi. When nippling up on the 8-5/8", the BOP will be tested to a minimum of 5M psi. All BOP tests will include a low pressure test as per BLM regulations. The 5M BOP diagrams are attached. Blind rams will be functioned tested each trip, pipe rams will be functioned tested each day.

A variance is requested to allow use of a flex hose as the choke line from the BOP to the Choke Manifold. If this hose is used, a copy of the manufacturer's certification and pressure test chart will be kept on the rig. Attached is an example of a certification and pressure test chart. The manufacturer does not require anchors.

XTO requests a variance to be able to batch drill this well if necessary. In doing so, XTO will set casing and ensure that the well is cemented properly and the well is static. With floats holding, no pressure on the csg annulus, and the installation of a 10K TA cap as per GE recommendations, XTO will contact the BLM to skid the rig to drill the remaining wells on the pad. Once surface and both intermediate strings are all completed, XTO will begin drilling the production hole on each of the wells.

6. Proposed Mud Circulation System

| INTERVAL | Hole Size | Mud Type | MW (ppg) | Viscosity (sec/qt) | Fluid Loss (cc) |
|-----------------|------------------|------------------------|---------------|-----------------------|--------------------|
| 0' - 488' | 88' 20" FW/Nativ | | 8.4-8.8 | 35-40 | NC |
| 488' - 3328' | 14-3/4" | Brine | 9.8-10.2 | 30-32 | NC |
| 3328' to 9883' | 10-5/8" | FW / Cut Brine | 8.7-9.4 | 30-32 | NC |
| 9883' to 20965' | 7-7/8" | Cut Brine / Polymer | 9.8 - 10.1 | 29-32 | NC - 20 |

The necessary mud products for weight addition and fluid loss control will be on location at all times.

Spud with fresh water/native mud. Drill out from under 16" surface casing with brine solution. A 9.8 ppg -10.2 ppg brine mud will be used while drilling through the salt formation. Use fibrous materials as needed to control seepage and lost circulation. Pump viscous sweeps as needed for hole cleaning. Pump speed will be recorded on a daily drilling report after mudding up. A Pason or Totco will be used to detect changes in loss or gain of mud volume. A mud test will be performed every 24 hours to determine: density, viscosity, strength, filtration and pH as necessary. Use available solids controls equipment to help keep mud weight down after mud up. Rig up solids control equipment to operate as a closed loop system.

7. Auxiliary Well Control and Monitoring Equipment

- A. A Kelly cock will be in the drill string at all times.
- B. A full opening drill pipe stabbing valve having appropriate connections will be on the rig floor at all times.
- C. H2S monitors will be on location when drilling below the 11-3/4" casing.

8. Logging, Coring and Testing Program

Mud Logger: Mud Logging Unit (2 man) below intermediate casing.

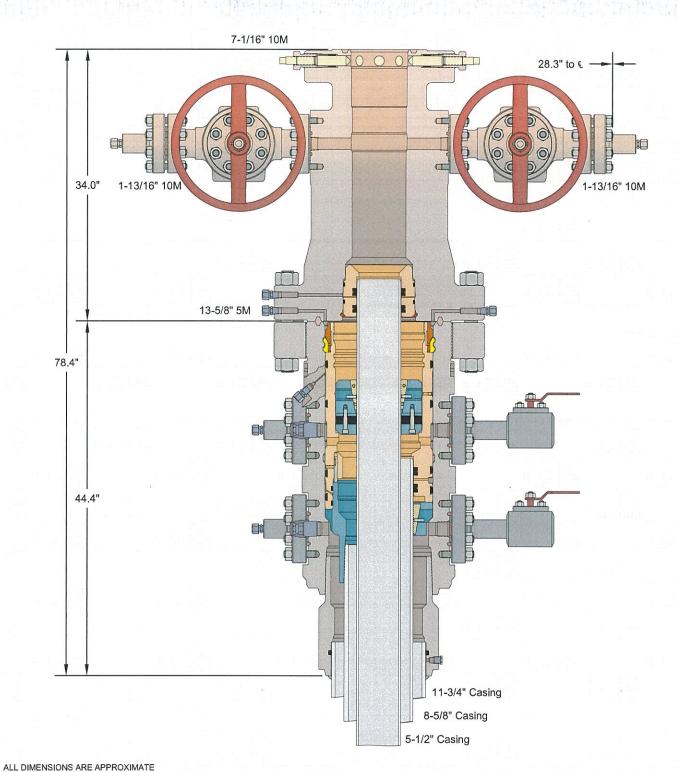
Open hole logging will not be done on this well.

9. Abnormal Pressures and Temperatures / Potential Hazards

None Anticipated. BHT of 170 to 190 F is anticipated. No H2S is expected but monitors will be in place to detect any H2S occurrences. Should these circumstances be encountered the operator and drilling contractor are prepared to take all necessary steps to ensure safety of all personnel and environment. Lost circulation could occur but is not expected to be a serious problem in this area and hole seepage will be compensated for by additions of small amounts of LCM in the drilling fluid. The maximum anticipated bottom hole pressure for this well is 5597 psi.

10. Anticipated Starting Date and Duration of Operations

Road and location construction will begin after Santa Fe and BLM have approved the APD. Anticipated spud date will be as soon after Santa Fe and BLM approval and as soon as a rig will be available. Move in operations and drilling is expected to take 40 days. If production casing is run, an additional 30 days will be needed to complete well and construct surface facilities and/or lay flow lines in order to place well on production.



GE Oil & Gas

| Assembly, With T-EBS-F Tubing Head | FOR REFERENCE ONLY DRAWING NO. 10012358 | | | |
|--|--|----------|---------|--|
| | APPRV | KN | 310CT16 | |
| 11-3/4" x 8-5/8" x 5-1/2" 10M RSH-2 Wellhead | DRAWN | VJK | 310CT16 | |
| the property of GE Oil & Gas Pressure Control LP and is considered confidential. Unless otherwise approved in writing, s contents may be used, copied, transmitted or reproduced except for the sole purpose of GE Oil & Gas Pressure Control LP. | хт | O ENERGY | , INC. | |



XTO Permian Operating, LLC

Eddy Co., NM JRU DI 1A Ennis 904H

Wellbore #1

Plan: Design #1

Standard Planning Report

28 April, 2020





Planning Report



| Database: | RyanUSA_32B | | Steel & MARY | L | ocal Co-ordinate | Reference: | Well 904H | 前 24 6 | and the ball | |
|--|---|---|---|----------------------------------|--|-----------------------------|--|---------------------------------------|---|--|
| Company: | XTO Permian (| Operating, LL | .C | The second | VD Reference: | | | bors X03) @ | 3193.00ft (Nabors | |
| Project: | Eddy Co., NM | | | N | ID Reference: | | X03) RT=33(Na X03) | RT=33(Nabors X03) @ 3193.00ft (Nabors | | |
| Site: | JRU DI 1A Enn | is | | P | North Reference: | | Grid | | | |
| Well: | 904H | | | 5 | Survey Calculation | Method: | Minimum 0 | Curvature | | |
| Wellbore: | Wellbore #1 | | | | | | | | | |
| Design: | Design #1 | | | | | | | | | |
| Project | Eddy Co., NM | | an agus agus an an an Mar gan gan an an an | rener telap en telippe metoda | ala nan ang marang ang an Mangada ang ang ang ang | | e part de la provincia de la p Nota de la provincia de la provi | an and the state | en de la companya de Esta de la companya d | |
| Geo Datum: | US State Plane 1 NAD 1927 (NADC New Mexico East | CON CONUS | | Sy | rstem Datum: | | Mean Sea Le | evel | | |
| Site | JRU DI 1A Ennis | 5 | | | | | | | | |
| Site Position: From: Position Uncertainty: | Мар | 0.00 ft | Northing: Easting: Slot Radius: | | 502,397.900 u 638,208.800 u 13-3/1 | sft Longi | | | 32° 22' 49.482274 103° 53' 8.284500 V 0.24 | |
| Well | 904H | | | | | | | | | |
| Well Position | +N/-S | 0.00 ft | Northing: | | 502,39 | 7.900 usft | Latitude: | | 32° 22' 49.479789 | |
| | +E/-W | 60.00 ft | | | 638,26 | 3.800 usft | Longitude: | | 103° 53' 7.584831 V | |
| Position Uncertainty | | 2.00 ft | Wellhead E | levation: | | | Ground Level | : | 3,160.00 | |
| Wellbore | Wellbore #1 | | | | | | | | | |
| Magnetics | Model Nam | e | Sample Date | | Declination (°) | | Dip Angle (°) | | Field Strength (nT) | |
| | HDGM_ | FILE | 4/28/202 | 20 | 6.9 | 92 | 60. | 10 | 47,929.0000000 | |
| Design | Design #1 | | | | | | | | | |
| Audit Notes: | | | | | | | | | | |
| Version: | | | Phase: | PLAN | | Tie On De | epth: | 0.00 | | |
| Vertical Section: | | Contraction of the second states of the | rom (TVD) (ft) | | +N/-S (ft) | +E/-W (ft) | | Direction (°) | | |
| | | | | | | A MARKET CONTRACT OF A DATE | | Carl Down of the later | | |

