OPERATOR'S COPY



United States Department of the Interior

BUREAU OF LAND MANAGEMENT

Roswell Field Office 2909 West Second Street Roswell, New Mexico 88201

IN REPLY REFER TO:

KAP 25 2000

Devon Energy Production Company, L.P. 20 North Broadway, Suite 1500 Oklahoma City, OK 73102-8260 Attn: Karen Cottom

Re: Delaware Formation in Sec 12, 13 & 24, T22S-R30E Master Drilling and Surface Use Plan Eddy County, New Mexico

Dear Karen:

The Master Drilling and Surface Use Plan, dated July 17, 2003, for the Delaware Formation in Sec 12, 13 & 24, T22S-R30E, Eddy County, New Mexico, is now approved. Revised page 5, received by fax on September 4, 2003, has been inserted. Changes have also been made to page 2, Casing Program. An approved copy is attached for your records.

Please direct any questions to Les Babyak, 505-627-0219.

Larry D. Bray

Assistant Field Manager Lands and Minerals

cc: NM 08000 (Amos, Hunt) NM 06000 (Lopez, Swoboda, Babyak)



20 North Broadway, Suite 1500 Oklahoma City, Oklahoma 73102-8260 Fax: (405) 552-4621

Telephone: (405) 228-7512

July 17, 2003

Bureau of Land Management Attn Armando Lopez 2909 West Second Street Roswell, NM 88201

Re:

Master Drilling and Surface Use Program

Delaware Formation in Sec 12, 13 & 24, T22S R30E

Dear Armando:

I am submitting a Master Drilling and Surface Use Program, one original and five copies, for the referenced area. I have enclosed the program and a map detailing the area for which we intend to use the program. I am also submitting eight APD's with the Master.

Please contact me should there be any additional information required. Thanks for your help.

Sincerely,

Karen Cottom

Engineering Technician

Devon Energy Production Company, L.P.

kc

Enclosure

R-111-P-POTASH

Master Drilling Program Delaware Formation on the Following Leases.

To be attached to Form 3160-3

UNIT AREA: Leases in the following sections, Townships and Ranges that are operated by Devon Energy Production Company, LP.

Lease Numbers as follows but not limited to:

Section	Lease Number	Description of Section	Township & Range
Section 12	NMNM89051	SE4/SE4	T22S R30E
Section 13	NMNM89051	E2, E2/SW4, SE4/NW4	T22S R30E
Section 24	NMNM89051	All of Section 24 except W2/NW4	T22S R30E

If drilling is proposed on additional leases, the BLM will be advised when they are proposed.

1. Geologic Name of Surface Formation:

Permian

2. Estimated Tops of Important Geologic Markers:

Permian	Surface
Base of Salt	3690'
Delaware	3950'
Bone Spring	7720'
Total Depth	7860'
•	

3. Estimated Depths of Anticipated Fresh Water, Oil or Gas:

Upper Permian Sands	100'	Fresh Water
Delaware	3950'	Oil
Delaware	7475'	Oil

No other formations are expected to yield oil, gas or fresh water in measurable volumes. The surface fresh water sands will be protected by setting 13 3/8" casing at approximately 620' and circulating cement back to surface. The Potash and salt will be protected by setting 8 5/8" casing at 3845' and circulating cement to surface. The 5 ½" production casing to be set at TD will be cemented to surface.

Memorandum 7/24/03

To: Engin

Engineers, RFO

From:

Geologist, RFO

Subject:

Devon Master Drilling and Surface Plan

Talked with Karen Cottom on July 24, 2003 in order to amend the plan's casing program. Surface casing will be set 420 ft. in sec. 12, 510 ft. in sec. 13 and 620 ft sec. 24, T. 22 S., R. 30 E., NMPM.

/John S. Simitz

2

420 ft in Sec 12 - T22S - R30E

4. Casing Program:

510 ft in Sec 13 - T22S - R30E 620 ft in Sec 24 - T22S - R30E

Hole Size	Interval	Csg OD	Weight,	Grade	Type
17 ½"	SEE ABOVE	13 3/8"	48#	H-40	ST&C
12 1/4"	0 – 3845'	8 5/8"	32#	J-55	ST&C
7 7/8"	0 – TD	5 1/2"	15.5 & 17#	J-55	LT&C

5. Casing Cementing & Setting Depth:

13 3/8"

Surface:

Cement to surface with 525 sx of Class C + 2% CaCl2

+ 1/4#/sx Flocele.

8 5/8"

Intermediate:

Cement to surface Lead w/1500 sx Lite + 15#/sx salt +

 $\frac{1}{4}$ sx FC and tail w/200 sx Class C + 2% CaCl2.

