

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

RECEIVED

|                                                                                                                           |  |                                 |  |                                            |  |                                        |  |
|---------------------------------------------------------------------------------------------------------------------------|--|---------------------------------|--|--------------------------------------------|--|----------------------------------------|--|
| Type Test<br><input checked="" type="checkbox"/> Initial <input type="checkbox"/> Annual <input type="checkbox"/> Special |  |                                 |  | Test Date<br>11-2-81                       |  | DEC 15 1981                            |  |
| Company<br>Yates Petroleum Corporation                                                                                    |  |                                 |  | Connection<br>Transwesten Pipeline Company |  | O. C. D.                               |  |
| Pool<br>Pecos Slope - Abo Gas<br><del>Undesignated Abo</del>                                                              |  |                                 |  | Formation<br>Abo                           |  | Unit<br>ARTESIA, OFFICE                |  |
| Completion Date<br>6-22-81                                                                                                |  | Total Length<br>4300'           |  | Plug Back TD<br>4296'                      |  | Elevation<br>3835'                     |  |
| Casing Size<br>4-1/2"                                                                                                     |  | Wt.<br>9.5#                     |  | Set At<br>4297                             |  | Perforations:<br>From 3753 To 3997     |  |
| Tubing Size<br>2-3/8"                                                                                                     |  | Wt.<br>4.7#                     |  | Set At<br>3690'                            |  | Perforations:<br>From - To -           |  |
| Type Well - Single - Bradenhead - C.G. or G.O. Multiple<br>Single                                                         |  |                                 |  | Packer Set At<br>-                         |  | County<br>Chaves                       |  |
| Producing Thru<br>tubing                                                                                                  |  | Reservoir Temp. °F<br>96 @ 3875 |  | Mean Annual Temp. °F<br>62                 |  | Base Press. - P <sub>atm</sub><br>13.2 |  |
| L<br>3900                                                                                                                 |  | H<br>3900                       |  | G <sub>g</sub><br>.652                     |  | % CO <sub>2</sub><br>0.92              |  |
|                                                                                                                           |  |                                 |  | % N <sub>2</sub><br>4.92                   |  | % H <sub>2</sub> S<br>0                |  |
|                                                                                                                           |  |                                 |  | Prover<br>-                                |  | Meter Run<br>2"                        |  |
|                                                                                                                           |  |                                 |  |                                            |  | Taps<br>Flanged                        |  |

| FLOW DATA |                        |   |                 |                    |             | TUBING DATA |                    | CASING DATA |                    | Duration<br>of<br>Flow |             |
|-----------|------------------------|---|-----------------|--------------------|-------------|-------------|--------------------|-------------|--------------------|------------------------|-------------|
| NO.       | Prover<br>Line<br>Size | X | Orifice<br>Size | Press.<br>p.s.i.g. | Diff.<br>hw | Temp.<br>°F | Press.<br>p.s.i.g. | Temp.<br>°F | Press.<br>p.s.i.g. |                        | Temp.<br>°F |
| SI        |                        |   |                 |                    |             |             | 1000               |             |                    |                        | days        |
| 1.        | 2.067                  | x | .875            | 310                | 83.0        | 75          | 590                | 67          |                    |                        | 24 hrs      |
| 2.        | 2.067                  | x | .875            | 320                | 47.7        | 75          | 707                | 67          |                    |                        | 24 hrs      |
| 3.        | 2.067                  | x | .875            | 325                | 28.8        | 75          | 783                | 67          |                    |                        | 24 hrs      |
| 4.        | 2.067                  | x | .875            | 330                | 12.3        | 75          | 867                | 67          |                    |                        | 24 hrs      |
| 5.        |                        |   |                 |                    |             |             |                    |             |                    |                        |             |