| Dej | (ft) | Depth To (ft) | Survey (Wellbore) | Tool Name | Remarks | |
|-----|------|------------------|-------------------------|-----------------|---------|--|
| 1 | 0.00 | 20,964.68 | Design #1 (Wellbore #1) | MWD+HRGM | | |
| | | | | OWSG MWD + HRGM | | |
| | | | | | | |

| Measured Depth (ft) | Inclination (°) | Azimuth (°) | Vertical Depth (ft) | +N/-S (ft) | +E/-W (ft) | Dogleg Rate (°/100ft) | Build Rate (°/100ft) | Turn Rate (°/100ft) | TFO (°) | Target |
|---------------------------|--------------------|----------------|---------------------------|---------------|---------------|-----------------------------|----------------------------|---------------------------|------------|---------------------|
| 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 3,300.00 | 0.00 | 0.00 | 3,300.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 5,310.80 | 30.16 | 167.30 | 5,219.20 | -504.51 | 113.68 | 1.50 | 1.50 | 0.00 | 167.30 | |
| 8,716.61 | 30.16 | 167.30 | 8,163.90 | -2,173.90 | 489.82 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 10,727.41 | 0.00 | 0.00 | 10,083.10 | -2,678.41 | 603.50 | 1.50 | -1.50 | 0.00 | 180.00 | |
| 11,623.00 | 89.56 | 89.89 | 10,656.04 | -2,677.33 | 1,172.04 | 10.00 | 10.00 | 10.04 | 89.89 | |
| 20,964.77 | 89.56 | 89.89 | 10,728.00 | -2,659.61 | 10,513.52 | 0.00 | 0.00 | 0.00 | 0.00 | JRU DI 1A Ennis 904 |

4/28/2020 11:52:32PM



Planning Report



| Database: | RyanUSA_32Bit | Local Co-ordinate Reference: | Well 904H |
|-----------|----------------------------|------------------------------|--|
| Company: | XTO Permian Operating, LLC | TVD Reference: | RT=33(Nabors X03) @ 3193.00ft (Nabors X03) |
| Project: | Eddy Co., NM | MD Reference: | RT=33(Nabors X03) @ 3193.00ft (Nabors X03) |
| Site: | JRU DI 1A Ennis | North Reference: | Grid |
| Vell: | 904H | Survey Calculation Method: | Minimum Curvature |
| Wellbore: | Wellbore #1 | | |
| Design: | Design #1 | | |

Planned Survey

| | Measured Depth | Inclination | Azimuth | Vertical Depth | +N/-S | +E/-W | Vertical Section | Dogleg Rate | Build Rate | Turn Rate |
|------|-------------------|-------------|---------|-------------------|---------|-------|---------------------|----------------|---------------|--------------|
| | (ft) | (°) | (°) | (ft) | (ft) | (ft) | (ft) | (°/100ft) | (°/100ft) | (°/100ft) |
| | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 100.00 | 0.00 | 0.00 | 100.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 200.00 | 0.00 | 0.00 | 200.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 1 | 300.00 | 0.00 | 0.00 | 300.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 400.00 | 0.00 | 0.00 | 400.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 500.00 | 0.00 | 0.00 | 500.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 600.00 | 0.00 | 0.00 | 600.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 700.00 | 0.00 | 0.00 | 700.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 800.00 | 0.00 | 0.00 | 800.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 900.00 | 0.00 | 0.00 | 900.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 1,000.00 | 0.00 | 0.00 | 1,000.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 1,100.00 | 0.00 | 0.00 | 1,100.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 1,200.00 | 0.00 | 0.00 | 1,200.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 1,300.00 | 0.00 | 0.00 | 1,300.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 1,400.00 | 0.00 | 0.00 | 1,400.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 1,500.00 | 0.00 | 0.00 | 1,500.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 1,600.00 | 0.00 | 0.00 | 1,600.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 1,700.00 | 0.00 | 0.00 | 1,700.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 1,800.00 | 0.00 | 0.00 | 1,800.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 1,900.00 | 0.00 | 0.00 | 1,900.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 2,000.00 | 0.00 | 0.00 | 2,000.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 2,100.00 | 0.00 | 0.00 | 2,100.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 2,200.00 | 0.00 | 0.00 | 2,200.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 2,300.00 | 0.00 | 0.00 | 2,300.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 2,400.00 | 0.00 | 0.00 | 2,400.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 181 | 2,500.00 | 0.00 | 0.00 | 2,500.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 2,600.00 | 0.00 | 0.00 | 2,600.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 2,700.00 | 0.00 | 0.00 | 2,700.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 2,800.00 | 0.00 | 0.00 | 2,800.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 2,900.00 | 0.00 | 0.00 | 2,900.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2015 | 3,000.00 | 0.00 | 0.00 | 3,000.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 3,100.00 | 0.00 | 0.00 | 3,100.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 3,200.00 | 0.00 | 0.00 | 3,200.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 3,300.00 | 0.00 | 0.00 | 3,300.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 3,400.00 | 1.50 | 167.30 | 3,399.99 | -1.28 | 0.29 | 0.59 | 1.50 | 1.50 | 0.00 |
| | 3,500.00 | 3.00 | 167.30 | 3,499.91 | -5.11 | 1.15 | 2.37 | 1.50 | 1.50 | 0.00 |
| | 3,600.00 | 4.50 | 167.30 | 3,599.69 | -11.49 | 2.59 | 5.33 | 1.50 | 1.50 | 0.00 |
| | 3,700.00 | 6.00 | 167.30 | 3,699.27 | -20.41 | 4,60 | 9.47 | 1.50 | 1.50 | 0.00 |
| | 3,800.00 | 7.50 | 167.30 | 3,798.57 | -31.88 | 7.18 | 14.78 | 1.50 | 1.50 | 0.00 |
| | 3,900.00 | 9.00 | 167.30 | 3,897.54 | -45.88 | 10.34 | 21.27 | 1.50 | 1.50 | 0.00 |
| | 4,000.00 | 10.50 | 167.30 | 3,996.09 | -62.40 | 14.06 | 28.93 | 1.50 | 1.50 | 0.00 |
| | 4,100.00 | 12.00 | 167.30 | 4,094.16 | -81.43 | 18.35 | 37.76 | 1.50 | 1.50 | 0.00 |
| | 4,200.00 | 13.50 | 167.30 | 4,191.70 | -102.96 | 23.20 | 47.74 | 1.50 | 1.50 | 0.00 |
| | 4,300.00 | 15.00 | 167.30 | 4,288.62 | -126.97 | 28.61 | 58.87 | 1.50 | 1.50 | 0.00 |
| | 4,400.00 | 16.50 | 167.30 | 4,384.86 | -153.45 | 34.58 | 71.15 | 1.50 | 1.50 | 0.00 |
| | 4,500.00 | 18.00 | 167.30 | 4,480.36 | -182.38 | 41.09 | 84.57 | 1.50 | 1.50 | 0.00 |
| | 4,600.00 | 19.50 | 167.30 | 4,575.05 | -213.73 | 48.16 | 99.11 | 1.50 | 1.50 | 0.00 |
| | 4,700.00 | 21.00 | 167.30 | 4,668.86 | -247.50 | 55.77 | 114.76 | 1.50 | 1.50 | 0.00 |
| | 4,800.00 | 22.50 | 167.30 | 4,761.74 | -283.65 | 63.91 | 131.52 | 1.50 | 1.50 | 0.00 |
| | 4,900.00 | 24.00 | 167.30 | 4,853.62 | -322.16 | 72.59 | 149.38 | 1.50 | 1.50 | 0.00 |
| | 5,000.00 | 25.50 | 167.30 | 4,944.43 | -363.00 | 81.79 | 168.32 | 1.50 | 1.50 | 0.00 |
| | 5,100.00 | 27.00 | 167.30 | 5,034.12 | -406.14 | 91.51 | 188.32 | 1.50 | 1.50 | 0.00 |