5-1/2"

Production:

Cement 1st Stage Lead w/ 173 sx 35:65 Poz C & tail

w/773 60:40 Poz C sx cmt. Set DV tool @± 4000' 2nd Stage Lead w/259 sx 35:65 Poz C & tail w/150 sx

60:40 Poz C, circulate cement to surface.

The above cement volumes could be revised pending the caliper measurement from the open hole logs.

6. Minimum Specifications for Pressure Control:

The blowout preventer equipment (BOP) shown in Exhibit #1 will consist of a double ram-type (3000 psi WP) preventer and bag-type (hydril) preventer (3000 psi WP). Both units will be hydraulically operated and the ram-type preventer will be equipped with blind rams on top and 4 ½" drill pipe rams on bottom. Both BOP's will be nippled up on the 13 3/8" surface csg and used continuously until TD is reached. All BOP's and accessory equipment will be tested to 1000 psi before drilling out of surface casing. Before drilling out of intermediate casing, the ram-type BOP and accessory equipment will be tested to 3000 psi and the hydril to 70% of rated working pressure (2100 psi).

Pipe rams will be operated and checked weekly and the blind rams each time the drill pipe is out of the hole. These functional tests will be documented on the drillers log. A 2" kill line and 3" choke line will be incorporated in the drilling spool below the ram-type BOP. Other accessory BOP equipment will include a Kelly cock, floor safety valve, choke lines and choke manifold having 3000 psi WP rating.

6. Types and Characteristics of the Proposed Mud System:

The well will be drilled to total depth using a fresh and Brine water mud systems. Depths of systems are as follows:

OI By Blotting and t	*U XUIIU 11 U.			
<u>Depth</u>	Type	Weight	Viscosity	Water
		(ppg)	(1/sec)	Loss
0' - 620'	Fresh Water	8.8	40-45	NC
620' – 3845'	Brine Water	10	30	NC
3845' – TD	Fresh Water/Gel/Starch	8.5 – 9.0	30-32	50-60

The necessary mud products for weight addition and fluid loss control will be on location at all times.

7. <u>Auxiliary Well Control and Monitoring Equipment</u>:

- A. A Kelly cock will be in the drill string at all times.
- B. A full opening drill pipe stabbing valve having the appropriate connections will be on the rig floor at all times.
- C. Hydrogen sulfide detection equipment will be in operation after drilling out the 8 5/8" casing shoe until 5 ½" casing is cemented.

8. <u>Logging, Testing and Coring Program</u>:

- A. Drillstem tests will be run on the basis of drilling shows.
- B. The open hole electrical logging program will be:
 - a. GR-AIT, GR-Compensated Neutron-Density from TD to 3845' and GR/CNL to surface. Selected SW cores may be taken in zones of interest.
 - b. No coring program is planned.
 - c. Additional testing will be initiated subsequent to setting the 5 ½" production casing. Specific intervals will be targeted based on log evaluation, geological sample shows and drill stem tests.

9. Abnormal Pressures, Temperatures and Potential Hazards:

No abnormal pressures or temperatures are foreseen. The anticipated bottom hole temperature at total depth is 122 degrees and maximum bottom hole pressure is 3500 psi. No Hydrogen sulfide or other hazardous gases or fluids have been encountered, reported or are known to exist at this depth in this area. No major loss circulation intervals have been encountered in adjacent wells.

10. Anticipated Starting Date and Duration of Operations:

Road and location preparation will not be undertaken until approval has been received from the BLM. The anticipated spud date will be provided with each well application. The drilling operation should require approximately 45 days. If the well is deemed productive, completion operations will require, at minimum, an additional 30 days of testing to ascertain whether the well will be connected to an existing production facility.

MASTER SURFACE USE AND OPERATING PLAN Delaware Formation on the Following Leases

This plan will be submitted with Form 3160-3, Application for Permit to Drill. The purpose of this plan is to describe the location of the proposed wells, the proposed construction activities and operations plan, the magnitude of necessary surface disturbance involved and the procedures to be followed in rehabilitating the surface after completion of the operations. This plan will allow a complete appraisal to be made of the environmental effects associated with the proposed operations.

<u>UNIT AREA:</u> Leases in the following Sections, Townships and Ranges that are Operated by Devon Energy Production Company, LP.

Lease Numbers as follows but not limited to:

Section	Lease Number	Description of Section	Township & Range
Section 12	NMNM89051	SE4/SE4	T22S R30E
Section 13	NMNM89051	E2, E2/SW4, SE4/NW4	T22S R30E
Section 24	NMNM89051	All of Section 24 except W2/NW4	T22S R30E

If drilling is proposed on additional leases, the BLM will be advised when they are proposed.

