

OCC

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test ☒ Initial / ☐ Annual ☐ Special				Test Date 4-7-71	
Company Read & Stevens, Inc				Connection Phillips (Pending)	
Pool Buffalo Valley				Formation Penn.	
Completion Date 3-14-71		Total Depth 8792		Elevation 3570 GL	
Csq. Size 4 1/2		Set At 8709		Perforations: From 8516 To 8645	
Thg. Size 2.375		Set At 8482		Perforations: From OPEN To	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single				Packer Set At 8482	
Producing Thru Tubing		Reservoir Temp. °F 150 @ 8700		Mean Annual Temp. °F 60	
Baro. Press. - P _a 13.2		State N. MEXICO		County Chaves	
L 8516		H 8516		G _g 0673	
% CO ₂		% N ₂		% H ₂ S	
Prover		Meter Run 3.067		Taps FLSE	

FLOW DATA							TUBING DATA		CASING DATA		Duration
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	of Flow
SI	—	—	—	—	—	—	2009	—	—	—	18 hr
1.	3.068		1.25	720	8	75	1702	60	PKR	—	75 M
2.	"		"	720	10	74	1557	60	"	—	130 M
3.	"		"	720	15	74	1411	60	"	—	60 M
4.	"		"	720	23	74	1255	60	"	—	60 M
5.	"		"	720	22	74	1105	60	"	—	60 M

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{spv}	Rate of Flow Q, Mcfd
1	7.577	76.85	723.2	.9852	1.219	1.077	753.7
2	7.577	85.60	723.2	.9850	1.219	1.077	825.7
3	7.577	109.89	723.2	.9848	1.219	1.077	1024.1
4	7.577	129.83	723.2	.9848	1.219	1.077	1274.4
5	7.577	143.25	723.2	.9848	1.219	1.077	1405.2

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1	110	535	140	0.862	97.0	63	XXXXXXX	XXXXXX	669	382
2	110	536	140	0.862						
3	110	534	140	0.862						
4	110	534	140	0.862						
5	110	534	140	0.862						

NO.	P _r ²	P _w ²	R _w ²	P _r ² - R _w ²	(1) $\frac{P_r^2}{P_r^2 - R_w^2} =$	(2) $\left[\frac{P_r^2}{P_r^2 - R_w^2} \right]^n =$
1	2337.2	5442.5	1947.9		1.721	1.609
2	2152.2	4642.2	2261.2			
3	1945.2	3862.0	3548.4			
4	1742.2	3105.2	4305.1			
5	1548.2	2396.9	5013.5			

AOF = Q $\left[\frac{P_r^2}{P_r^2 - R_w^2} \right]^n = 2051$

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Absolute Open Flow 2030 Mcfd @ 15.025		Angle of Slope θ		Slope, n	
Remarks: From BHP Bomb set @ 2525' used for flow rate to check calculations					
Approved By Commission:		Conducted By: G.A. Snow		Checked By:	