Planning Report



| Database: | RyanUSA_32Bit | Local Co-ordinate Reference: | Well 904H |
|-----------|----------------------------|------------------------------|---------------------------------------|
| Company: | XTO Permian Operating, LLC | TVD Reference: | RT=33(Nabors X03) @ 3193.00ft (Nabors |
| | | | X03) |
| Project: | Eddy Co., NM | MD Reference: | RT=33(Nabors X03) @ 3193.00ft (Nabors |
| | | | X03) |
| Site: | JRU DI 1A Ennis | North Reference: | Grid |
| Well: | 904H | Survey Calculation Method: | Minimum Curvature |
| Wellbore: | Wellbore #1 | | |
| Design: | Design #1 | | |

Planned Survey

| Measured Depth | Inclination | Azimuth | Vertical Depth | +N/-S | +E/-W | Vertical Section | Dogleg Rate | Build Rate | Turn Rate |
|-------------------|-------------|---------|-------------------|-----------|--------|---------------------|----------------|---------------|--------------|
| (ft) | (°) | (°) | (ft) | (ft) | (ft) | (ft) | (°/100ft) | (°/100ft) | (°/100ft) |
| 5,200.00 | 28,50 | 167.30 | 5,122.61 | -451.56 | 101.75 | 209.38 | 1.50 | 1.50 | 0.00 |
| 5,300.00 | 30.00 | 167.30 | 5,209.86 | -499.23 | 112,49 | 231,48 | 1.50 | 1.50 | 0.00 |
| 5,310.80 | 30,16 | 167.30 | 5,219.20 | -504.51 | 113.68 | 233.93 | 1.50 | 1.50 | 0.00 |
| 5,400.00 | 30.16 | 167.30 | 5,296,33 | -548.23 | 123.53 | 254.21 | 0.00 | 0.00 | 0.00 |
| 5,500.00 | 30.16 | 167.30 | 5,382.79 | -597.25 | 134.57 | 276.93 | 0.00 | 0.00 | 0.00 |
| 5,600.00 | 30.16 | 167.30 | 5,469.25 | -646.26 | 145.62 | 299.66 | 0.00 | 0.00 | 0.00 |
| 5,700.00 | 30.16 | 167.30 | 5,555.71 | -695.28 | 156.66 | 322.39 | 0.00 | 0.00 | 0.00 |
| 5,800.00 | 30.16 | 167.30 | 5,642.17 | -744.30 | 167.71 | 345.12 | 0.00 | 0.00 | 0.00 |
| | | | | | | | | | |
| 5,900.00 | 30.16 | 167.30 | 5,728.63 | -793.31 | 178.75 | 367.85 | 0.00 | 0.00 | 0.00 |
| 6,000.00 | 30.16 | 167.30 | 5,815.09 | -842.33 | 189.79 | 390.57 | 0.00 | 0.00 | 0.00 |
| 6,100.00 | 30.16 | 167.30 | 5,901.55 | -891.34 | 200.84 | 413.30 | 0.00 | 0.00 | 0.00 |
| 6,200.00 | 30.16 | 167.30 | 5,988.01 | -940.36 | 211.88 | 436.03 | 0.00 | 0.00 | 0.00 |
| 6,300.00 | 30.16 | 167.30 | 6,074.48 | -989.37 | 222.93 | 458.76 | 0.00 | 0.00 | 0.00 |
| 6,400.00 | 30.16 | 167.30 | 6,160.94 | -1,038.39 | 233.97 | 481.49 | 0.00 | 0.00 | 0.00 |
| 6,500.00 | 30.16 | 167.30 | 6,247.40 | -1,087.41 | 245.02 | 504.21 | 0.00 | 0.00 | 0.00 |
| 6,600.00 | 30.16 | 167.30 | 6,333.86 | -1,136.42 | 256.06 | 526.94 | 0.00 | 0.00 | 0.00 |
| 6,700.00 | 30.16 | 167.30 | 6,420.32 | -1,185.44 | 267.10 | 549.67 | 0.00 | 0.00 | 0.00 |
| 6,800.00 | 30.16 | 167.30 | 6,506.78 | -1,234.45 | 278.15 | 572.40 | 0.00 | 0.00 | 0.00 |
| 6,900.00 | 30.16 | 167.30 | 6,593.24 | -1,283,47 | 289.19 | 595.13 | 0.00 | 0.00 | 0.00 |
| 7,000.00 | 30.16 | 167.30 | 6,679.70 | -1,332,49 | 300,24 | 617.85 | 0.00 | 0.00 | 0.00 |
| 7,100.00 | 30.16 | 167.30 | 6,766.16 | -1,381.50 | 311.28 | 640.58 | 0.00 | 0.00 | 0.00 |
| 7,200.00 | 30.16 | 167.30 | 6,852.62 | -1,430.52 | 322.33 | 663.31 | 0.00 | 0.00 | 0.00 |
| 7,300.00 | 30.16 | 167.30 | 6,939.08 | -1,479.53 | 333.37 | 686.04 | 0.00 | 0.00 | 0.00 |
| 7,400.00 | 30.16 | 167.30 | 7,025.54 | -1,528.55 | 344.41 | 708.76 | 0.00 | 0.00 | 0.00 |
| 7,500.00 | 30.16 | 167.30 | 7,112.01 | -1,577.56 | 355.46 | 731.49 | 0.00 | 0.00 | Ò.00 |
| 7,600.00 | 30.16 | 167.30 | 7,198.47 | -1,626.58 | 366.50 | 754.22 | 0.00 | 0.00 | 0.00 |
| 7,700.00 | 30.16 | 167.30 | 7,284.93 | -1,675.60 | 377.55 | 776.95 | 0.00 | 0.00 | 0.00 |
| 7,800.00 | 30.16 | 167.30 | 7,371.39 | -1,724.61 | 388.59 | 799.68 | 0.00 | 0.00 | 0.00 |
| 7,900.00 | 30,16 | 167.30 | 7,457.85 | -1.773.63 | 399.64 | 822.40 | 0.00 | 0.00 | 0.00 |
| 8,000.00 | 30,16 | 167.30 | 7,544.31 | -1,822.64 | 410.68 | 845.13 | 0.00 | 0.00 | 0.00 |
| 8,100.00 | 30.16 | 167.30 | 7,630,77 | -1,871.66 | 421.72 | 867.86 | 0.00 | 0.00 | 0.00 |
| 8,200.00 | 30.16 | 167.30 | 7,717.23 | -1,920.68 | 432.77 | 890.59 | 0.00 | 0.00 | 0.00 |
| 8,200.00 | 30.16 | 167.30 | 7,803.69 | -1,969.69 | 432.77 | 913.32 | 0.00 | 0.00 | 0.00 |
| | | | | | | | | | |
| 8,400.00 | 30.16 | 167.30 | 7,890.15 | -2,018.71 | 454.86 | 936.04 | 0.00 | 0.00 | 0.00 |
| 8,500.00 | 30.16 | 167.30 | 7,976.61 | -2,067.72 | 465.90 | 958.77 | 0.00 | 0.00 | 0.00 |
| 8,600.00 | 30.16 | 167.30 | 8,063.07 | -2,116.74 | 476.95 | 981.50 | 0.00 | 0.00 | 0.00 |
| 8,700.00 | 30.16 | 167.30 | 8,149.54 | -2,165.75 | 487.99 | 1,004.23 | 0.00 | 0.00 | 0.00 |
| 8,716.61 | 30.16 | 167.30 | 8,163.90 | -2,173.90 | 489.82 | 1,008.00 | 0.00 | 0.00 | 0.00 |
| 8,800.00 | 28.91 | 167.30 | 8,236.45 | -2,214.00 | 498.86 | 1,026.60 | 1.50 | -1.50 | 0.00 |
| 8,900.00 | 27.41 | 167.30 | 8,324.61 | -2,260.04 | 509,23 | 1,047.95 | 1.50 | -1.50 | 0.00 |
| 9,000.00 | 25.91 | 167.30 | 8,413.97 | -2,303.81 | 519.10 | 1,068.24 | 1.50 | -1.50 | 0.00 |
| 9,100.00 | 24.41 | 167.30 | 8,504.48 | -2,345.29 | 528.44 | 1,087.47 | 1.50 | -1.50 | 0.00 |
| 9,200.00 | 22.91 | 167.30 | 8,596.07 | -2,384.44 | 537.26 | 1,105.63 | 1.50 | -1.50 | 0.00 |
| 9,300.00 | 21.41 | 167.30 | 8,688.68 | -2,421.23 | 545.56 | 1,122.69 | 1.50 | -1.50 | 0.00 |
| 9,400.00 | 19.91 | 167.30 | 8,782.25 | -2,455.65 | 553.31 | 1,138.65 | 1.50 | -1.50 | 0.00 |
| 9,500.00 | 18.41 | 167.30 | 8,876.71 | -2,487.67 | 560.53 | 1,153.50 | 1.50 | -1.50 | 0.00 |
| 9,600.00 | 16.91 | 167.30 | 8,971.99 | -2,517.27 | 567.19 | 1,167.22 | 1.50 | -1.50 | 0.00 |
| 9,700.00 | 15.41 | 167.30 | 9,068.03 | -2,544.42 | 573.31 | 1,179.81 | 1.50 | -1.50 | 0.00 |
| 9,800.00 | 13.91 | 167.30 | 9,164.78 | -2,569.11 | 578.88 | 1,191.26 | 1.50 | -1.50 | 0.00 |
| 9,900.00 | 12.41 | 167.30 | 9,262.15 | -2,591.32 | 583.88 | 1,201.56 | 1.50 | -1.50 | 0.00 |
| 10,000.00 | 10.91 | 167.30 | 9,360.08 | -2,611.04 | 588.32 | 1,210.70 | 1.50 | -1.50 | 0.00 |
| 10,100.00 | 9.41 | 167.30 | 9,458.51 | -2,628.25 | 592.20 | 1,218.68 | 1.50 | -1.50 | 0.00 |



