STATE OF NEW MEXICO
ENERGY AND MINERALS DEPARTMENT

OIL CONSERVATION DIVISION
P. O. BOX 2088
SANTA FE, NEW MEXICO 87501

Form C-122
Revised 10-1-78

C/SF
File

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

RECEIVED
DEC 17 '87
O. C. D.
ARTESIA, OFFICE

Type Test: [X] Initial [ ] Annual [ ] Special				Test Date: 12-03-87	
Company: ELK OIL CO.		Connection: AIR			
Pool: N. FOOR RANCH PENN		Formation: PENN		Unit:	
Completion Date: 12-8-87	Total Depth: 6530	Plug Back TD: 6460	Elevation: 3958 GR	Farm or Lease Name: J R STATE	
Csg. Size: 5½ (2-3/8)	Wt.: 15.5	d:	Set At: 6520	Perforations: From 6341 To 6394	Well No.: 1
Tbg. Size: 2-3/8	Wt.:	d:	Set At: 6274	Perforations: From OPEN To ENDED	Unit: N Sec.: 32 Twp.: 8S Rge.: 27E
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: SINGLE			Packer Set At: 6274		County: CHAVES
Producing Thru: TUBING	Reservoir Temp. °F:	Mean Annual Temp. °F: 60	Baro. Press. – P_a: 13.2		State: NEW MEXICO
L	H	Gg: .70	% CO_2	% N_2	% H_2S

Prover: 2 | Meter Run: | Taps:

NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	TUBING DATA Press. p.s.i.g.	TUBING DATA Temp. °F	CASING DATA Press. p.s.i.g.	CASING DATA Temp. °F	Duration of Flow
SI							1867		PACKER		
1.	2	x	3/32	1770		65	1772		"		1 hr.
2.	2	x	3/16	1437		65	1440		"		"
3.	2	x	1/4	980		65	985		"		"
4.	2	x	5/16	750		65	755		"		"
5.											

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	.1410		1783.2	.9952	1.1952	1.2143	363
2.	.6082		1450.2	.9952	1.1952	1.1862	1244
3.	1.0870		993.2	.9952	1.1952	1.1397	1452
4.	1.6720		763.2	.9952	1.1952	1.0929	1658
5.							

NO.	P_r	Temp. °R	T_r	Z
1				
2.				
3.				
4.				
5.				

Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
Specific Gravity Separator Gas _____ XXXXXXXXXX
Specific Gravity Flowing Fluid XXXXX _____
Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
Critical Temperature _____ R _____ R

P_c 2196.2 P_c^2 4823

NO	P_t^2	P_w	R_w^2	$P_c^2 - R_w^2$
1		2067.2	4273	550
2		1693.2	2867	1956
3		1281.2	1641	3182
4		944.2	891	3932
5				

(1) $\frac{P_c^2}{P_c^2 - R_w^2} = 1.2266$ (2) $\left[\frac{P_c^2}{P_c^2 - R_w^2}\right]^n = 1.1869$

Post FD-2
1-8-88
comp & BK

AOF = Q $\left[\frac{P_c^2}{P_c^2 - R_w^2}\right]^n = 2000$

Absolute Open Flow 2000 Mcfd @ 15.025 | Angle of Slope θ 51° | Slope, n 1.1869

Remarks:
ALL BOTTOM HOLE PRESSURES DONE WITH AMERADA TYPE GAUGE.

Approved By Division	Conducted By:	Calculated By:	Checked By:
	KELTIC SERVICE	MIKE KELLY	