N. M. . C. COM.

NEW MEXICO OIL CONSERVATION COMMSSION

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test: ☒ Initial ☐ Annual ☐ Special				Test Date: 4-13-73	
Company: Read & Stevens, Inc		Connection: (Pending)			
Pool: Buffalo Valley Penn		Formation: Atoka - Penn.		Unit	
Completion Date: 3-31-73	Total Depth: 8815	Plug Back TD: 8769	Elevation: 3601 Gl.	Farm or Lease Name: Langley "Comm"	
Csg. Size: 5 1/2 / Wt.: 15-17 / d: 5. / Set At: 8815		Perforations: From 8626 To 8646		Well No.: 1	
Tbg. Size: 2 3/8 / Wt.: 4.7 / d: 1.995 / Set At: 8393		Perforations: From NONE To		Unit: C / Sec.: 13 / Twp.: 15S / Rge.: 27E	
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: Single		Packer Set At: 8393		County: Chaves	
Producing Thru: Tubing	Reservoir Temp. °F: 128 @ 8500	Mean Annual Temp. °F: 60	Baro. Press. – P_a: 13.2	State: New Mexico	
L: 8626 / H: 8626	Gg: 0.625	% CO_2: —	% N_2: —	% H_2S: —	Prover: — / Meter Run: 4.026 / Taps: Flange

FLOW DATA						TUBING DATA		CASING DATA		
NO.	Prover Line Size	X Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration of Flow
SI	—	—	—	—	—	1675	—	—	—	72 hrs SI
1.	4.026	1.5	440	8	99	1540	74	PKR	—	60"
2.	4.026	1.5	420	24	82	1410	74	"	—	60"
3.	4.026	1.5	460	36	84	1315	74	"	—	30"
4.	4.026	1.5	460	52	84	1200	74	"	—	30"
5.										

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	10.84	60.21	453.2	0.9645	1.265	1.033	822.6
2.	10.84	101.96	433.2	0.9795	1.265	1.037	1420.1
3.	10.84	130.52	473.2	0.9777	1.265	1.038	1816.4
4.	10.84	156.86	473.2	0.9777	1.265	1.038	2182.9
5.							

NO.	P_t	Temp. °R	T_r	Z
1.	0.675	559	1.532	0.937
2.	0.646	542	1.485	0.930
3.	0.705	544	1.490	0.928
4.	0.705	544	1.490	0.928
5.				

Gas Liquid Hydrocarbon Ratio: 133.33 Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons: 63 Deg.
Specific Gravity Separator Gas: 0.625 XXXXXXXXX
Specific Gravity Flowing Fluid: XXXXX
Critical Pressure: 671 P.S.I.A. ____ P.S.I.A.
Critical Temperature: 365 R ____ R

P_c 2186.2 * P_c^2 4779.5

NO	P_t^2	P_w *	P_w^2	$P_c^2 - P_w^2$
1	—	2012.2	4,048.9	730.6
2	—	1866.2	3,482.7	1296.8
3	—	1760.2	3,098.3	1681.2
4	—	1634.2	2,670.6	2108.9
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} =$ ____ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n =$ ____

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n =$ 4800 Mcfd @ 15.025

RECEIVED
APR 27 1973
U. S. GEOLOGICAL SURVEY

Angle of Slope θ: ____ Slope, n: .949

Remarks: * From BHP Bomb set @ 8650'

Approved By Commission:	Conducted By:	Calculated By:	Checked By:
	R. A. Snow	R. A. Snow	