Copy
C-122

NEW MEXICO OIL CONSERVATION COMMISSION

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

RECEIVED
APR 13 1973
O. C. C.
ARTESIA, OFFICE

Type Test: [X] Initial [ ] Annual [ ] Special				Test Date: 4-6-73	
Company: DALPORT OIL CORP.		Connection: TO AIR			
Pool: DOUBLE L Queen Assoc.		Formation: QUEEN		Unit: O	
Completion Date: 4-2-73	Total Depth: 1881	Plug Back TD: 1874	Elevation: 3822 GR.	Farm or Lease Name: FALGOUT FEDERAL	
Csg. Size: 4½ / Wt.: 9.5# / d: 4.082 / Set At: 1881		Perforations: From 1838 To 1851		Well No.: 2	
Tbg. Size: 2 3/8 / Wt.: 4.5# / d: 1.995 / Set At: 1796		Perforations: From OPEN To ENDED		Unit: G / Sec.: 26 / Twp.: 14S / Rge.: 29E	
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: SINGLE		Packer Set At: NONE		County: CHAVES	
Producing Thru: TUBING	Reservoir Temp. °F:	Mean Annual Temp. °F: 60	Baro. Press. – P_a: 13.2	State: NEW MEXICO	

L	H	Gg	% CO_2	% N_2	% H_2S	Prover	Meter Run	Taps
1796	1796	0.897	0.17	60.63	------	O.W.T.		

	FLOW DATA				TUBING DATA		CASING DATA		
NO.	Prover Line Size X Orifice Size	Press. IN ~~MCF~~ HG	Diff. ~~MCF~~	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration of Flow
SI					460.0		461.0		48 HRS
1.	4" OWT X 1.00"		4.5	75	359.0	75	360.0		0.50
2.	4" OWT X 1.00"		11.0	75	283.0	75	283.0		0.75
3.	4" OWT X 1.00"		16.5	74	206.0	74	206.0		0.75
4.	4" OWT X 1.00"		21.5	73	99.0	73	103.0		1.00
5.									

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	~~MCF~~ VOLUMES ~~MCF~~ BEFORE CORR.	Pressure P_m	Flow Temp. Factor Ft,	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	VOLUMES	180.1		.9859	.8179	1.000	145.2
2.	FROM	291.1		.9859	.8179	1.000	234.7
3.	GOR TEST	366.1		.9868	.8179	1.000	295.5
4.	MANUAL	427.7		.9877	.8179	1.000	345.5
5.							

NO.	P_r	Temp. °R	T_r	Z
1	NOT APPLICABLE			
2.				
3.				
4.				
5.				

Gas Liquid Hydrocarbon Ratio: DRY Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons: ____ Deg.
Specific Gravity Separator Gas: 0.897 XXXXXXXXX
Specific Gravity Flowing Fluid: XXXXX
Critical Pressure: ____ P.S.I.A. ____ P.S.I.A.
Critical Temperature: ____ R ____ R

P_c 474.2 P_c^2 224.9

NO	P_t^2	P_w	R_w^2	$P_c^2 - R_w^2$
1	138.50	373.2	139.30	85.60
2	87.73	296.2	87.73	137.17
3	48.05	219.2	48.05	176.85
4	12.59	116.2	13.50	211.40
5				

(1) $\frac{P_c^2}{P_c^2 - R_w^2} = 1.0639$ (2) $\left[\frac{P_c^2}{P_c^2 - R_w^2}\right]^n = 1.0561$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - R_w^2}\right]^n = 364.9$

Absolute Open Flow: 364.9 Mcfd @ 15.025 Angle of Slope θ: 48.6° Slope, n: 0.881

Remarks: ____

Approved By Commission:	Conducted By:	Calculated By:	Checked By:
	M.C.T.	R.L.W.	J.W.W.