1. Existing Roads:

- A. The well site and elevation plat for each well will be provided with the 3160-3 when proposed.
- B. All roads to the location are shown on Exhibit #2 of each individual application. The existing roads are illustrated in red and are adequate for travel during drilling and production operations. Upgrading of the roads prior to drilling will be done where necessary as determined during the onsite inspections.
- C. Directions to location will be provided for each individual well application.
- D. Routine grading and maintenance of existing roads will be conducted as necessary to maintain their condition as long as any operations continue on the lease.

2. Proposed Access Road

Exhibit #3 of each application will show the new access road (if necessary) to be constructed and will be illustrated in yellow. The road will be constructed as follows:

- A. The maximum width of the road will be fifteen (15) feet.
- B. It will be crowned and made of 6 inches of rolled and compacted caliche. Water will be deflected, as necessary, to avoid accumulation and prevent surface erosion.
- C. Surface material will be native caliche. This material will be obtained from a BLM approved pit nearest in proximity to the location.
- D. The average grade will be approximately 1%.
- E. No cattle guards; grates or fence cuts will be required
- F. No turnouts are planned.

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4. Location of Existing and/or Proposed Facilities:

In the event the well is found productive, the collection facilities will be placed on the first well drilled in Section 24, T22S R30E and the first well drilled in Section 13, T22S R30E. The tank battery, all connections and lines will adhere to API standards. Off lease storage will be requested at time of drilling for all additional wells in each Section if needed.

- A. If the well is productive, rehabilitation plans are as follows:
 - a. The reserve pit will be back-filled after the contents of the pit are dry (within 120 days after completion, weather permitting).
 - b. The drill site will then be contoured as close to the original natural state as possible.

5. Methods of Handling Water Disposal:

- A. Drill cuttings will be disposed into the reserve pit.
- B. Drilling fluids will be contained in steel mud tanks or lined earthen pits and the reserve pit. The reserve pit will contain excess drilling fluid or fluid from the well during drilling, cementing, and completion operations. The reserve pit will be an earthen pit roughly 70' x 70' x 5', or smaller, in size.
- C. The reserve pit will be fenced on three sides throughout drilling operations and will be totally isolated upon removal of the rotary rig. The pit will be lined using a 5-7 mil plastic to minimize loss of drilling fluids.
- D. Water produced from the well during completion operations will be disposed into a steel tank or reserve pit, if volumes prove excessive. After placing the well on production through the production facilities, all water will be collected in tanks and injected into the water injection system. Produced oil will be separated into steel stock tanks until sold.
- E. A portable chemical toilet will be available on the location for human waste during the drilling operations.
- F. Garbage, trash and waste paper produced during drilling operations will be collected in a contained trailer and disposed at a approved landfill. All waste material will be contained to prevent scattering by the wind. All water, fluids, salt or other chemicals will be disposed into the reserve pit. No toxic waste or hazardous chemicals will be generated by this operation.
- G. All waste material will be removed within 30 days after the well is either completed or abandoned. The reserve pit will be completely fenced until it has dried. At the point the reserve pit is found sufficiently dry, it will be backfilled and reclaimed. The portion of the drilling pad used by the production equipment (pumping unit) will remain in use.

6. Well Site Layout:

- A. The drill pad layout will be shown on Exhibit 4 for each individual well. Dimensions
- B. No permanent living facilities are planned, but temporary trailers for the tool pusher, drilling foreman and mud logger may be on location throughout drilling operations.
- C. The reserve pit and earthen pits will be lined using plastic sheeting of 5-7 mil thickness.

7. Surface Ownership:

The well site and lease is located entirely on Federal surface. J. C. Mills, Abernathy, TX and Kenneth Smith, Carlsbad, NM have the Federal grazing lease on this surface.

8. Other Information:

- A. The project areas are classified as grassland and top soil is sandy. The vegetation is native scrub grasses with abundant oakbrush, sage-brush, yucca, and prickly pear.
- B. There is no permanent water in the immediate area.
- C. A Cultural Resources Examination for each APD will be completed by Don Clifton Archeological Services, Inc. and forwarded to the Carlsbad, New Mexico BLM office.

9. <u>Lessee's and Operator's Representative</u>:

The Devon Energy Corporation representatives responsible for assuring compliance of the surface use plan are:

Operations Engineering Advisor	Don Mayberry Superintendent
Devon Energy Production, L.P. 20 North Broadway Suite 1500 Oklahoma City, OK 73102	Devon Energy Production Company, L.P. P.O. Box 250 Artesia, NM 88211-0250
(405) 228-4301 (office) (405) 834-9207 (home)	(505) 748-3371 (office) (505) 746-4945 (home)

Certification:

I hereby certify that I am familiar with the conditions that presently exist; that the statements made in this plan are, to the best of my knowledge, true and correct; and that the work associated with the operations proposed herein will be performed by Devon Energy Corporation (Nevada) and its contractors and subcontractors in conformity with this plan and the terms and conditions under which it is approved.

