

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

RECEIVED
Form O.C.C.-D
Revised 9-1-65

NOV 17 1978

Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 10-27-78		O. C. C. ARTESIA, OFFICE	
Company Depco, Inc. ✓				Connection					
Pool Buffalo Valley Penn				Formation Morrow				Unit	
Completion Date 10-12-78		Total Depth 9185		Plug Back TD 9185		Elevation 3551 Gr.		Farm or Lease Name R & S Federal Com	
Csg. Size 4 1/2	Wt. 11.6	d	Set At 9184	Perforations: From 8936 To 8966		Well No. 1			
Thg. Size 2 3/8"	Wt. 4.7	d	Set At 8847	Perforations: From Open Ended To		Unit Sec. Twp. Rye. L 17 15 28			
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single						Packer Set At 8859		County Chaves	
Producing Thru Tubing		Reservoir Temp. °F #		Mean Annual Temp. °F		Baro. Press. - P _a		State New Mexico	
L 8951	H 8951	G _g .685	% CO ₂	% N ₂	% H ₂ S	Prover	Meter Run X	Taps	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI							2261	56			
1.	2	x	1.250	526.8	13.0	66	2196	61			60 Min.
2.	2	x	1.250	640.2	88.4	70	2090	66			60 Min.
3.	2	x	1.500	743.0	65.6	72	2022	66			60 Min.
4.	2	x	1.500	753.6	108.2	72	1913	68			60 Min.
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	8.120	83.785	540.0	.9943	1.208	1.063	869
2	8.120	240.334	653.4	.9905	1.208	1.075	2,510
3	12.76	222.726	756.2	.9887	1.208	1.085	3,683
4	12.76	288.041	766.8	.9987	1.208	1.085	4,811
5							

NO.	P _f	Temp. °R	T _f	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1.	.81	526	1.36	.885	A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.	.98	530	1.37	.866	Specific Gravity Separator Gas .685 X X X X X X X X
3.	1.13	532	1.38	.850	Specific Gravity Flowing Fluid X X X X X
4.	1.15	532	1.38	.850	Critical Pressure 699 P.S.I.A. P.S.I.A.
5.					Critical Temperature 386.5 R R

NO.	P _f	P _s	P _s ²	P _f ² - P _s ²	(1) $\frac{P_f^2}{P_f^2 - P_s^2} = 7.961$	(2) $\left[\frac{P_f^2}{P_f^2 - P_s^2} \right]^n = 7.961$
1		3093.2	9568	312	$AOF = Q \left[\frac{P_f^2}{P_f^2 - P_s^2} \right]^n = 38,302$	<i>Posted 11-22-78</i>
2		3009.2	9055	725		
3		2987.2	8923	957		
4		2939.2	8639	1241		
5						

Absolute Open Flow <u>38,300</u> Mcfd @ 15.025		Angle of Slope @ <u>45°</u>	Slope, n <u>1.00</u>
Remarks: _____			
Approved By Commission:		Conducted By: <u>Jones</u>	Calculated By: <u>Turner</u>
		Checked By:	