

MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

RECEIVED

Type Test ☒ Initial ☐ Annual ☐ Special						Test Date May 17, 1969		JUN 3 1969 D. C. C. ANTENNA OFFICE	
Company Pan American Pet. Corp.				Connection Phillips Pet. Co.					
Pool Buffalo Valley				Formation Penn				Unit	
Completion Date Nov. 7, 1968		Total Depth 8413		Plug Back TD 8348		Elevation 3493 RDB		Farm or Lease Name Federal "C" Gas Com.	
Csg. Size 5 1/2	Wt. 14 - 17	d 8413	Set At 8413	Perforations: From 8232 To 8257		Well No. 1			
Tbg. Size 2 3/8	Wt. 4.7	d 1.995	Set At 7915	Perforations: From open To ended		Unit C	Sec. 11	Twp. 13S	Rge. 27E
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single						Packer Set At 7907		County Chaves	
Producing Thru Tbg		Reservoir Temp. °F 1350_a 8245		Mean Annual Temp. °F		Baro. Press. - P _a 13.2		State New Mexico	
L 7915	H 7915	Gg .670	% CO ₂ .32	% N ₂ .86	% H ₂ S 0	Prover -	Meter Run X	Taps Flange	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							2007		Packer		24
1.	4 X 2.50			659.2	2.76	76	1500	68			2
2.	4 X 2.50			692.4	5.12	75	1400	68			1
3.	4 X 2.50			692.4	6.48	73	1300	67			1
4.	4 X 2.50			709.3	8.62	72	1150	68			1
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	32.64	43.08	672.4	.9850	1.222	1.066	1804
2	32.64	60.01	705.6	.9859	1.222	1.071	2527
3	32.64	67.62	705.6	.9877	1.222	1.071	2853
4	32.64	79.83	722.5	.9887	1.222	1.075	3384
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1.	1.01	536	1.42	.880	44.03	64.7	.670	X X X X X X X X	669	668
2.	1.05	535	1.41	.872				X X X X X		398
3.	1.05	533	1.41	.872						
4.	1.08	532	1.40	.865						
5.										

P _c 2020.7 P _c ² 4083.2				(1) $\frac{P_c^2}{P_c^2 - R_w^2} = 1.658$		(2) $\left[\frac{P_c^2}{P_c^2 - R_w^2} \right]^n = 1.249$	
NO.	P _r ²	P _w	R _w ²	P _c ² - R _w ²			
1		1536.3	2360.2	1723.0			
2		1463.4	2141.5	1941.7			
3		1381.2	1907.7	2175.5			
4		1273.0	1620.5	2462.7			
5							

Absolute Open Flow 5610 Mcfd @ 15.025				Angle of Slope θ		Slope, n 1.000	
Remarks: Slope in excess of 1.000; used slope = 1.000 through high rate							

Approved By Commission:	Conducted By: D. C. Pennington	Calculated By: Wm. H. Hall	Checked By: H. L. Smith
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OIL REPORTS & GAS SERVICES
P. O. BOX 763 HOBBS, N. M.