Date: July 16, 2003

Signed: James Blount

Operations Engineering Advisor

UNITED STATES DEPARTMENT OF THE INTERIOR

Bureau of Land Management Roswell Field Office 2909 West Second Street Roswell, New Mexico 88201-1287

Statement Accepting Responsibility for Operations

Operator Name: Street or Box: City, State: Zip Code:	Devon Energy Production Company, LP 20 North Broadway, Ste 1500 Oklahoma City, OK 73102
• • • • • • • • • • • • • • • • • • • •	able terms, conditions, stipulations and restrictions in the leased land or portion thereof, as described
Lease No.:	NMNM89051
Legal Description of Land:	Sec 12 – SE4/SE4 Sec 13 – E2, E2/SW4, SE4/NW4 Sec 24 – All of section 24 except W2/NW4
Formation(s):	Delaware
Bond Coverage:	Nationwide
BLM Bond File No.:	CO1104
Authorized Signature: Title:	James Blount Operations Engineering Advisor
Date:	7/16/03

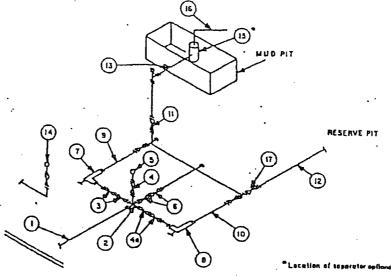
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Attachment to Exhibit #1

NOTES REGARDING BLOWOUT PREVENTORS

Quahada Ridge SE Eddy County, New Mexico

- 1. Drilling nipple will be constructed so it can be removed mechanically without the aid of a welder. The minimum internal diameter will equal BOP bore.
- 2. Wear ring will be properly installed in head.
- 3. Blowout preventor and all associated fittings will be in operable condition and tested to 1000 psi with the rig pump.
- 4. All fittings will be flanged.
- 5. A full bore safety valve with proper thread connections will be available on the rotary rig floor at all times.
- 6. All choke lines will be anchored to prevent movement.
- 7. All BOP equipment will be equal to or larger in bore than the internal diameter of the last casing string.
- 8. Will maintain a Kelly cock attached to the Kelly.
- 9. Hand wheels and wrenches will be properly installed and tested for safe operation.
- 10. All BOP equipment will meet API standards and include a minimum 40 gallon accumulator having two independent means of power to initiate closing operation.
- 11. BOP will consist of a single annular preventor and a set of double rams as shown in Exhibit #1.



BEYOND SUBSTRUCTURE

			MINI	MUM REQL	HEMENT	5				
			3,000 MWP			5,000 MWP		10,000 MWP		,
No.		1,0,	NOMINAL	RATING	1.0.	NOMINAL	RATING	1.D.	NOMINAL	DAITAR
1	Line from drilling spool		3*	3,000		3-	5,000		3.	10,000
. 2	Cross 3"x3"x3"x2"			3,000			5,000			
	Crass 3"x3"x3"x3"									10,000
3	Valvos(1) Gate □ Plug □(2)	3-1/8-		3,000	3-1/8*		5,000	3-1/6"		10,000
4	Valve Gale □ (2)	1-13/16*		3,000	1-13/16*		5,000	1-13/16-		10,000
43	Valves(1)	2-1/16"		3,000	2-1/16°		5,000	3-1/8"		10,000
5	Pressure Gauge			3,000		1	5,000			10,000
6	Valves Plug ((2)	3-1/8"		3,000	3-1/8"		5,000 、	3-1/8"		10,000
7	Adjustable Choke(3)	2"		3,000	2.		5;000	2.	 	10,000
8	Adjustable Choke	1-		3,000	1"		5,000	2.	1	10,000
9	Line		, 3	3,000	[3-	5,000		3-	10,000
10	Line		2"	3,000		2.	5,000	i	3"	. 10,000
11	Valves Plug □(2)	3-1/8"	·	3,000	3-1/8"		5,000	3-1/8"		10,000
12	Lines		3,	1,000		3.	1,000		3"	2,000
13	Lines	·	3-	1,000		3-	1,000	•	3-	2,000
14	Remote reading compound standpipe pressure gauge			3,000			5,000	·		10,000
15	Gas Separator		2'x5'			2'x5'			2'x5'	
16	Line		4*	1,000		4-	1,000		4-	2,000
17	Valves Gate C	3-1/8"		3,000	3-1/8"		5,000	3-1/8*		10,000

- (1) Only one required in Class 3M.
- (2) Gate valves only shall be used for Class 10M.
- (3) Remote operated hydraulic choke required on 5,000 psi and 10,000 psi for drilling.