Planning Report



| Database: | RyanUSA_32Bit | Local Co-ordinate Reference: | Well 904H |
|-----------|----------------------------|------------------------------|---|
| Company: | XTO Permian Operating, LLC | TVD Reference: | RT=33(Nabors X03) @ 3193.00ft (Nabors X03) X03) |
| Project: | Eddy Co., NM | MD Reference: | RT=33(Nabors X03) @ 3193.00ft (Nabors X03) |
| Site: | JRU DI 1A Ennis | North Reference: | Grid |
| Well: | 904H | Survey Calculation Method: | Minimum Curvature |
| Wellbore: | Wellbore #1 | | |
| Design: | Design #1 | | |

Planned Survey

| Measur Depth (ft) | | Inclination (°) | Azimuth (°) | Vertical Depth (ft) | +N/-S (ft) | +E/-W (ft) | Vertical Section (ft) | Dogleg Rate (°/100ft) | Build Rate (°/100ft) | Turn Rate (°/100ft) |
|-------------------------|-------|--------------------|----------------|---------------------------|---------------|---------------|-----------------------------|-----------------------------|----------------------------|---------------------------|
| 10,200 | 0.00 | 7.91 | 167.30 | 9,557.37 | -2,642.94 | 595.51 | 1,225.49 | | | |
| | | | | | | | | 1.50 | -1.50 | 0.00 |
| 10,300 | | 6.41 | 167.30 | 9,656.58 | -2,655.10 | 598.25 | 1,231.13 | 1.50 | -1.50 | 0.00 |
| 10,400 | | 4.91 | 167.30 | 9,756.09 | -2,664.72 | 600.42 | 1,235.59 | 1.50 | -1.50 | 0.00 |
| 10,500 | 0.00 | 3.41 | 167.30 | 9,855.83 | -2,671.80 | 602.01 | 1,238.87 | 1.50 | -1.50 | 0.00 |
| 10,600 | 0.00 | 1.91 | 167.30 | 9,955.71 | -2,676.33 | 603.03 | 1,240.97 | 1.50 | -1.50 | 0.00 |
| 10,700 | 0.00 | 0.41 | 167.30 | 10,055.69 | -2,678.31 | 603.48 | 1,241.89 | 1.50 | -1.50 | 0.00 |
| 10,727 | 7.41 | 0.00 | 0.00 | 10,083.10 | -2,678,41 | 603.50 | 1,241.94 | 1.50 | -1.50 | 0.00 |
| 10,750 | | 2.26 | 89.89 | 10,105.69 | -2,678.40 | 603.95 | 1,242.37 | 10.00 | 10.00 | 0.00 |
| 10,800 | | 7.26 | 89.89 | 10,155.50 | -2,678.40 | 608.09 | 1,246.39 | 10.00 | 10.00 | 0.00 |
| 10,850 | | 12.26 | 89.89 | 10,204.76 | -2,678.38 | 616.57 | 1,254.60 | 10.00 | 10.00 | 0.00 |
| 10,900 | | 17.26 | 89.89 | 10,253.09 | -2,678.36 | 629.30 | 1,266.93 | 10.00 | 10.00 | 0.00 |
| | | | | | | | | | | |
| 10,950 | | 22.26 | 89.89 | 10,300.13 | -2,678.32 | 646.20 | 1,283.31 | 10.00 | 10.00 | 0.00 |
| 11,000 | | 27.26 | 89.89 | 10,345.52 | -2,678.28 | 667.13 | 1,303.59 | 10.00 | 10.00 | 0.00 |
| 11,050 | | 32.26 | 89.89 | 10,388.92 | -2,678.24 | 691.94 | 1,327.63 | 10.00 | 10.00 | 0.00 |
| 11,100 | | 37.26 | 89.89 | 10,429.98 | -2,678.18 | 720.44 | 1,355.25 | 10.00 | 10.00 | 0.00 |
| 11,150 | 0.00 | 42.26 | 89.89 | 10,468.41 | -2,678.12 | 752.41 | 1,386.22 | 10.00 | 10.00 | 0.00 |
| 11,200 | 0.00 | 47.26 | 89.89 | 10,503.90 | -2,678.06 | 787.60 | 1,420.33 | 10.00 | 10.00 | 0.00 |
| 11,250 | 0.00 | 52.26 | 89.89 | 10,536.19 | -2,677.98 | 825.76 | 1,457.30 | 10.00 | 10.00 | 0.00 |
| 11,300 | | 57.26 | 89.89 | 10,565.03 | -2,677,91 | 866.58 | 1,496.86 | 10.00 | 10.00 | 0.00 |
| 11,350 | | 62.26 | 89.89 | 10,590,20 | -2,677.82 | 909.76 | 1,538.70 | 10.00 | 10.00 | 0.00 |
| 11,400 | | 67.26 | 89.89 | 10,611.52 | -2,677.74 | 954.97 | 1,582.51 | 10.00 | 10.00 | 0.00 |
| 11 450 | 00 | 72.26 | 89.89 | 10,628.81 | -2,677.65 | 1,001.87 | | | | |
| 11,450 | | | | | | | 1,627.95 | 10.00 | 10.00 | 0.00 |
| 11,500 | | 77.26 | 89.89 | 10,641.95 | -2,677.56 | 1,050.10 | 1,674.68 | 10.00 | 10.00 | 0.00 |
| 11,550 | | 82.26 | 89.89 | 10,650.84 | -2,677.46 | 1,099.28 | 1,722.35 | 10.00 | 10.00 | 0.00 |
| 11,600 | | 87.26 | 89.89 | 10,655.40 | -2,677.37 | 1,149.06 | 1,770.58 | 10.00 | 10.00 | 0.00 |
| 11,623 | 3.00 | 89.56 | 89.89 | 10,656.04 | -2,677.33 | 1,172.04 | 1,792.85 | 10.00 | 10.00 | 0.00 |
| 11,700 | 0.00 | 89.56 | 89.89 | 10,656.63 | -2,677.18 | 1,249.05 | 1,867.47 | 0.00 | 0.00 | 0.00 |
| 11,800 | 0.00 | 89.56 | 89.89 | 10,657.40 | -2,676.99 | 1,349.04 | 1,964.36 | 0.00 | 0.00 | 0.00 |
| 11,900 | 0.00 | 89.56 | 89.89 | 10,658,17 | -2,676.80 | 1,449.04 | 2,061.26 | 0.00 | 0.00 | 0.00 |
| 12,000 | | 89.56 | 89.89 | 10,658.95 | -2,676.61 | 1,549.04 | 2,158.16 | 0.00 | 0.00 | 0.00 |
| 12,100 | | 89.56 | 89.89 | 10,659.72 | -2,676.42 | 1,649.03 | 2,255.05 | 0.00 | 0.00 | 0.00 |
| 12,200 | 00 | 89.56 | 89.89 | 10,660.49 | -2,676.23 | 1,749.03 | 2,351,95 | 0.00 | 0.00 | 0.00 |
| 12,300 | | 89.56 | 89.89 | 10,661.26 | -2,676.04 | 1,849.03 | 2,448.85 | 0.00 | 0.00 | 0.00 |
| 12,300 | | 89.56 | 89.89 | 10,662.03 | -2,675.85 | 1,949.03 | 2,545.74 | | | |
| | | | | | | | | 0.00 | 0.00 | 0.00 |
| 12,500 | | 89.56 | 89.89 | 10,662.80 | -2,675.66 | 2,049.02 | 2,642.64 | 0.00 | 0.00 | 0.00 |
| 12,600 | 0.00 | 89.56 | 89.89 | 10,663.57 | -2,675.47 | 2,149.02 | 2,739.54 | 0.00 | 0.00 | 0.00 |
| 12,700 | 00.0 | 89.56 | 89.89 | 10,664.34 | -2,675.28 | 2,249.02 | 2,836.43 | 0.00 | 0.00 | 0.00 |
| 12,800 | 00.0 | 89.56 | 89.89 | 10,665.11 | -2,675.09 | 2,349.01 | 2,933.33 | 0.00 | 0.00 | 0.00 |
| 12,900 | 00.0 | 89.56 | 89.89 | 10,665.88 | -2,674.90 | 2,449.01 | 3,030.22 | 0.00 | 0.00 | 0.00 |
| 13,000 | 00.0 | 89.56 | 89.89 | 10,666.65 | -2,674.71 | 2,549.01 | 3,127.12 | 0.00 | 0.00 | 0.00 |
| 13,100 | | 89.56 | 89.89 | 10,667.42 | -2,674.52 | 2,649.00 | 3,224.02 | 0.00 | 0.00 | 0.00 |
| 13,200 | 00.00 | 89,56 | 89.89 | 10,668,19 | -2,674.34 | 2,749.00 | 3,320.91 | 0.00 | 0.00 | 0.00 |
| 13,300 | | 89.56 | 89.89 | 10,668.96 | -2,674.15 | 2,849.00 | 3,417.81 | 0.00 | 0.00 | 0.00 |
| 13,400 | | 89.56 | 89.89 | 10,669.73 | -2,673,96 | 2,948,99 | 3,514,71 | 0.00 | 0.00 | 0.00 |
| 13,500 | | 89.56 | 89.89 | 10,670,50 | -2,673.77 | 3,048.99 | 3,611.60 | 0.00 | 0.00 | 0.00 |
| 13,600 | | 89.56 | 89.89 | 10,671.27 | -2,673.58 | 3,048.99 | 3,708.50 | 0.00 | 0.00 | 0.00 |
| | | | | | | | | | | |
| 13,700 | | 89.56 | 89.89 | 10,672.04 | -2,673.39 | 3,248.98 | 3,805.40 | 0.00 | 0.00 | 0.00 |
| 13,800 | | 89.56 | 89.89 | 10,672.81 | -2,673.20 | 3,348.98 | 3,902.29 | 0.00 | 0.00 | 0.00 |
| 13,900 | | 89.56 | 89.89 | 10,673.58 | -2,673.01 | 3,448.98 | 3,999.19 | 0.00 | 0.00 | 0.00 |
| 14,000 | | 89.56 | 89.89 | 10,674.35 | -2,672.82 | 3,548.97 | 4,096.09 | 0.00 | 0.00 | 0.00 |
| 14,100 | .00 | 89.56 | 89.89 | 10,675.12 | -2,672.63 | 3,648.97 | 4,192.98 | 0.00 | 0.00 | 0.00 |
| 14,200 | .00 | 89.56 | 89.89 | 10,675.89 | -2,672.44 | 3,748.97 | 4,289.88 | 0.00 | 0.00 | 0.00 |
| | | | | | | | | | | |



