MULTI-POINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

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NOV 9 1982

O. C. D.
ARTESIA, OFFICE

Type Test: [X] Initial FOUR POINT [ ] Annual [ ] Special — Test Date: 11-2-82

Company: STEVENS OPERATING	Connection: AIR NEW WELL		Unit: G
Pool: PECOS SLOPE ~~U.D.~~	Formation: ABO		
Completion Date: ~~10-26-82~~ 11-5-82	Total Depth: 4470	Plug Back TD: ~~4400~~ 4470	Elevation: ~~3583~~ 3595
Farm or Lease Name: DIAMOND A			
Csg. Size: 4.500 / Wt.: 11.6 / d: 4.000 / Set At: ~~4970~~ 4470	Perforations: From 3898 To 4033		Well No.: 1
Tbg. Size: 2.375 / Wt.: 4.7 / d: 1.995 / Set At: ~~3903~~ 3806	Perforations: From OPEN To ENDED		Unit: G / Sec.: ~~29~~ 28 / Twp.: 7W / Rge.: 26E
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: SINGLE	Packer Set At: NONE		County: CHAVES
Producing Thru: TUBING	Reservoir Temp. °F: 113 @ 3965	Mean Annual Temp. °F: 60°	Baro. Press. – P_a: 13.2
			State: NEW MEXICO

L	H	G_g	% CO_2	% N_2	% H_2S	Prover	Meter Run	Taps
3965	3965	0.642	0.09	6.58	0	2.0	0	

NO.	FLOW DATA: Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	TUBING DATA: Press. p.s.i.g.	Temp. °F	B.H.P. DATA: Press. p.s.i.g.	CHOKE	Duration of Flow
SI							998		1112		73.2
1	2.00	X	0.375	105	0	37	902	49	1075	14/64	1 HR
2	2.00	X	0.375	290	0	40	882	49	993	17/64	1 HR
3	2.00	X	0.375	395	0	50	777	48	879	18.5/64	1 HR
4	2.00	X	0.375	455	0	51	672	47	772	19.5/64	1 HR
5											

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	2.37	0	118.2	1.0229	1.2483	1.0116	362
2	2.37	0	303.2	1.0198	1.2483	1.0301	944
3	2.37	0	408.2	1.0098	1.2483	1.0383	1268
4	2.37	0	468.2	1.0088	1.2483	1.0435	1460
5							

NO.	P_r	Temp. °R	T_r	Z
1	0.18	497	1.41	0.977
2	0.46	500	1.41	0.942
3	0.62	510	1.44	0.928
4	0.71	511	1.45	0.918
5				

Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
Specific Gravity Separator Gas 0.642 XXXXXXXXXX
Specific Gravity Flowing Fluid XXXXX
Critical Pressure 659 P.S.I.A. _____ P.S.I.A.
Critical Temperature 353 R _____ R

P_t 1017.2 P_c^2 1035.

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1	1184	984	968	66
2	1012	911	830	205
3	796	809	654	380
4	617	713	508	527
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.9647$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1.5734$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 2297.$

Post ID-2 7-22-83 Comp + RK

Absolute Open Flow 2297. Mcfd @ 15.025 — Angle of Slope θ 56.1 — Slope, n 0.671

Remarks: BOTTOM HOLE PRESSURE MEASURED WITH AMERADA PRESSURE ELEMENTS.

Approved By Commission:	Conducted By:	Calculated By:	Checked By:
	DON BENNETT	BENNETT-CATHEY	