EQUIPMENT SPECIFICATIONS AND INSTALLATION INSTRUCTIONS

- 1. All connections in choke manifold shall be welded, studded, flanged or Cameron clamp of comparable rating.
- 2. All flanges shall be API 68 or 68X and ring gaskets shall be API RX or BX. Use only BX for 10 MWP.
- 3. All lines shall be securely anchored.
- 4. Chokes shall be equipped with tungsten carbide seats and needles, and replacements shall be available.
- 5. Choke manifold pressure and standpipe pressure gauges shall be available at the choke manifold to assist in regulating chokes. As an alternate with automatic chokes, a choke manifold pressure gauge shall be located on the rig floor in conjunction with the standpipe pressure gauge.
- Line from drilling spool to choke manifold should be as straight as possible. Lines downstream from chokes shall make turns by large bends or 90° bends using bull plugged toos.
- 7. Discharge lines from chokes, choke bypass and from top of gas apparator should vent as far as practical from the well.

3 MWP

STACK REQUIREMENTS

			Min.	Min.
No.	item	I.D.	Nominal	
1	Flowline			
2	Fill up line			2"
3	Drilling nipple			
4	Annular preventer			
5	Two single or one dual hy operaled rams	draulically		
6a	Drilling spool with 2" min. 3" min chake line outlets			
6b	2" min. kill line and 3" min outlets in ram. (Alternate t			
7	Valve	3-1/8"		
В	Gale valve—power opera	led	3-1/8"	
9	Line to choke manifold			3.
10	Valves	Gate 🗆 Plug 🗅	2-1/16"	
11	Check valve		2-1/16*	
12	Casing head			
13	Valve	Gate □ Plug □	1-13/16"	
14	Pressure gauge with need	die valve		·
15	Kill line to rig mud pump r	nanilold		2*

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@		<u> </u>	
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	PREVENTER], 0	
	ELIND HAME		
. @	PIPE RANS		
	DRILLING)
(1)	CASING	7 0	(P)
	HEAD CASING)
		•	•

CONFIGURATION

OPTIONAL						
16	Flanged valve	1-13/16"				

CONTRACTOR'S OPTION TO FURNISH:

- 1.All equipment and connections above bradenhead or casinghead. Working pressure of preventers to be 3,000 psl, minimum.
- Automatic accumulator (80 gallon, minimum) capable of closing BOP in 30 seconds or less and, holding them closed against full rated working pressure.
- 3.BOP controls, to be located near drillers position.
- 4. Kelly equipped with Kelly cock.
- 5.Inside blowout prevventer or its equivalent on derrick floor at all times with proper threads to fit pipe being used.
- 6.Kelly saver-sub equipped with rubber casing protector at all times.
- 7.Plug type blowout preventer tester.
- 8.Extra set pipe rams to fit drill pipe in use on location at all times.
- 9. Type RX ring gaskets in place of Type R.

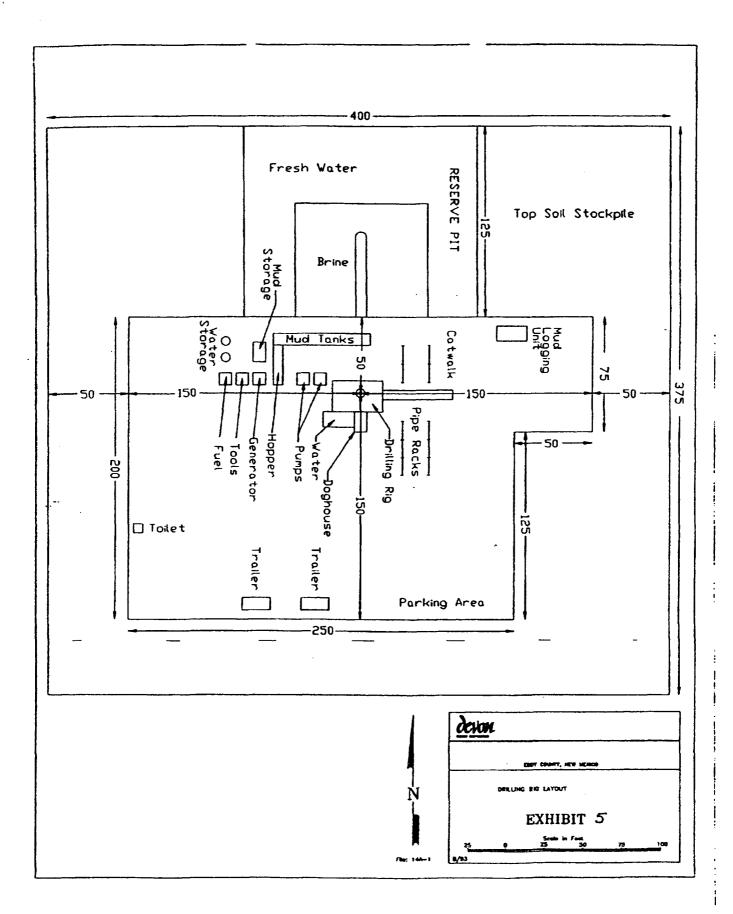
MEC TO FURNISH:

- Bradenhead or casinghead and side valves.
- 2. Wear bushing, II required.