grant .

Planning Report



| Database: | RyanUSA_32Bit | Local Co-ordinate Reference: | Well 904H |
|-----------|----------------------------|------------------------------|---------------------------------------|
| Company: | XTO Permian Operating, LLC | TVD Reference: | RT=33(Nabors X03) @ 3193.00ft (Nabors |
| | | | X03) |
| Project: | Eddy Co., NM | MD Reference: | RT=33(Nabors X03) @ 3193.00ft (Nabors |
| | | | X03) |
| Site: | JRU DI 1A Ennis | North Reference: | Grid |
| Well: | 904H | Survey Calculation Method: | Minimum Curvature |
| Wellbore: | Wellbore #1 | | |
| Design: | Design #1 | | |

Planned Survey

| Measured Depth | Inclination | Azimuth | Vertical Depth | +N/-S | +E/-W | Vertical Section | Dogleg Rate | Build Rate | Turn Rate |
|-------------------|-------------|---------|-------------------|-----------|----------------|---------------------|----------------|---------------|--------------|
| (ft) | (°) | (°) | (ft) | (ft) | +E/-VV (ft) | (ft) | (°/100ft) | (°/100ft) | (°/100ft) |
| 14,300.00 | 89,56 | 89.89 | 10,676.66 | -2,672.25 | 3,848.96 | 4,386.78 | 0.00 | 0.00 | 0.00 |
| 14,400.00 | 89.56 | 89.89 | 10,677.43 | -2,672.06 | 3,948.96 | 4,483.67 | 0.00 | 0.00 | 0.00 |
| 14,500.00 | 89.56 | 89.89 | 10,678.20 | -2,671.87 | 4,048.96 | 4,580.57 | 0.00 | 0.00 | 0.00 |
| 14,600.00 | 89.56 | 89.89 | 10,678.97 | -2,671.68 | 4,148.96 | 4,677.47 | 0.00 | 0.00 | 0.00 |
| 14,700.00 | 89.56 | 89.89 | 10,679.74 | -2,671,49 | 4,248.95 | 4,774.36 | 0.00 | 0.00 | 0.00 |
| 14,800.00 | 89.56 | 89.89 | 10,680.51 | -2,671.30 | 4,348.95 | 4,871.26 | 0.00 | 0.00 | 0.00 |
| 14,900.00 | 89.56 | 89.89 | 10,681.28 | -2.671.11 | 4,448.95 | 4,968.16 | 0.00 | 0.00 | 0.00 |
| 15,000.00 | 89.56 | 89.89 | 10,682.05 | -2,670.92 | 4,548.94 | 5,065.05 | 0.00 | 0.00 | 0.00 |
| 15,100.00 | 89.56 | 89.89 | 10,682.82 | -2,670.73 | 4,648.94 | 5,161.95 | 0.00 | 0.00 | 0.00 |
| | | | | | | | | | |
| 15,200.00 | 89.56 | 89.89 | 10,683,59 | -2,670.54 | 4,748.94 | 5,258.85 | 0.00 | 0.00 | 0.00 |
| 15,300.00 | 89.56 | 89.89 | 10,684.36 | -2,670.35 | 4,848.93 | 5,355.74 | 0.00 | 0.00 | 0.00 |
| 15,400.00 | 89.56 | 89.89 | 10,685.14 | -2,670.16 | 4,948.93 | 5,452.64 | 0.00 | 0.00 | 0.00 |
| 15,500.00 | 89.56 | 89.89 | 10,685,91 | -2,669.97 | 5,048.93 | 5,549.54 | 0.00 | 0.00 | 0.00 |
| 15,600.00 | 89.56 | 89.89 | 10,686.68 | -2,669.78 | 5,148.92 | 5,646.43 | 0.00 | 0.00 | 0.00 |
| 15,700.00 | 89.56 | 89.89 | 10,687.45 | -2,669.59 | 5,248.92 | 5,743.33 | 0.00 | 0.00 | 0.00 |
| 15,800.00 | 89.56 | 89.89 | 10,688.22 | -2,669.40 | 5,348.92 | 5,840.22 | 0.00 | 0.00 | 0.00 |
| 15,900.00 | 89.56 | 89.89 | 10,688.99 | -2,669.21 | 5,448.91 | 5,937.12 | 0.00 | 0.00 | 0.00 |
| 16,000.00 | 89.56 | 89.89 | 10,689.76 | -2,669.02 | 5,548.91 | 6,034.02 | 0.00 | 0.00 | 0.00 |
| 16,100.00 | 89.56 | 89.89 | 10,690.53 | -2,668.83 | 5,648.91 | 6,130.91 | 0.00 | 0.00 | 0.00 |
| 16,200.00 | 89.56 | 89.89 | 10,691.30 | -2,668.64 | 5,748.90 | 6,227.81 | 0.00 | 0.00 | 0.00 |
| 16,300.00 | 89.56 | 89.89 | 10,692.07 | -2,668.45 | 5,848.90 | 6,324.71 | 0.00 | 0.00 | 0.00 |
| 16,400.00 | 89.56 | 89.89 | 10,692.84 | -2,668.26 | 5,948.90 | 6,421.60 | 0.00 | 0.00 | 0.00 |
| 16,500.00 | 89.56 | 89.89 | 10,693,61 | -2,668.08 | 6,048.90 | 6,518.50 | 0.00 | 0.00 | 0.00 |
| 16,600.00 | 89.56 | 89.89 | 10,694.38 | -2,667.89 | 6,148.89 | 6,615.40 | 0.00 | 0.00 | 0.00 |