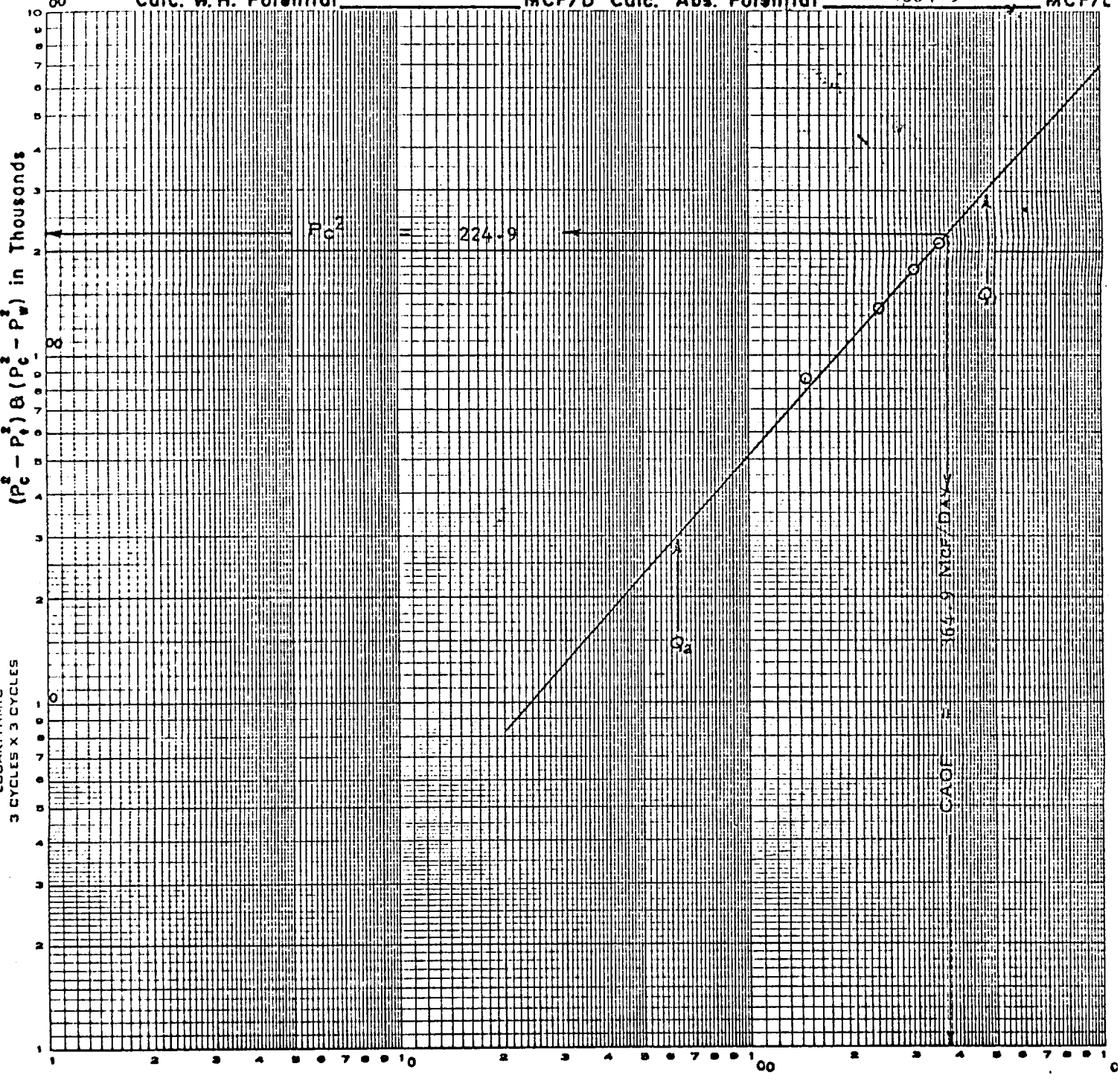
BACK PRESSURE CURVE

Operator DALPORT OIL CORP. Lease FALGOUT FEDERAL Well No. 2

County CHAVES Field DOUBLE L Location G-SEC. 26, T14S, R29E

Date of Test 4-6-73 Slope "n" 0.881 W.H. _____ Abs.

Calc. W.H. Potential _____ MCF/D Calc. Abs. Potential 364.9 MCF/D



Q in MCF/Day

SLOPE (N) = Q_1 = 475 = 6.6766936

Q_2 = 62.5 = 5.7958800

N = 0.8808136

$$AOF = 345.5\left(\frac{224.9}{211.4}\right)^{.881} = 364.9 \text{ MCFD}$$