

AUG 28 1978

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELLForm C-122
Revised 9-1-65O. C. C.
ARTESIA, OFFICE

Type Test ☒ Initial ☐ Annual ☐ Special		Test Date 8/15/78		SPUD DATE: 7-16-78							
Company McClellan Oil Corporation		Connection None		Unit							
Pool Sams Ranch <i>Grayburg</i>		Formation Premier Sands		Farm or Lease Name McClellan Federal							
Completion Date 8-10-78		Total Depth 1825		Plug Back TD 3594.1 GL							
Csg. Size 4 1/2	Wt. 9.5	d Set At 1790	Perforations: From 1790 To 1825		Well No. 1						
Tqg. Size None	Wt.	d Set At	Perforations: From To		Unit Sec. Twp. Rye. 11 14 28						
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single			Packer Set At None		County Chaves						
Producing Thru		Reservoir Temp. *F @		Mean Annual Temp. *F Baro. Press. - P _a 13.2							
Csg. L	H 1790	Gg 716 (Assumed)	% CO ₂	% N ₂	% H ₂ S						
Prover		Meter Run		Taps							
FLOW DATA			TUBING DATA		CASING DATA						
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. hw	Temp. *F	Press. p.s.i.g.	Temp. *F	Press. p.s.i.g.	Temp. *F	Duration of Flow
SI	6" Positive Cks.										72 hrs.
1.	1/8		901	82			901				20 Min.
2.	9/64		882	84			882				60 Min.
3.	11/64		824	84			824				60 Min.
4.	13/64		710	78			710				60 Min.
5.											
RATE OF FLOW CALCULATIONS											
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd				
1	.2618		914.2	.9795	1.182	1.096	304				
2	.3346		895.2	.9777	1.182	1.094	379				
3	.5090		837.2	.9777	1.182	1.088	536				
4	.7208		723.2	.9831	1.182	1.075	651				
5											
NO.		P _r	Temp. *R	T _r	Z	Gas Liquid Hydrocarbon Ratio None Mcf/bbl.		Dry Gas			
1.		1.37	542	1.37	.832	A.P.I. Gravity of Liquid Hydrocarbons		Deg.			
2.		1.34	544	1.38	.835	Specific Gravity Separator Gas .716 (Assu.)		X X X X X X X X			
3.		1.25	544	1.38	.845	Specific Gravity Flowing Fluid X X X X X		P.S.I.A. P.S.I.A.			
4.		1.08	538	1.36	.865	Critical Pressure 668		R R			
5.						Critical Temperature 395					
NO.		P _c	P _w	P _w ²	P _c ² - P _w ²	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 3.280$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2.958$					
1				835.8	172.6	AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.586$					
2				801.4	207.0						
3				701.0	307.4						
4				523.2	485.2						
5											
Absolute Open Flow		1.586 Mcfd @ 15.025				Angle of Slope θ		47.5		Slope, n .913	
Remarks:											
Conducted By:				Calculated By:				Checked By:			

McCLELLAN OIL CORPORATION

McClellan Federal No. 1

0-11-14-28

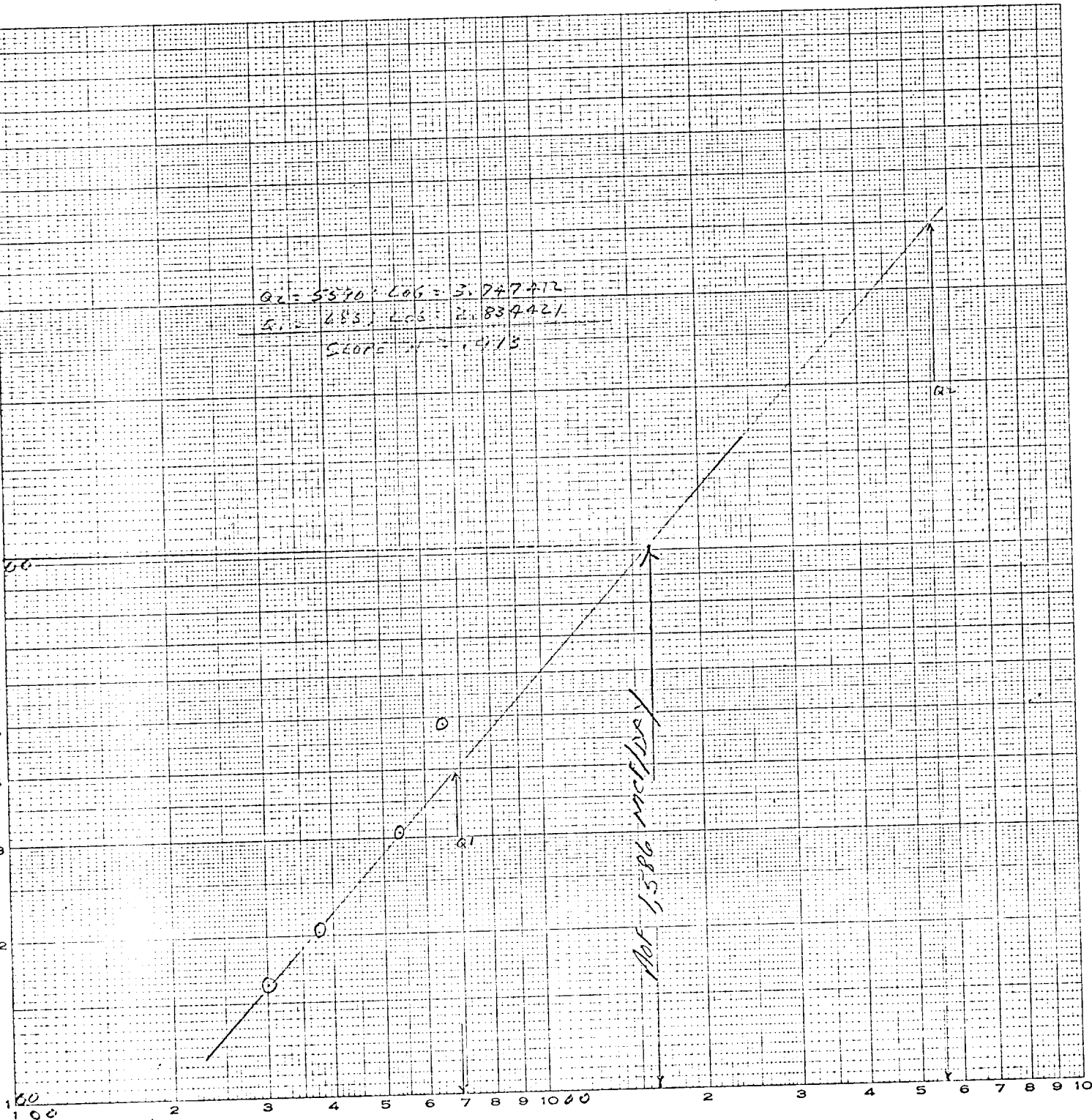
Chaves County, New Mexico

August 10, 1978

DIETZEN CORPORATION
MADE IN U.S.A.
P2-102 IN THSND'S

NO. 341-L22 DIETZEN GRAPH PAPER
LOGARITHMIC
2 CYCLES X 2 CYCLES

$Q_2 = 5370$ $\log = 3.747412$
 $Q_1 = 685$ $\log = 2.834421$
SLOPE $m = 1.013$



Q=MCF/D