

125 file
Form C-122
Revised 9-1-65
RECEIVED

Type Test ☒ Initial ☐ Annual ☐ Special		Test Date 10-29-75		APR 25 1977	
Company Dalport Oil Corporation			Connection To Air		
Pool <i>S/E Chaves Queen Gas</i> <i>Lucky Lake area associated</i>			Formation Queen		Unit ARTERIA, OFFICE
Completion Date 10-29-75		Total Depth 10,730'		Plug Back TD 1923'	
Elevation 3907 Gr.		Farm or Lease Name Shell Federal			
Csg. Size 8 5/8"	Wt. 36#	d 7.825"	Set At 4073'	Perforations: From 1844' To 1860'	
Tbg. Size 2 3/8"	Wt. 4.7#	d 1.995"	Set At 1820'	Perforations: From To	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single			Packer Set At None		County Chaves
Producing Thru Tubing		Reservoir Temp. °F @		Mean Annual Temp. °F 30	
Baro. Press. - P _g 13.2		State New Mexico			
L 1852	H 1852	G _g 0.9187	% CO ₂ 0.095	% N ₂ 64.963	% H ₂ S -0-
Prover		Meter Run		Taps	
Positive Chokes					

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI	Positive Chokes										72 Hrs.
1.	8/64			435.0		64	435.0	64			30 Min
2.	10/64			364.0		66	364.0	66			30 Min
3.	12/64			320.0		66	320.0	66			30 Min
4.	14/64			270.0		70	270.0	70			30 Min
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	0.2618		448.2	.9962	1.043	1.025	125.0
2	0.4173		377.2	.9943	1.043	1.021	166.7
3	0.6101		333.2	.9943	1.043	1.019	214.8
4	0.8419		283.2	.9905	1.043	1.015	250.0
5							

NO.	P _r	Temp. °R	T _r	Z	TSTM	
1.	0.47	524	1.49	.951	Gas Liquid Hydrocarbon Ratio	Mcf/bbl.
2.	0.40	526	1.50	.959	A.P.I. Gravity of Liquid Hydrocarbons	Deg.
3.	0.35	526	1.50	.964	Specific Gravity Separator Gas	0.9187
4.	0.30	530	1.51	.970	Specific Gravity Flowing Fluid	XXXXXX
5.					Critical Pressure	944 * P.S.I.A.
					Critical Temperature	351 * R

P_c 573.2 P_c² 328.6

NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²
1	200.9	#	200.9	127.7
2	142.3	#	142.3	186.3
3	111.0	#	111.0	217.6
4	80.20	#	80.2	248.4
5	see below			

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.3229$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.3229$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 331$

Absolute Open Flow		331	Mcf/d @ 15.025	Angle of Slope θ	45.0°	Slope, n	1.00 limit
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Remarks: *N₂ percentage exceeds tables, therefore critical pressure & Temperature are estimated
Good point alignment but slightly in excess of 1.000 limits
#Friction Negligible

Approved By Commission:	Conducted By: G. Parker	Calculated By: R. West	Checked By: J. West
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