GENERAL NOTES:

- Deviations from this drawing may be made only with the express permission of MEC's Drilling Manager.
- 2.All connections, valves, fittings, piping, etc., subject to well or pump pressure must be flanged (suitable clamp connections acceptable) and have minimum working pressure equal to rated working pressure of preventers up through chore. Valves must be full opening and suitable for high pressure mud service.
- Controls to be of standard design and each marked, showing opening and closing position.
- 4. Chokes will be positioned so as not to hamper or delay changing of choke beans. Replaceable parts for adjustable choke, other bean sizes, retainers, and choke wrenches to be conveniently located for immediate use.
- 5.All valves to be equipped with handwheels or handles ready for immediate
- 5. Choke lines must be suitably anchored.

- 7. Handwheels and extensions to be connected and ready for use.
- B. Valves adjacent to drilling apool to be kept open. Use outside valves except for emergency.
- 8.All seamless steel control piping (3000 psi working pressure) to have flexible joints to avoid stress. Hoses will be permitted.
- Casinghead connections shall not be used except in case of emergency.
- 11.Do not use kill line for routine fill-up operations.



DEVON ENERGY CORPORATION

HYDROGEN SULFIDE DRILLING OPERATIONS PLAN

A. Hydrogen Sulfide Training

All rig crews and company personnel will receive training from a qualified instructor in the following areas prior to penetrating any hydrogen sulfide bearing formations during drilling operations:

- 1. The hazards and characteristics of hydrogen sulfide (H2S).
- 2. The proper use and maintenance of the H2S safety equipment and of personal protective equipment to be utilized at the location such as H2S detection monitors, alarms and warning systems, and breathing equipment. Briefing areas and evacuation procedures will also be discussed and established.
- 3. Proper rescue techniques and procedures will be discussed and established.

In addition to the above, supervisory personnel will be trained in the prevention of oil and gas well blowouts in accordance with Minerals Management Service Standards Subpart - 0 - 250 - 212.

Prior to penetrating any known H2S bearing formation, H2S training will be required at the rig sight for all rig crews and company personnel that have not previously received such training. This instruction will be provided by a qualified instructor with each individual being required to pass a 20 question test regarding H2S safety procedures. All contract personnel employed on an unscheduled basis will be required to have received appropriate H2S training.

This Hydrogen Sulfide Drilling And Operations Plan shall be available at the wellsite during drilling operations.

B. H2S Safety Equipment And Systems

All H2S safety equipment and systems will be installed, tested, and operational when drilling operations reach a depth approximately 500' above any known or probable H2S bearing formation. The safety systems to be utilized during drilling operations are as follows:

1. Well Control Equipment

- (a) Double ram BOP with a properly sized closing unit and pipe rams to accommodate all pipe sizes in use.
- (b) A choke manifold with a minimum of one remote choke.

2. H2S Detection And Monitoring Equipment

- (a) Three (3) H2S detection monitors will be placed in service at the location. One monitor will be placed near the bell nipple on the rig floor; one will be placed at the rig substructure; and, one will be at the working mud pits or shale shaker. This monitoring system will have warning lights and audible alarms that will alert personnel when H2S levels reach 10 ppm.
- (b) One (1) Sensidyne Pump with the appropriate detection tubes will also be available to perform spot checks for H2S concentrations in any remote or isolated areas.

3. Protective Equipment For Essential Personnel

Protective equipment will consist of the following:

- (a) Four (4) five minute escape packs located at strategic points around the rig.
- (b) Two (2) thirty minute rescue packs to be located at the designated briefing areas.

4. Visual Warning System

Visual warning system will consist of the following:

- (a) Two wind direction indicators.
- (b) One condition / warning sign which will be posted on the road providing direct access to the location. The sign will contain lettering of sufficient size to be readable at a reasonable distance from the immediate location. The sign will inform the public that a hydrogen sulfide gas environment could be encountered at the location.

DEVON ENERGY COPPURATION Hydrogen Sulfide Drilli. Operations Plan

5. Mud Program

(a) The mud program has been designed to minimize the volume of H2S circulated to surface. Proper mud weight and safe drilling practices (for example, keeping the hole filled during trips) will minimize hazards when drilling in H2S bearing formations.