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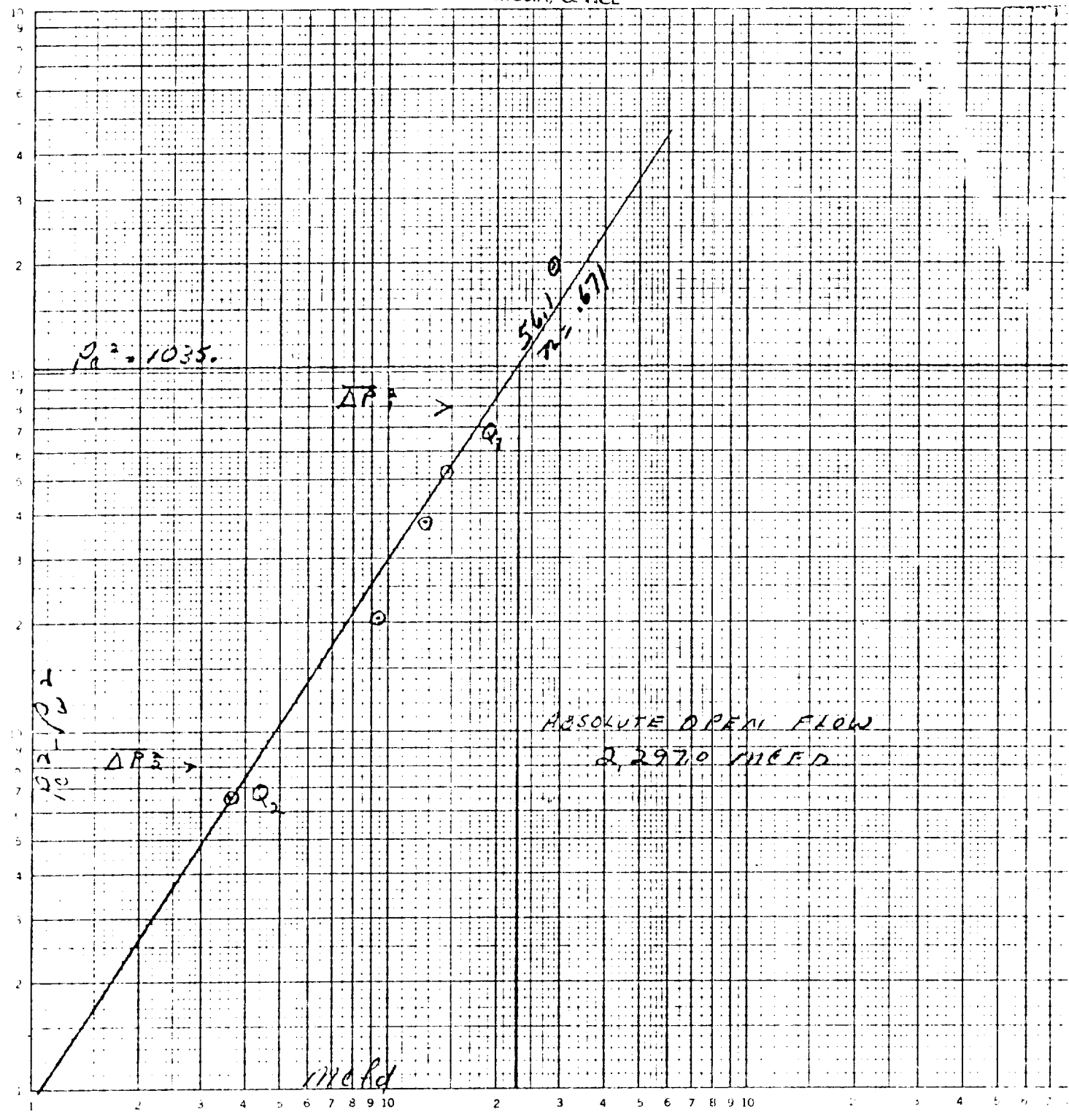
O. C. D.
ARTESIA, OFFICE

UNIT E, S 26, T 7S, R 26E
Chaves County

11-2-82



46 7400

KEUFFEL & ESSER CO. MADE IN U.S.A.

$\overline{\Delta P_1^2}$ $P_c^2 - P_w^2 = 800$

$\overline{\Delta P_2^2}$ $P_c^2 - P_w^2 = 80$

$Q_1 = 1954.3$ MCFD

$Q_2 = 417.0$ MCFD

$\text{Log } Q_1 = 3.291$

$\text{Log } Q_2 = 2.620$

$n = .671$