STATE OF NEW MEXICO
ENERGY AND MINERALS DEPARTMENT

P. O. BOX 2088
SANTA FE, NEW MEXICO 87501

Form C-122
Revised 10-1-78

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

RECEIVED
MAY 04 '88
O. C. D.
ARTESIA, OFFICE

45 F. File

Type Test: [X] Initial [ ] Annual [ ] Special				Test Date: 4-4-88	
Company: MCKAY OIL CORPORATION			Connection: AIR		
Pool: WEST PECOS SLOPE ABO			Formation: ABO		Unit: J
Completion Date: 4-4-88	Total Depth: 4170'		Plug Back TD: 3167'	Elevation: 4195 KB	Farm or Lease Name: HOMESTEAD
Csg. Size: 4-1/2" / Wt.: 10.5# / d: 4.090 / Set At: 3251'			Perforations: From 2685' To 2697		Well No.: #1
Tbg. Size: 2-3/8" / Wt.: 4.7# / d: 1.995 / Set At: 2651'			Perforations: From -- To --		Unit J / Sec. 20 / Twp. 6S / Rge. 22E
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: Single			Packer Set At: 2654'		County: Chaves
Producing Thru: Tubing	Reservoir Temp. °F: 90 @ 2691	Mean Annual Temp. °F: 60	Baro. Press. – P_a: 13.2		State: NM

L	H	Gg	% CO_2	% N_2	% H_2S	Prover	Meter Run	Taps
2691	2691	0.636	0.00	6.698	0.00	2.00	--	--

	FLOW DATA					TUBING DATA		CASING DATA		
NO.	Prover Line Size	X Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration of Flow
SI						835		PKR.		72 HRS.
1.	2.000	0.125	160	--	60	818	60			
2.	2.000	0.250	187	--	60	736	60			
3.	2.000	0.375	144	--	60	580	60			
4.	2.000	0.375	156	--	60	438	60			
5.										

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	0.2648	--	173.2	1.000	1.254	1.014	58
2.	1.087	--	200.2	1.000	1.254	1.016	277
3.	2.378	--	157.2	1.000	1.254	1.026	481
4.	2.378	--	169.2	1.000	1.254	1.028	519
5.							

NO.	P_t	Temp. °R	T_r	Z
1.	0.26	520	1.49	.973
2.	0.30	520	1.49	.969
3.	0.24	520	1.49	.975
4.	0.26	520	1.49	.973
5.				

Gas Liquid Hydrocarbon Ratio -- Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons -- Deg.
Specific Gravity Separator Gas 0.636 XXXXXXXXX
Specific Gravity Flowing Fluid XXXXX
Critical Pressure 658 P.S.I.A. ____ P.S.I.A.
Critical Temperature 348 R ____ R

P_c 848.2 P_c^2 719.4

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1	690.9	831.0	690.9	28.5
2	559.8	749.7	560.6	158.8
3	350.5	594.8	352.7	366.7
4	203.4	453.9	206.0	513.4
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 25.242$

(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 13.881$

Post ID-2
5-13-88
comp 4 BK

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 805.1$

Absolute Open Flow 805 Mcfd @ 15.025 | Angle of Slope θ 50.82 | Slope, n 0.815

Remarks:

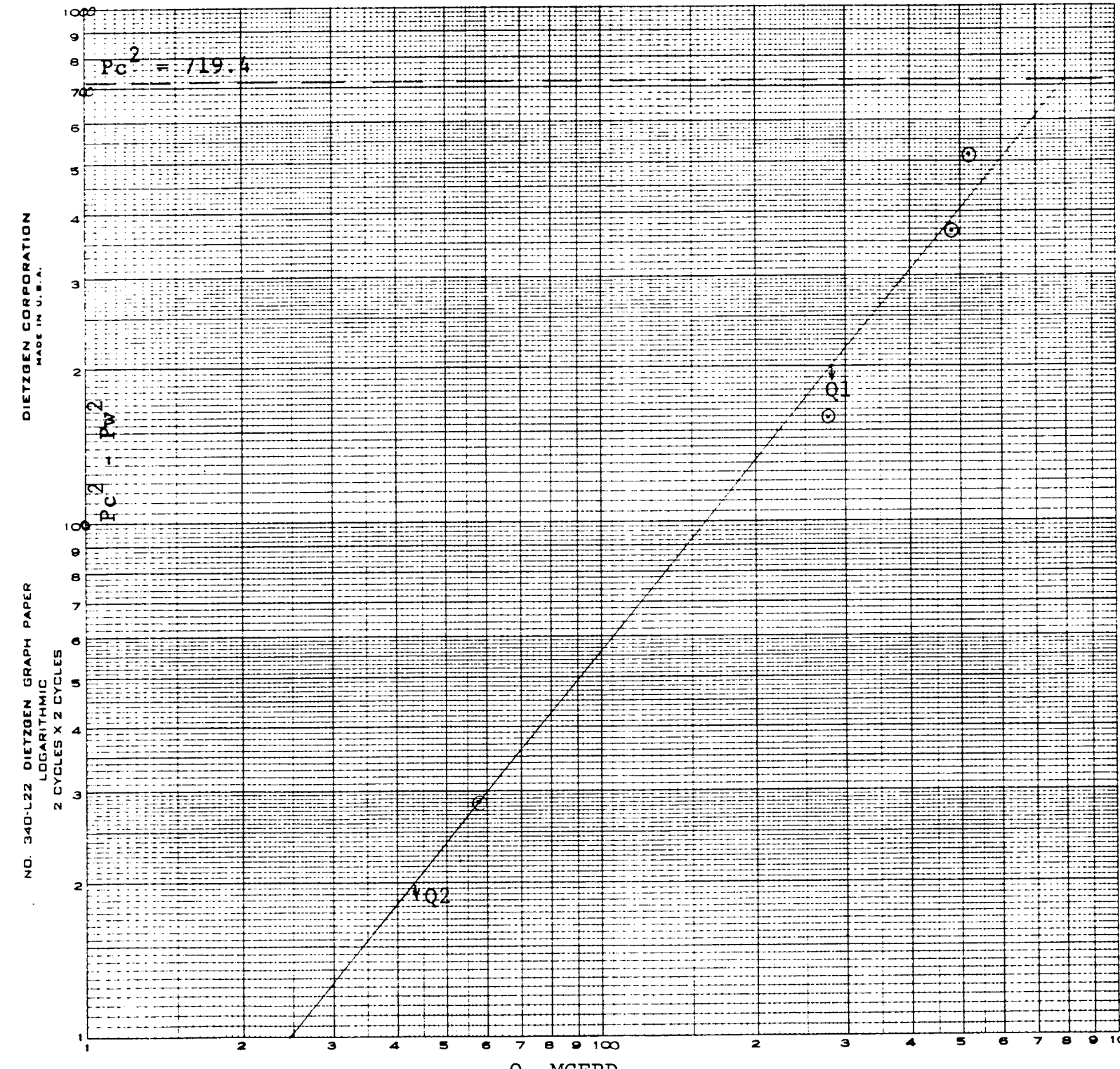
Approved By Division	Conducted By:	Calculated By:	Checked By:
	D. Kelton	C. Sanders	P. Stewart

