

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 1-18-1975	
Company READ & Stevens, Inc						Connection Pending	
Pool Buffalo Valley						Formation Atoka - Penn.	
Completion Date 8-28-74		Total Depth 8891'		Plug Back TD 8730'		Elevation 3630 RKB	
Csg. Size 5 1/2"		Set At 8891'		Perforations: From To		Well No. 1	
Tubg. Size 2 3/8"		Set At 8617		Perforations: From 8626 To 8702		Unit Sec. Twp. Rge. J 13 15S 27E	
Type Well - Single - Brdhead - G.G. or G.O. Multiple Casing Set Through and Perforated						Packer Set At 8617	
Producing Thru Tubing		Reservoir Temp. °F 128°		Mean Annual Temp. °F 60		Baro. Press. - P _a 13.2	
L 8626		Gg 8626		% CO ₂ 0.625		Prover 3.068	
				% N ₂ —		Meter Run 3.068	
				% H ₂ S —		Taps Flgs	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. hw	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							2225				20 hrs S.L.
1.	3.068	1.0	400	5	83	1960	50	PKR	—	60	
2.	3.068	1.0	400	10	83	1685	55	PKR	—	60	
3.	3.068	1.0	400	14	84	1400	55	PKR	—	75	
4.	3.068	1.0	400	19	85	1139	45	PKR	—	75	
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	4.789	45.45	413.2	0.9786	1.265	1.033	278.3
2	4.789	64.28	413.2	0.9786	1.265	1.033	393.7
3	4.789	76.06	413.2	0.9777	1.265	1.033	465.5
4	4.789	88.60	413.2	0.9768	1.265	1.033	541.6
5							

NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
					96.944	63	0.625	X X X X X X X X	671	365
1.	.0616	543	1.49	0.938						
2.	.0616	543	1.49	0.938						
3.	.0616	544	1.49	0.938						
4.	.0616	545	1.49	0.938						
5.										

NO.	P _i ²	P _w *	R _w ²	P _i ² - R _w ²
1		2613.2	6828.8	2142.4
2		2265.2	5131.1	3840.1
3		1914.2	3664.2	5307.0
4		1612.2	2599.2	6372.0
5				

(1) $\frac{P_c^2}{P_c^2 - R_w^2} =$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - R_w^2} \right]^n =$

(2) $\left[\frac{P_c^2}{P_c^2 - R_w^2} \right]^n =$

RECEIVED

FEB 11 1975

Absolute Open Flow 680	Mcf @ 15.025	Angle of Slope @	G.B.C. ARTESIA OFFICE 633
Remarks: * From BHP Bomb set @ 8681'			

Approved By Commission:	Conducted By: G.A. SNOW	Calculated By: G.A. SNOW	Checked By:
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