| 16,700.00 | 89.56 | . 89.89 | 10,695,15 | -2,667,70 | 6,248.89 | 6,712.29 | 0.00 | 0.00 | 0.00 |
| 16,800.00 | 89.56 | 89.89 | 10,695.92 | -2,667.51 | 6,348.89 | 6,809.19 | 0.00 | 0.00 | 0.00 |
| 16,900.00 | 89.56 | 89.89 | 10,696.69 | -2,667.32 | 6,448.88 | 6,906.09 | 0.00 | 0.00 | 0.00 |
| 17,000.00 | 89.56 | 89.89 | 10,697.46 | -2,667.13 | 6,548.88 | 7,002.98 | 0.00 | 0.00 | 0.00 |
| 17,100.00 | 89.56 | 89.89 | 10,698.23 | -2,666.94 | 6,648.88 | 7,099.88 | 0.00 | 0.00 | 0.00 |
| 17,200.00 | 89,56 | 89.89 | 10,699,00 | -2,666.75 | 6,748.87 | 7,196.78 | 0.00 | 0.00 | 0.00 |
| 17,300.00 | 89.56 | 89.89 | 10,699.77 | -2,666.56 | 6,848.87 | 7,293.67 | 0.00 | 0.00 | 0.00 |
| 17,400.00 | 89.56 | 89.89 | 10,700.54 | -2,666.37 | 6,948.87 | 7,390.57 | 0.00 | 0.00 | 0.00 |
| 17,500.00 | 89.56 | 89.89 | 10,701.31 | -2,666.18 | 7,048.86 | 7,487.47 | 0.00 | 0.00 | 0.00 |
| 17,600.00 | 89.56 | 89.89 | 10,701.31 | -2,665.99 | 7,148.86 | 7,584.36 | 0.00 | 0.00 | 0.00 |
| | | | | | | | | | |
| 17,700.00 | 89.56 | 89.89 | 10,702.85 | -2,665.80 | 7,248.86 | 7,681.26 | 0.00 | 0.00 | 0.00 |
| 17,800.00 | 89.56 | 89.89 | 10,703.62 | -2,665.61 | 7,348.85 | 7,778.16 | 0.00 | 0.00 | 0.00 |
| 17,900.00 | 89.56 | 89.89 | 10,704.39 | -2,665.42 | 7,448.85 | 7,875.05 | 0.00 | 0.00 | 0.00 |
| 18,000.00 | 89.56 | 89.89 | 10,705.16 | -2,665.23 | 7,548.85 | 7,971.95 | 0.00 | 0.00 | 0.00 |
| 18,100.00 | 89.56 | 89.89 | 10,705.93 | -2,665.04 | 7,648.85 | 8,068.85 | 0.00 | 0.00 | 0.00 |
| 18,200.00 | 89.56 | 89.89 | 10,706.70 | -2,664.85 | 7,748.84 | 8,165.74 | 0.00 | 0.00 | 0.00 |
| 18,300.00 | 89.56 | 89.89 | 10,707.47 | -2,664.66 | 7,848.84 | 8,262.64 | 0.00 | 0.00 | 0.00 |
| 18,400.00 | 89,56 | 89.89 | 10,708.24 | -2,664.47 | 7,948.84 | 8,359.54 | 0.00 | 0.00 | 0.00 |
| 18,500.00 | 89.56 | 89.89 | 10,709.01 | -2,664.28 | 8,048.83 | 8,456.43 | 0.00 | 0.00 | 0.00 |
| 18,600.00 | 89.56 | 89.89 | 10,709.78 | -2,664.09 | 8,148.83 | 8,553.33 | 0.00 | 0.00 | 0.00 |
| 18,700.00 | 89.56 | 89.89 | 10,710.55 | -2,663.90 | 8,248.83 | 8,650.22 | 0.00 | 0.00 | 0.00 |
| 18,800.00 | 89.56 | 89.89 | 10,711.33 | -2,663.71 | 8,348.82 | 8,747.12 | 0.00 | 0.00 | 0.00 |
| 18,900.00 | 89.56 | 89.89 | 10,712.10 | -2,663.52 | 8,448.82 | 8,844.02 | 0.00 | 0.00 | 0.00 |
| 19,000.00 | 89.56 | 89.89 | 10,712.87 | -2,663.33 | 8,548.82 | 8,940.91 | 0.00 | 0.00 | 0.00 |
| 19,100.00 | 89.56 | 89.89 | 10,713.64 | -2,663.14 | 8,648.81 | 9,037.81 | 0.00 | 0.00 | 0.00 |
| | | | | | | | | | |
| 19,200.00 | 89.56 | 89.89 | 10,714.41 | -2,662.95 | 8,748.81 | 9,134.71 | 0.00 | 0.00 | 0.00 |
| 19,300.00 | 89.56 | 89.89 | 10,715.18 | -2,662.76 | 8,848.81 | 9,231.60 | 0.00 | 0.00 | 0.00 |
| 19,400.00 | 89.56 | 89.89 | 10,715.95 | -2,662.57 | 8,948.80 | 9,328.50 | 0.00 | 0.00 | 0.00 |



Planning Report



| Database: | RyanUSA_32Bit | Local Co-ordinate Reference: | Well 904H |
|-----------|----------------------------|------------------------------|--|
| Company: | XTO Permian Operating, LLC | TVD Reference: | RT=33(Nabors X03) @ 3193.00ft (Nabors X03) |
| Project: | Eddy Co., NM | MD Reference: | RT=33(Nabors X03) @ 3193.00ft (Nabors X03) |
| Site: | JRU DI 1A Ennis | North Reference: | Grid |
| Well: | 904H | Survey Calculation Method: | Minimum Curvature |
| Wellbore: | Wellbore #1 | | |
| Design: | Design #1 | | |

