

MULTIPOINT AND ONE POINT BACK PRESSURE TEST

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FOR GAS WELL

FEB 02 1984

O. C. D.
ARTESIA, OFFICE

Type Test ☒ Initial ☐ Annual ☐ Special		Test Date 1-13-84	
Company McKay Oil Corporation ✓		Connection AIR - NEW WELL	
Pool Pecos Slope ABO		Formation ABO	
Completion Date 12-26-83		Total Depth 4,750'	
Plug Back TD 4,711'		Elevation 3720'	
Form or Lease Name McKay Pennzoil Fed		Well No. 1	
Csg. Size 4.50		Wt. 11.60	
d 4.000		Set At 4,745'	
Perforations: From 4219'		To 4429'	
Thq. Size 2,375		Wt. 4.70	
d 1,995		Set At 4,312'	
Perforations: From Open		To Ended	
Type Well - Single - Bradenhead - G.C. or G.O. Multiple Single		Packer Set At None	
Producing Thru 2 3/8" Tubing		Reservoir Temp. °F 99	
Mean Annual Temp. °F 60		Baro. Press. - P _a 13.2	
State N. M.		County Chaves	
L 4,319'		H 4,319'	
Cg 0.691		% CO ₂ 1.226	
% N ₂ 4.880		% H ₂ S Prover	
Meter Run 4.026		Taps Flange	
FLOW DATA			
NO.	Prover Line Size	X	Orifice Size
SI			
1.	4.026 x 1.875		500
2.	4.026 x 1.875		480
3.	4.026 x 1.875		430
4.	4.026 x 1.875		525
5.			
TUBING DATA			
NO.	Prover Line Size	X	Orifice Size
SI			
1.	4.026 x 1.875		500
2.	4.026 x 1.875		480
3.	4.026 x 1.875		430
4.	4.026 x 1.875		525
5.			
CASING DATA			
NO.	Prover Line Size	X	Orifice Size
SI			
1.	4.026 x 1.875		500
2.	4.026 x 1.875		480
3.	4.026 x 1.875		430
4.	4.026 x 1.875		525
5.			
RATE OF FLOW CALCULATIONS			
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m
1	17.26	45.31	513.2
2	17.26	75.31	493.2
3	17.26	143.56	443.2
4	17.26	226.12	538.2
5			
NO.	Flow Temp. °F	Grav. Factor F _g	Super. Factor F _{sp}
1	78	.9831	1.054
2	78	.9831	1.052
3	75	.9859	1.046
4	80	.9813	1.056
5			
NO.	R	Temp. °R	T _r
1	.77	538	1.39
2	.74	538	1.39
3	.66	535	1.38
4	.80	540	1.39
5			
Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.			
A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.			
Specific Gravity Separator Gas 0.691			
Specific Gravity Flowing Fluid _____			
Critical Pressure _____ P.S.I.A.			
Critical Temperature _____ R			
P _c 975.2 P _c ² 951.0			
NO.	P ₁ ²	P _w	P _w ²
1		948.2	899.1
2		930.2	865.3
3		882.2	778.3
4		822.2	676.0
5			
(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 3.458$			
(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 3.260$			
AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 15,860$			
Absolute Open Flow 15,860 Mcf @ 15.025			
Angle of Slope 43.6°			
Slope, n .95236			
Remarks:			
Approved By Division			
Conducted By: Gary Roberts			
Calculated By: Jim Johnson			
Checked By:			