RATE OF FLOW CALCULATIONS

| NO. | Coefficient<br>(24 Hour) | $\sqrt{h_w P_m}$ | Pressure<br>P <sub>m</sub> | Flow Temp.<br>Factor<br>F <sub>t</sub> | Gravity<br>Factor<br>F <sub>g</sub> | Super<br>Compress.<br>Factor, F <sub>sp</sub> | Rate of Flow<br>Q, Mcf/d |
|-----|--------------------------|------------------|----------------------------|----------------------------------------|-------------------------------------|-----------------------------------------------|--------------------------|
| 1   | 3.729                    | 163.8            | 323.2                      | .9859                                  | 1.238                               | 1.027                                         | 766                      |
| 2   | 3.729                    | 126.1            | 333.2                      | .9859                                  | 1.238                               | 1.027                                         | 589                      |
| 3   | 3.729                    | 98.7             | 338.2                      | .9859                                  | 1.238                               | 1.028                                         | 461                      |
| 4   | 3.729                    | 65.0             | 343.2                      | .9859                                  | 1.238                               | 1.028                                         | 304                      |
| 5   |                          |                  |                            |                                        |                                     |                                               |                          |

| NO. | P <sub>t</sub> | Temp. °R | T <sub>r</sub> | Z    | Gas Liquid Hydrocarbon Ratio<br>A.P.I. Gravity of Liquid Hydrocarbons | Super<br>Compress.<br>Factor, F <sub>sp</sub> | Rate of Flow<br>Q, Mcf/d |
|-----|----------------|----------|----------------|------|-----------------------------------------------------------------------|-----------------------------------------------|--------------------------|
| 1   | .49            | 535      | 1.49           | .949 | Dry                                                                   | 1.027                                         | 766                      |
| 2   | .50            | 535      | 1.49           | .948 | Dry                                                                   | 1.027                                         | 589                      |
| 3   | .51            | 535      | 1.49           | .947 | Dry                                                                   | 1.028                                         | 461                      |
| 4   | .52            | 535      | 1.49           | .946 | Dry                                                                   | 1.028                                         | 304                      |
| 5   |                |          |                |      |                                                                       |                                               |                          |