Planned Survey

| Measured Depth (ft) | Inclination (°) | Azimuth (°) | Vertical Depth (ft) | +N/-S (ft) | +E/-W (ft) | Vertical Section (ft) | Dogleg Rate (°/100ft) | Build Rate (°/100ft) | Turn Rate (°/100ft) |
|---------------------------|--------------------|----------------|---------------------------|---------------|---------------|-----------------------------|-----------------------------|----------------------------|---------------------------|
| 19,500.00 | 89,56 | 89.89 | 10,716.72 | -2,662.38 | 9,048.80 | 9,425.40 | 0.00 | 0.00 | 0.0 |
| 19,600.00 | 89.56 | 89.89 | 10,717.49 | -2,662.19 | 9,148.80 | 9,522.29 | 0.00 | 0.00 | 0.0 |
| 19,700.00 | 89.56 | 89.89 | 10,718.26 | -2,662.00 | 9,248.79 | 9,619.19 | 0.00 | 0.00 | 0.0 |
| 19,800.00 | 89.56 | 89.89 | 10,719.03 | -2,661.81 | 9,348.79 | 9,716.09 | 0.00 | 0.00 | 0.0 |
| 19,900.00 | 89.56 | 89.89 | 10,719.80 | -2,661.63 | 9,448.79 | 9,812.98 | 0.00 | 0.00 | 0.0 |
| 20,000.00 | 89.56 | 89.89 | 10,720.57 | -2,661.44 | 9,548.79 | 9,909.88 | 0.00 | 0.00 | 0.0 |
| 20,100.00 | 89.56 | 89.89 | 10,721.34 | -2,661.25 | 9,648.78 | 10,006.78 | 0.00 | 0.00 | 0.0 |
| 20,200.00 | 89.56 | 89.89 | 10,722.11 | -2,661.06 | 9,748.78 | 10,103.67 | 0.00 | 0.00 | 0.0 |
| 20,300.00 | 89.56 | 89.89 | 10,722.88 | -2,660.87 | 9,848.78 | 10,200.57 | 0.00 | 0.00 | 0.0 |
| 20,400.00 | 89,56 | 89.89 | 10,723.65 | -2,660.68 | 9,948.77 | 10,297.47 | 0.00 | 0.00 | 0.0 |
| 20,500.00 | 89,56 | 89.89 | 10,724.42 | -2,660.49 | 10,048.77 | 10,394.36 | 0.00 | 0.00 | 0.0 |
| 20,600.00 | 89.56 | 89.89 | 10,725.19 | -2,660.30 | 10,148.77 | 10,491.26 | 0.00 | 0.00 | 0.0 |
| 20,700.00 | 89.56 | 89.89 | 10,725.96 | -2,660.11 | 10,248.76 | 10,588.16 | 0.00 | 0.00 | 0.0 |
| 20,800.00 | 89.56 | 89.89 | 10,726.73 | -2,659.92 | 10,348.76 | 10,685.05 | 0.00 | 0.00 | 0.0 |
| 20,900.00 | 89.56 | 89.89 | 10,727.50 | -2,659.73 | 10,448.76 | 10,781.95 | 0.00 | 0.00 | 0.0 |
| 20,964,77 | 89.56 | 89.89 | 10,728.00 | -2.659.61 | 10,513,52 | 10,844,71 | 0.00 | 0.00 | 0.0 |

| Design Targets | | | | | | | | | |
|--|------------------------|----------------------------|----------------------------|--------------------------|-----------------------------|---------------------------|-------------------|---------------------|---------------------|
| Target Name - hit/miss target - Shape | Dip Angle (°) | Dip Dir. (°) | TVD (ft) | +N/-S (ft) | +E/-W (ft) | Northing (usft) | Easting (usft) | Latitude | Longitude |
| JRU DI 1A Ennis 904H - - plan misses target o - Point | 0.00 center by 237. | | 10,656.00 8.37ft MD (1 | -2,678.41 0488.92 TVD | 603.50 , -2678.09 N, 7 | 499,719.500 771.99 E) | 638,872.300 | 32° 22' 22.949728 N | 103° 53' 0.678634 W |
| JRU DI 1A Ennis 904H - - plan misses target o - Point | 0.00 center by 14.7 | and a second second second | 10,727.00 0.00ft MD (10 | -2,659.71 727.50 TVD, | 10,463.52 -2659.73 N, 10 | 499,738.200 0448.76 E) | 648,732.300 | 32° 22' 22.710064 N | 103° 51' 5.708438 W |
| JRU DI 1A Ennis 904H - - plan hits target cent - Point | 0.00 er | 0.00 | 10,728.00 | -2,659.61 | 10,513.52 | 499,738.300 | 648,782.300 | 32° 22′ 22.708826 N | 103° 51' 5.125426 W |



Planning Report



| Database: | RyanUSA_32Bit | Local Co-ordinate Reference: | Well 904H |
|-----------|----------------------------|------------------------------|--|
| Company: | XTO Permian Operating, LLC | TVD Reference: | RT=33(Nabors X03) @ 3193.00ft (Nabors X03) |
| Project: | Eddy Co., NM | MD Reference: | RT=33(Nabors X03) @ 3193.00ft (Nabors X03) |
| Site: | JRU DI 1A Ennis | North Reference: | Grid |
| Well: | 904H | Survey Calculation Method: | Minimum Curvature |
| Wellbore: | Wellbore #1 | | |
| Design: | Design #1 | | |

Formations

| Measured Depth (ft) | Vertical Depth (ft) | Name | Lithology | Dip Dip Direction (°) (°) | n |
|---------------------------|---------------------------|--------------------------------|-----------|---------------------------------|---|
| 143.00 | 143.00 | Rustler | | | |
| 513.00 | 513.00 | Salado (Top of Salt) | | | |
| 2,167.00 | 2,167.00 | Castile Anhydrite 1 Top | | | |
| 2,603.00 | 2,603.00 | Castile Anhydrite 1 Base | | | |
| 2,825.00 | 2,825.00 | Castile Anhydrite 2 Top | | | |
| 2,927.00 | 2,927.00 | Castile Anhydrite 2 Base | | | |
| 3,278.00 | 3,278.00 | Base of Salt | | | |
| 3,530.14 | 3,530.00 | Delaware/Lamar | | | |
| 3,573.23 | 3,573.00 | Bell Canyon | | | |
| 4,674.47 | 4,645.00 | Cherry Canyon | | | |
| 6,231.21 | 6,015.00 | Brushy Canyon Ss. | | | |
| 7,813.43 | 7,383.00 | Bone Spring Lm. | | | |
| 7,862.01 | 7,425.00 | Avalon Ss. | | | |
| 8,121.08 | 7,649.00 | Upper Avalon Carb. | | | |
| 8,213.61 | 7,729.00 | Upper Avalon Sh. | | | |
| 8,299.20 | 7,803.00 | Middle Avalon Carb. | | | |
| 8,491.19 | 7,969.00 | Lower Avalon Sh. | | | |
| 8,708.63 | 8,157.00 | First Bone Spring Carb. | | | |
| 8,872.23 | 8,300.00 | First Bone Spring Ss. | | | |
| 9,379.51 | 8,763.00 | Second Bone Spring Carb. | | | |
| 9,532.94 | 8,908.00 | Second Bone Spring Ss. | | | |
| 9,990.75 | 9,351.00 | Second Bone Spring A/B Carb. | | | |
| 10,081.23 | 9,440.00 | Second Bone Spring B Ss. | | | |
| 10,233.94 | 9,591.00 | Third Bone Spring Carb. | | | |
| 10,495.17 | 9,851.00 | Third Bone Spring Shale | | | |
| 10,965.07 | 10,314.00 | Third Bone Spring Ss. | | | |
| 11,403.87 | 10,613.00 | Third Bone Spring Ss Red Hills | | | |
| 11,619.27 | 10,656.00 | Horizontal Landing Point | | | |
| 16,940.34 | 10,697.00 | Wolfcamp Shale | | | |
| 18,887.64 | 10,712.00 | Wolfcamp X Ss. | | | |
| 20,964.77 | 10,728.00 | Horizontal TD | | | |

XTO respectfully requests approval to utilize a spudder rig to pre-set surface casing.

Description of Operations:

- 1. Spudder rig will move in to drill the surface hole and pre-set surface casing on the well.
 - After drilling the surface hole section, the spudder rig will run casing and cement following all of the applicable rules and regulations (OnShore Order 2, all COAs and NMOCD regulations).
 - b. The spudder rig will utilize fresh water-based mud to drill the surface hole to TD. Solids control will be handled entirely on a closed loop basis. No earth pits will be used.
- 2. The wellhead will be installed and tested as soon as the surface casing is cut off and WOC time has been reached.
- 3. A blind flange at the same pressure rating as the wellhead will be installed to seal the wellbore. Pressure will be monitored with needle valves installed on two wing valves.
 - a. A means for intervention will be maintained while the drilling rig is not over the well.
- 4. Spudder rig operations are expected to take 2-3 days per well on the pad.
- 5. The BLM will be contacted and notified 24 hours prior to commencing spudder rig operations.
- 6. Drilling Operations will begin with a larger rig and a BOP stack equal to or greater than the pressure rating that was permitted will be nippled up and tested on the wellhead before drilling operations resume on each well.
 - a. The larger rig will move back onto the location within 180 days from the point at which the wells are secured and the spudder rig is moved off location.
 - b. The BLM will be notified 24 hours before the larger rig moves back on the pre-set locations
- 7. XTO will have supervision on the rig to ensure compliance with all BLM and NMOCD regulations and to oversee operations.
- 8. Once the rig is removed, XTO will secure the wellhead area by placing a guard rail around the cellar area.

Subject: Request for a Variance Allowing break Testing of the Blowout Preventer Equipment (BOPE)

XTO Energy requests a variance to ONLY test broken pressure seals on the BOPE and function test BOP when skidding a drilling rig between multiple wells on a pad.