6. Metallurgy

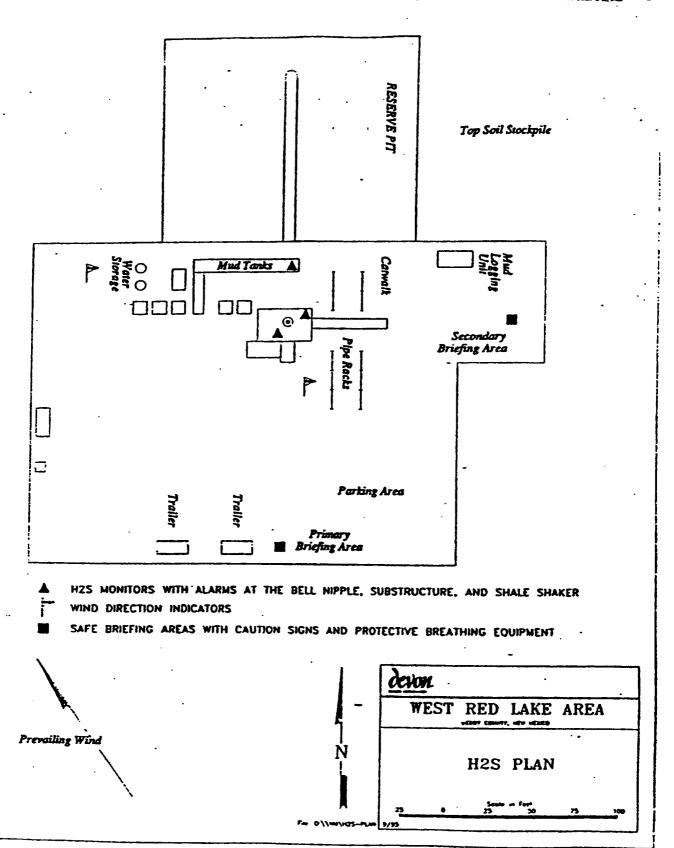
(a) All drill strings, casings, tubing, wellhead, blowout preventers, drilling spools, kill lines, choke manifold and lines, and valves shall be suitable for H2S service.

7. Communication

(a) Two way radio and cellular telephone communication will be available in company vehicles.

C. Diagram of Drilling Location

1. Attached is a diagram representing a typical location layout as well as the location of H2S monitors, briefing areas, and wind direction indicators.



Well name:

Operator:

Devon Energy

String type:

Surface

Location:

New Mexico

Design parameters:			Minimum design factors: Collapse:			Environme	No		
Mud	Collapse Mud weight: 9.000 ppg Design is based on evacuated pipe.		Design factor 1.125			Surface tem Bottom hole Temperature Minimum se	75 °F		
Burst				Burst: Design fac	tor	1.00	Miniman 30	ouon longui.	020 K
Max	anticipated : essure:	surface	332 psi						
	Internal gradient: 0.433 psi/ft		Tension:			Non-directio	nal string.		
Calculated BHP 601 psi		8 Round STC: 1		1.80 (J)		ŭ			
,			8 Round LTC: 1.80 (J) Buttress: 1.60 (J)						
No backup mud specified.									
			Premium: 1.50 (J)						
			Body yield: 1.60 (B)			Re subsequent strings:			
						Next set	3,840 ft		
				Tension is based on air weight. Neutral point: 538 ft			Next mud weight: Next setting BHP: Fracture mud wt: Fracture depth: Injection pressure		10.000 ppg
			1,995 psi						
			15.000 ppg 3.840 ft						
			2,992 psi						
							mjection	piessule	2,992 psi
Run	Segment		Nominal		End	True Vert	Measured	Drift	Est.
Seq	Length	Size	Weight	Grade	Finish	Depth	Depth	Diameter	Cost
	(ft)	(in)	(lbs/ft)			(ft)	(ft)	(in)	(\$)
1	620	13.375	48.00	H-40	ST&C	620	620	12.59	7689
Run	Collapse	Collapse	Collapse	Burst	Burst	Burst	Tension	Tension	Tension

Strength

(psi)

1730

Design

Factor

2.88

Load

(kips)

29.8

Devon Energy

Strength

(psi)

740

Design

Factor

2.55

Load

(psi)

601

Date: June 26,2003 Oklahoma City, Oklahoma

Strength

(kips)

322

Design

Factor

10.82 J

Remarks:

Seq

1

Load

(psi)

290

Collapse is based on a vertical depth of 620 ft, a mud weight of 9 ppg. The casing is considered to be evacuated for collapse purposes. Collapse strength is based on the Westcott, Dunlop & Kemler method of biaxial correction for tension.

Burst strength is not adjusted for tension.

