Submit in duplicate to appropriate district office.
See Rule 401 & Rule 1122

State of New Mexico
Energy Minerals and Natural Resources
Oil Conservation Division
2040 South Pacheco
Santa Fe, NM 87505

Form C-122
Revised October, 1999

30-015-32808

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Operator	UNIT PET. CO.				Lease or Unit Name		HARROUN COM		
Type Test: ☑ Initial ☐ Annual ☐ Special					Test Date: 12/17/03		Well No.: 2		
Completion Date: 10/4/03	Total Depth: 12720			Plug Back TD: 12672		Elevation: 3027 GL	Unit Ltr - Sec - TWP - Rge: D 33 22S 28E		
Csg. Size: 4 1/2	Wt.: 13.5	d: 3.92	Set At: 12720	Perforations: From: 12105	To: 12250		County: EDDY		
Tbg. Size: 2 3/8	Wt.: 4.7	d: 1.995	Set At: 11900	Perforations: From:	To:		Pool: DUBLIN RANCH-MORROW GAS		
Type Well-Single-Bradenhead-G.G. or G.O. Multiple: SINGLE				Packer Set At: 11900			Formation: MORROW		
Producing Thru: TUBING	Reservoir Temp.: 202	Mean Annual Temp.: 60		Baro. Press.-P_a: 13.2			Connection: SALES		
L: 11900	H: 11900	Gg: 0.5789	%CO_2: 1.784	%N_2: 0.2889	%H_2S:	Prover:	Meter Run: 2.067		Taps: FLG

	FLOW DATA				TUBING DATA		CASING DATA		
No.	Prover Line Size x Orifice Size	Press p.s.i.g.	Diff. h_w	Temp.	Press p.s.i.g.	Temp.	Press p.s.i.g.	Temp.	Duration of Flow
SI					3275				
1	2.067 X 1.125	600	43	70	2200				24 HRS
2									
3									
4									
5									

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RATE OF FLOW CALCULATIONS

No.	COEFFICIENT (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor F_g	Super Compress Factor F pv	Rate of Flow Q. Mcfd
1							1030
2	TOTAL	FLOW	METER				
3							
4							
5							

No.	P_r	Temp. R	T_r	Z
1				
2				
3	TOTAL	FLOW	METER	
4				
5				

Gas Liquid Hydrocarbon Ratio: N/A Mcf/bbl.
A.P. I. Gravity of Liquid Hydrocarbons: N/A Deg.
Specific Gravity Separator Gas: 0.5789 XXXXXXX
Specific Gravity Flowing Fluid: XXXXX
Critical Pressure: 677 P.S.I.A. ____ P.S.I.A.
Critical Temperature: 353 R. ____ R

P_c 3288.2 P_c^2 10812.2

No.	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1		2222.5	4939.4	5872.8
2				
3				
4				
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} =$ 1.841 (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n =$ 1.481

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n =$ 1.896

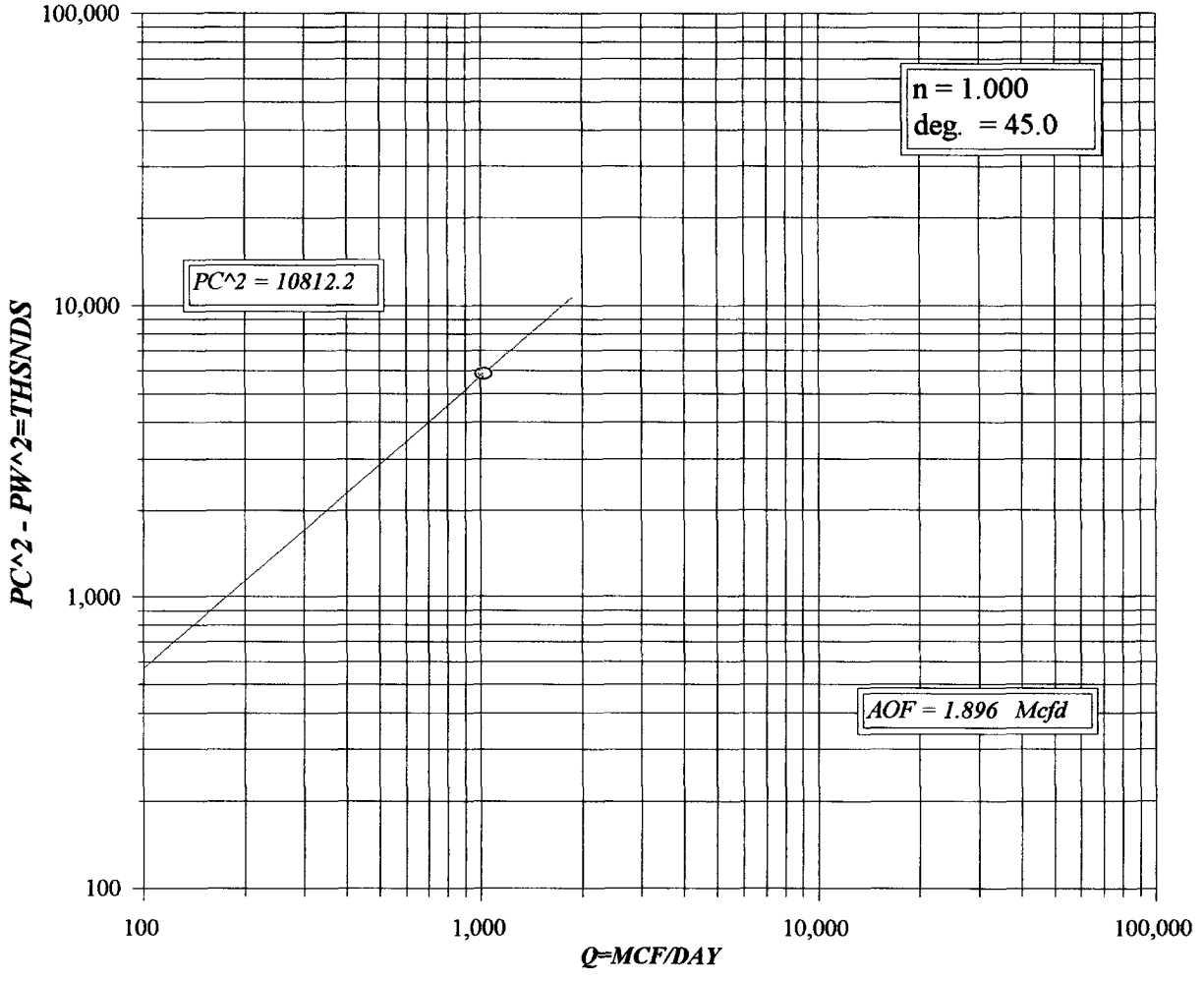
Absolute Open Flow: 1.896 Mcfd @ 15.025 | Angle of Slope (): 45 | Slope n: 1