MCKAY OIL CORPORATION

Homestead #1

Sec. 20, T6S, R22E

April 4, 1988



Q1 = 282 ; log = 2.45025

Q2 = 43.2; log = 1.63548

0.81477

n = 0.815

AOF = 805 MCFPD

θ = 50.82

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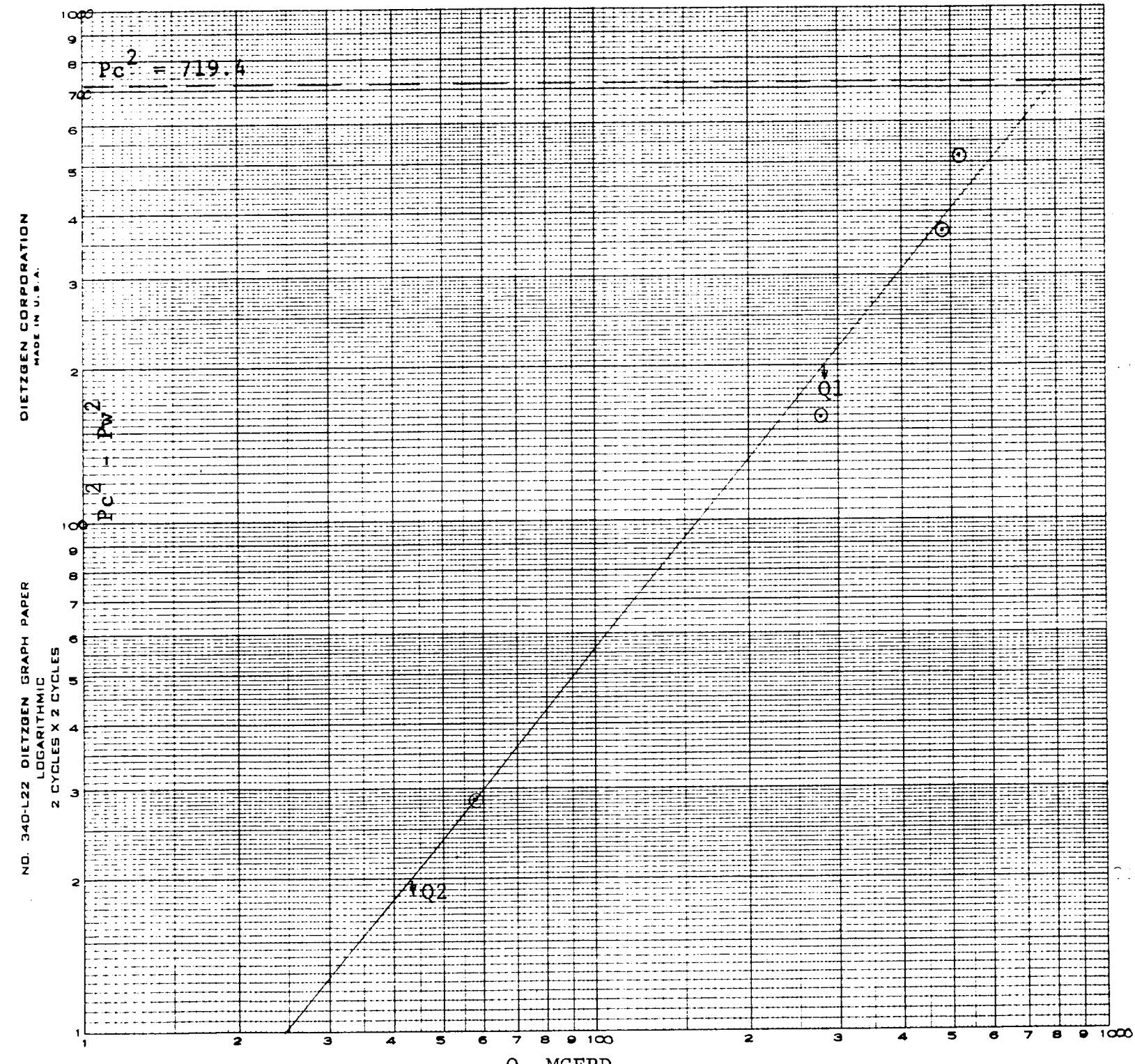

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