Background

Onshore Oil and Gas Order (OOGO) No. 2, Drilling Operations, Sections III.A.2.i.iv.B states that the BOP test must be performed whenever any seal subject to test pressure is broken. The current interpretation of the Bureau of Land Management (BLM) requires a complete BOP test and not just a test of the affected component. OOGO No. 2, Section I.D.2 states, "Some situation may exist either on a well-by-well basis or field-wide basis whereby it is commonly accepted practice to vary a particular minimum standard(s) established in this order. This situation can be resolved by requesting a variance...". XTO Energy feels the break testing the BOPE is such a situation. Therefore, as per OOGO No. 2, Section IV., XTO Energy submits this request for the variance.

Supporting Documentation

OOGO No. 2 became effective on December 19, 1988 and has remained the standard for regulating BLM onshore drilling operations for over 30 years. During this time there have been significant changes in drilling technology. BLM continues to use the variance request process to allow for the use of modern technology and acceptable engineering practices that have arisen since OOGO No. 2 was originally released. The XTO Energy drilling rig fleet has many modern upgrades that allow the intact BOP stack to be moved between well slots on a multi-well pad, as well as, wellhead designs that incorporate quick connects facilitating release of the BOP from the wellhead without breaking any BOP stack components apart. These technologies have been used extensively offshore, and other regulators, API, and many operators around the world have endorsed break testing as safe and reliable.



Figure 1: Winch System attached to BOP Stack

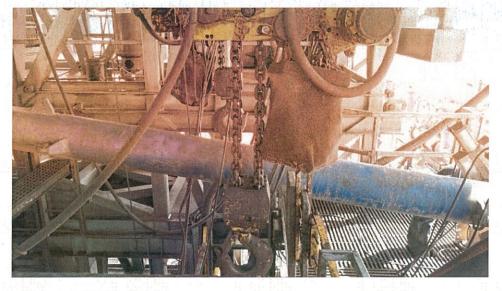


Figure 2: BOP Winch System

American Petroleum Institute (API) standards, specification and recommended practices are considered the industry standard and are consistently utilized and referenced by the industry. OOGO No. 2 recognizes API recommended Practices (RP) 53 in its original development. API Standard 53, *Well Control Equipment Systems for Drilling Wells* (Fifth Edition, December 2018, Annex C, Table C.4) recognizes break testing as an acceptable practice. Specifically, API Standard 53, Section 5.3.7.1 states "A pressure test of the pressure containing component shall be performed following the disconnection or repair, limited to the affected component." See Table C.4 below for reference.

| | Pressure Test-Low | Pressure Test—High Pressure | | | | |
|--|--|---|---|--|--|--|
| Component to be Pressure Tested | Pressure ³⁰ psig (MPa) | Change Out of Component, Elastomer, or Ring Gasket | No Change Out of Component, Elastomer, or Ring Gasket | | | |
| Annular preventer ⁶ | 250 to 350 (1.72 to 2.41) | RWP of annular preventer | MASP or 70% annular RWP, whichever is lower. | | | |
| Fixed pipe, variable bore, blind, and BSR preventers ^{bd} | 250 to 350 (1.72 to 2.41) | RWP of ram preventer or wellhead system, whichever is lower | ITP | | | |
| Choke and kill line and BOP side outlet valves below ram preventers (both sides) | 250 to 350 (1.72 to 2.41) | RWP of side outlet valve or wellhead system, whichever is lower | ITP | | | |
| Choke manifold—upstream of chokes* | 250 to 350 (1.72 to 2.41) | RWP of ram preventers or wellhead system, whichever is lower | ITP | | | |
| Choke manifold—downstream of chokes® | 250 to 350 (1.72 to 2.41) | RWP of valve(s), line(s), or M whichever is lower | ASP for the well program, | | | |
| Kelly, kelly valves, drill pipe safety valves, IBOPs | 250 to 350 (1.72 to 2.41) | MASP for the well program | | | | |
| Annular(s) and VBR(s) shall be pre- For pad drilling operations, moving pressure-controlling connections For surface offshore operations, the | during the evaluation period. The p ssure tested on the largest and sma from one wellhead to another within when the integrity of a pressure set the ram BOPs shall be pressure test | n the 21 days, pressure testing is req al is broken. | program. uired for pressure-containing an the closing and locking pressur | | | |

The Bureau of Safety and Environmental Enforcement (BSEE), Department of Interior, has also utilized the API standards, specification and best practices in the development of its offshore oil and gas regulations and incorporates them by reference within its regulations.

Break testing has been approved by the BLM in the past with other operators based on the detailed information provided in this document.

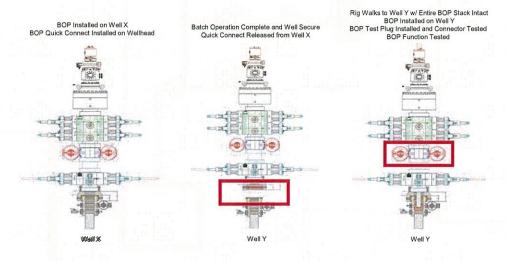
XTO Energy feels break testing and our current procedures meet the intent of OOGO No. 2 and often exceed it. There has been no evidence that break testing results in more components failing than seen on full BOP tests. XTO Energy's internal standards requires complete BOPE tests more often than that of OOGO No. 2 (Every 21 days). In addition to function testing the annular, pipe rams and blind rams after each BOP nipple up, XTO Energy performs a choke drill with the rig crew prior to drilling out every casing shoe. This is additional training for the rig crew that exceeds the requirements of the OOGO No.2.

Procedures

- XTO Energy will use this document for our break testing plan for New Mexico Delaware basin. The summary below will be referenced in the APD or Sundry Notice and receive approval prior to implementing this variance.
- 2. XTO Energy will perform BOP break testing on multi-wells pads where multiple intermediate sections can be drilled and cased within the 21-day BOP test window.
 - a. A full BOP test will be conducted on the first well on the pad.
 - b. The first intermediate hole section drilled on the pad will be the deepest. All of the remaining hole sections will be the same depth or shallower.
 - i. Our Lower WC targets set the intermediate casing shoe no deeper than the Wolfcamp B.
 - ii. Our Upper WC targets set the intermediate casing shoe shallower than the Wolfcamp B.
 - c. A Full BOP test will be required if the intermediate hole section being drilled has a MASP over 5M.
 - d. A full BOP test will be required prior to drilling any production hole.
- 3. After performing a complete BOP test on the first well, the intermediate hole section will be drilled and cased, two breaks would be made on the BOP equipment.
 - a. Between the HCV valve and choke line connection
 - b. Between the BOP quick connect and the wellhead
- 4. The BOP is then lifted and removed from the wellhead by a hydraulic system.
- 5. After skidding to the next well, the BOP is moved to the wellhead by the same hydraulic system and installed.
- 6. The connections mentioned in 3a and 3b will then be reconnected.
- 7. Install test plug into the wellhead using test joint or drill pipe.
- 8. A shell test is performed against the upper pipe rams testing the two breaks.
- 9. The shell test will consist of a 250 psi low test and a high test to the value submitted in the APD or Sundry (e.g. 5,000 psi or 10,000psi).
- 10. Function test will be performed on the following components: lower pipe rams, blind rams, and annular.

- 11. For a multi-well pad the same two breaks on the BOP would be made and on the next wells and steps 4 through 10 would be repeated.
- 12. A second break test would only be done if the intermediate hole section being drilled could not be completed within the 21 day BOP test window.

Note: Picture below highlights BOP components that will be tested during batch operations



Summary

A variance is requested to **ONLY** test broken pressure seals on the BOP equipment when moving from wellhead to wellhead which is in compliance with API Standard 53. API Standard 53 states, that for pad drilling operation, moving from one wellhead to another within 21 days, pressure testing is required for pressure-containing and pressure-controlling connections when the integrity of a pressure seal is broken.

The BOP will be secured by a hydraulic carrier or cradle. The BLM will be contacted if a Well Control event occurs prior to the commencement of a BOPE Break Testing operation.

Based on discussions with the BLM on February 27th 2020 and the supporting documentation submitted to the BLM, we will request permission to ONLY retest broken pressure seals if the following conditions are met:

1. After a full BOP test is conducted on the first well on the pad.

2. The first intermediate hole section drilled on the pad will be the deepest. All of the remaining hole sections will be the same depth or shallower.

3. Full BOP test will be required if the intermediate hole section being drilled has a MASP over 5M.

4. Full BOP test will be required prior to drilling the production hole.