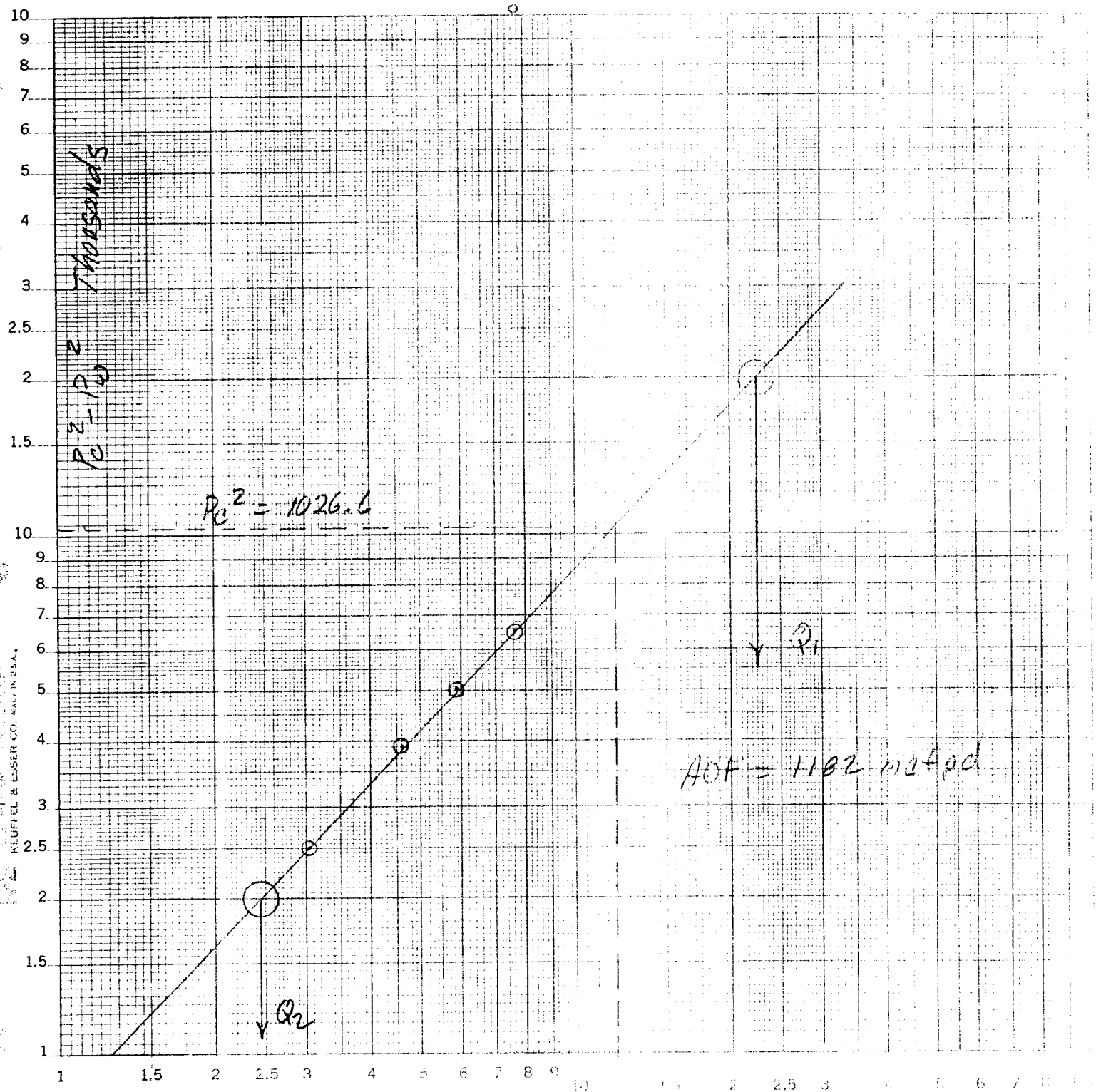
| NO. | P <sub>t</sub> <sup>2</sup> | P <sub>w</sub> | P <sub>w</sub> <sup>2</sup> | P <sub>t</sub> <sup>2</sup> - P <sub>w</sub> <sup>2</sup> | (1) $\frac{P_t^2}{P_t^2 - P_w^2} =$ | (2) $\left[ \frac{P_t^2}{P_t^2 - P_w^2} \right]^n =$ |
|-----|-----------------------------|----------------|-----------------------------|-----------------------------------------------------------|-------------------------------------|------------------------------------------------------|
| 1   | 363.9                       |                | 372.1                       | 654.5                                                     | 4.0966                              | 3.8883                                               |
| 2   | 518.7                       |                | 523.5                       | 503.1                                                     |                                     |                                                      |
| 3   | 633.9                       |                | 636.8                       | 389.8                                                     |                                     |                                                      |
| 4   | 774.8                       |                | 776.0                       | 250.6                                                     |                                     |                                                      |
| 5   |                             |                |                             |                                                           |                                     |                                                      |

Absolute Open Flow 1182 Mcf/d @ 15.025 Angle of Slope 4° Slope, n .963

Remarks:

|                      |                               |                               |             |
|----------------------|-------------------------------|-------------------------------|-------------|
| Approved By Division | Conducted By:<br>David Weaver | Calculated By:<br>Al Springer | Checked By: |
|----------------------|-------------------------------|-------------------------------|-------------|

Yates Petroleum Corp.  
 Hahn "NH" Fed. #2  
 Unit A, sec 9, T-15, R-25E  
 Chaves County, New Mexico



$$(P_e^2 - P_w^2)_1 = 2000$$

$$(P_e^2 - P_w^2)_2 = 200$$

$$Q_1 = 2,250$$

$$Q_2 = 245$$

$$\log Q_1 = 3.35218$$

$$\log Q_2 = 2.38914$$

$$n = .963 \quad .963$$

COMPANY Nates Petroleum Corp. LEASE Hahn "NH" Fed WELL NO. #2 DATE 12/11/81

LOCATION: Unit A Section 3 Township 9S Range 25E

L 3900 H 3900 L/H 1.000 G 0.652 % CO<sub>2</sub> 0.92 % N<sub>2</sub> 4.92 % H<sub>2</sub>S 0