Well name:

Operator:

Devon Energy

String type:

Intermediate

Location:

New Mexico

Design parameters:				Minimum design factors:			Environment:			
Collapse			Collapse:			H2S conside	No 75 °F			
Mud weight: 10.000 ppg Design is based on evacuated pipe.				Design fac	ctor	1.125	Temperature	temperature:		
				Burst:				3		
				Design factor 1.00						
	anticipated	surface	050							
pressure: 353 psi Internal gradient: 0.433 psi/ft Calculated BHP 2,016 psi			Tension:			Non directio	and string			
			8 Round STC: 1.80 (J) 8 Round LTC: 1.80 (J)			Non-directional string.				
									No t	No backup mud specified.
				Premium: 1.50 (J)						
				Body yield: 1.60 (B)			Re subsequent strings:			
							Next set	7,860 ft		
				Tension is based on air weight. Neutral point: 3,270 ft			Next mud weight: Next setting BHP:		9.200 ppg	
									3,756 psi	
							Fracture mud wt:		15.000 ppg	
							Fracture	•	3,840 ft	
							Injection	pressure	2,992 psi	
Run	Segment		Nominal		End	True Vert	Measured	Drift	Est.	
Seq	Length	Size	Weight	Grade	Finish	Depth	Depth	Diameter	Cost	
	(ft)	(in)	(ibs/ft)			(ft)	(ft)	(in)	(\$)	
1	3840	8.625	32.00	J-55	LT&C	3840	3840	7.875	30945	
Run	Collapse	Collapse	Collapse	Burst	Burst	Burst	Tension	Tension	Tension	
Seq	Load	Strength	Design	Load	Strength	Design	Load	Strength	Design	
	(psi)	(psi)	Factor	(psi)	(psi)	Factor	(kips)	(kips)	Factor	
4	4005	2620	1 27	2010	2020	4.05	400.0	447	2.20	

3930

1.95

122.9

Devon Energy

2530

1.27

2016

Date: June 26,2003 Oklahoma City, Oklahoma

417

3.39 J

Collapse is based on a vertical depth of 3840 ft, a mud weight of 10 ppg. The casing is considered to be evacuated for collapse purposes. Collapse strength is based on the Westcott, Dunlop & Kemler method of biaxial correction for tension.

Burst strength is not adjusted for tension.

Remarks:

1995

Well name:

Operator:

Devon Energy

String type:

Production

Location:

New Mexico

Design parameters:

Collapse

Burst

Mud weight:

9.200 ppg

Design is based on evacuated pipe.

Minimum design factors:

Collapse:

Design factor 1.125 **Environment:**

H2S considered?

No 75 °F

Surface temperature: Bottom hole temperature:

186 °F

Temperature gradient:

1.40 °F/100ft

Burst:

Design factor

1.00

1.80 (J) 1.80 (J)

1.60 (J)

Minimum section length: 620 ft

358 psi

Internal gradient: 0.433 psi/ft Calculated BHP

Max anticipated surface pressure:

3,804 psi

No backup mud specified.

Buttress:

Premium:

Tension:

Body yield:

8 Round STC:

8 Round LTC:

1.50 (J) 1.60 (B)

Tension is based on air weight. Neutral point: 6,840 ft

Estimated cost:

28,401 (\$)

Non-directional string.

Run	Segment		Nominal		End	True Vert	Measured	Drift	Est.	-
Seq	Length	Size	Weight	Grade	Finish	Depth	Depth	Diameter	Cost	
	(ft)	(in)	(lbs/ft)			(ft)	(ft)	(in)	(\$)	
3	100	5.5	17.00	J-55	LT&C	100	100	4.767	387	
2	7100	5.5	15.50	J-55	LT&C	7200	7200	4.825	25070	
1	760	5.5	17.00	J-55	LT&C	7960	7960	4.767	2944	
Run	Collapse	Collapse	Collapse	Burst	Burst	Burst	Tension	Tension	Tension	
Seq	Load	Strength	Design	Load	Strength	Design	Load	Strength	Design	
	(psi)	(psi)	Factor	(psi)	(psi)	Factor	(kips)	(kips)	Factor	
3	48	3881	81.20	401	5320	13.27	124.7	247	1.98 J	
2	3441	3989	1.16	3475	4810	1.38	123	217	1.76 J	
1	3804	4910	1.29	3804	5320	1.40	12.9	247	19.12 J	

Devon Energy

Date: July 1,2003 Oklahoma City, Oklahoma

Remarks:

Collapse is based on a vertical depth of 7960 ft, a mud weight of 9.2 ppg. The casing is considered to be evacuated for collapse purposes. Collapse strength is based on the Westcott, Dunlop & Kemler method of biaxial correction for tension.

Burst strength is not adjusted for tension.