Remarks:

Approved By Division:	Conducted By:	Calculated By:	Checked By:
	PRO WELL TESTING	MERV BUECKER	BM

UNIT PET. CO.

HARROUN COM #2



C122D FORM IMPORTED FROM SYMPHONY ON 9-9-01

COMPANY :	UNIT PET.CO.		LEASE :	HARROUN COM		WELL NO. :	2		Pc =	3288.2	Pc2 =	10812.2	
UNIT :	B		SECTION :	33		TOWNSHIP :	22S						
L :	11900	H :	11900	L/H :	1	G/GMIX :	0.579		Pt2 =	4898.3	Pw =	2222.5	
%CO2 :	1.784	%N2 :	0.2889	H2S :			DATE :	01/00/00		0.0		#DIV/0!	
d :	1.995	Fr :	0.018183	GH :	8197.0		RANGE :	28E		0.0		#DIV/0!	
										0.0		#DIV/0!	
VOL 1 :	1030	PSIA 1 :	2213.2			RESV.TEMP	202.0						
VOL 2 :		PSIA 2 :							Pc2-Pw2=	5872.8	Pw2 =	4939.4	
VOL 3 :		PSIA 3 :				SHUT-IN PRES =	3288.2			#DIV/0!		#DIV/0!	
VOL 4 :		PSIA 4 :								#DIV/0!		#DIV/0!	
			PCR :	679									
			TCR :	348						n =	1.000		
									Pc2/(Pc2-Pw2) =		1.841		
											#DIV/0!		
											#DIV/0!		
											#DIV/0!		
LINE	RATE 1		RATE 2		RATE 3		RATE 4						
	1ST	2ND	1ST	2ND	1ST	2ND	1ST	2ND					
1 QM	1.030	1.030	0.000	0.000	0.000	0.000	0.000	0.000					
2 TW	534	534	534	534	534	534	534	534	[Pc2/Pc2-Pw2]n =		1.841		
3 Ts	662.0	662.0	662.0	662.0	662.0	662.0	662.0	662.0			#DIV/0!		
4 T	598.0	598.0	598.0	598.0	598.0	598.0	598.0	598.0			#DIV/0!		
PR (est)	3.26		0.00		0.00		0.00				#DIV/0!		
5 Z(est)	0.849	0.850	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!					
6 TZ	507.4	508.0	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!		AOF= Q	1.896		
7 GH/TZ	16.153	16.135	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!			#DIV/0!		
8 eS	1.833	1.831	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!			#DIV/0!		
9 I-e-S	0.454	0.454	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!			#DIV/0!		
10 Pt	2213.2	2213.2	0.0	0.0	0.0	0.0	0.0	0.0					
11 Pt2 /1000	4898.3	4898.3	0.0	0.0	0.0	0.0	0.0	0.0					
12 Fr	0.018183	0.018183	0.018183	0.018183	0.018183	0.018183	0.018183	0.018183					
13 Fc=FrTZ	9.227	9.238	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!					
14 FcQm	9.50	9.51	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!					
15 L/H(FcQm)2	90.3	90.5	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!					
16 Fw	41.0362	41.096425	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!					
17 Pw2	4939.3	4939.4	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!					
18 Ps2	9051.9	9045.7	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!					
19 Ps	3008.6	3007.6	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!					
20 P	2610.9	2610.4	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!					
21 Pr	3.85	3.84	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!					
22 Tr	1.72	1.72	1.72	1.72	1.72	1.72	1.72	1.72					
23 Z	0.850	0.850	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!			FORM C122-D		