d 1.995 F<sub>1</sub> .01823 GH 2542 P<sub>CI</sub> 665 T<sub>CI</sub> 360

TABLE IX B X

| LINE                                                                                      | Rate #1 | Rate #2 | Rate #3 | Rate #4 |  |  |  |  |
|-------------------------------------------------------------------------------------------|---------|---------|---------|---------|--|--|--|--|
| 1 Q <sub>m</sub>                                                                          | .766    | .589    | .461    | .304    |  |  |  |  |
| 2 T <sub>w</sub> (W.H. °H)                                                                | 52.1    | 52.7    | 52.7    | 52.7    |  |  |  |  |
| 3 T <sub>s</sub> (B.H. °R)                                                                | 556     | 556     | 556     | 556     |  |  |  |  |
| 4 T = ( $\frac{1}{W} + \frac{1}{S}$ )                                                     | 541.5   | 541.5   | 541.5   | 541.5   |  |  |  |  |
| 5 D (Est.)                                                                                | .905    | .890    | .899    | .869    |  |  |  |  |
| 6 T <sub>D</sub>                                                                          | 490.06  | 481.94  | 475.98  | 470.56  |  |  |  |  |
| 7 GH-TZ                                                                                   | 5.1871  | 5.275   | 5.3406  | 5.4020  |  |  |  |  |
| 8 e <sup>s</sup> (Table XIV)                                                              | 1.215   | 1.219   | 1.222   | 1.225   |  |  |  |  |
| 9 1-e <sup>s</sup> (Table XIV)                                                            | .177    | .180    | .182    | .184    |  |  |  |  |
| 10 F <sub>1</sub>                                                                         | 603.2   | 720.2   | 796.2   | 880.2   |  |  |  |  |
| 11 P <sub>1</sub> = 1000                                                                  | 363.85  | 518.7   | 633.9   | 794.75  |  |  |  |  |
| 12 F <sub>1</sub> (Table XV)                                                              | .01823  | .01823  | .01823  | .01823  |  |  |  |  |
| 13 F <sub>1</sub> = F <sub>1</sub> T <sub>1</sub>                                         | 8.9337  | 8.7857  | 8.6771  | 8.5784  |  |  |  |  |
| 14 F <sub>1</sub> = F <sub>1</sub>                                                        | 6.8133  | 5.1748  | 4.0001  | 2.6078  |  |  |  |  |
| 15 L/H (F <sub>1</sub> Q <sub>m</sub> ) <sup>2</sup>                                      | 46.8301 | 26.778  | 16.0011 | 6.8008  |  |  |  |  |
| 16 F <sub>1</sub> = L/H (F <sub>1</sub> Q <sub>m</sub> ) <sup>2</sup> (1-e <sup>s</sup> ) | 8.2889  | 4.8201  | 2.9122  | 1.2513  |  |  |  |  |
| 17 P <sub>w</sub> <sup>2</sup> = P <sub>1</sub> <sup>2</sup> + F <sub>w</sub>             | 372.1   | 523.5   | 636.8   | 776.00  |  |  |  |  |
| 18 F <sub>1</sub> <sup>2</sup> = e <sup>s</sup> P <sub>w</sub> <sup>2</sup>               | 452.1   | 638.2   | 778.2   | 950.60  |  |  |  |  |
| 19 P <sub>3</sub>                                                                         | 672.4   | 798.8   | 882.17  | 974.91  |  |  |  |  |
| 20 P = ( $\frac{F_1}{2} + F_3$ )                                                          | 531.8   | 759.5   | 834.19  | 927.59  |  |  |  |  |
| 21 P <sub>1</sub> = P/P <sub>3</sub>                                                      | .76     | 1.14    | 1.26    | 1.39    |  |  |  |  |
| 22 T <sub>1</sub> = (T/T <sub>1</sub> ) <sup>1.5</sup>                                    | 1.50    | 1.50    | 1.50    | 1.50    |  |  |  |  |
| 23 Z (Table XI)                                                                           | .905    | .890    | .879    | .869    |  |  |  |  |