C/SF
C-122

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

RECEIVED
MAR 22 1982
O. C. D.
ARTESIA, OFFICE

Type Test: ☐ Initial ☐ Annual ☒ Special				Test Date: 3/15/82	
Company: Read & Stevens /		Connection: El Paso			Unit: -
Pool: Buffalo Valley Penn.		Formation: Atoka			
Completion Date: 10/21/81	Total Depth: 9040'		Plug Back TD: 8983'	Elevation: 3637 KB	Farm or Lease Name: Harris Fed.
Csg. Size: 4 1/2" / Wt.: 11.6 / d: 4.00 / Set At: 9040			Perforations: From 8742 To 8785		Well No.: 6
Tbg. Size: 2 3/8 / Wt.: 4.7 / d: 1.99 / Set At: 8624			Perforations: From To		Unit: I / Sec.: 23 / Twp.: 15S / Rge.: 27E
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: Single			Packer Set At: 8624		County: Chaves
Producing Thru: Tubing	Reservoir Temp. °F: 135 @ 8760	Mean Annual Temp. °F: 60	Baro. Press. – P_a: 13.2		State: New Mexico
L: 8760	H:	Gg: .649	% CO_2: .78	% N_2: 2.39	% H_2S: Prover: Meter Run: 4.025 Taps: Flange

FLOW DATA / TUBING DATA / CASING DATA

NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	Tubing Press. p.s.i.g.	Tubing Temp. °F	Casing Press. p.s.i.g.	Casing Temp. °F	Duration of Flow
SI							2390		Packer		
1.	4.025	X	.875	755	50	77	2100	70	"		1 Hr
2.	4.025	X	.875	760	65	74	1950	71	"		"
3.	4.025	X	.875	760	76	74	1825	70	"		"
4.	4.025	X	.875	760	81	74	1700	72	"		"
5.											

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	3.702	195.98	768	.984	1.266	1.064	961
2	3.702	224.18	773	.987	1.266	1.066	1120
3	3.702	241.59	773	.987	1.266	1.066	1191
4	3.702	250.26	773	.987	1.266	1.066	1234
5							

NO.	P_t	Temp. °R	T_r	Z
1	3.13	560	1.53	.794
2	2.90	560	1.53	.798
3	2.72	560	1.53	.803
4	2.53	560	1.53	.810
5				

Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
Specific Gravity Separator Gas _____ XXXXXXXXXX
Specific Gravity Flowing Fluid XXXXX _____
Critical Pressure 670 P.S.I.A. _____ P.S.I.A.
Critical Temperature 374 R _____ R

P_c 3313 P_c^2 10982

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1		2668	8988	1994
2		2480	6150	4832
3		2322	5392	5590
4		2164	4683	6299
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.743$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1.280$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1580$

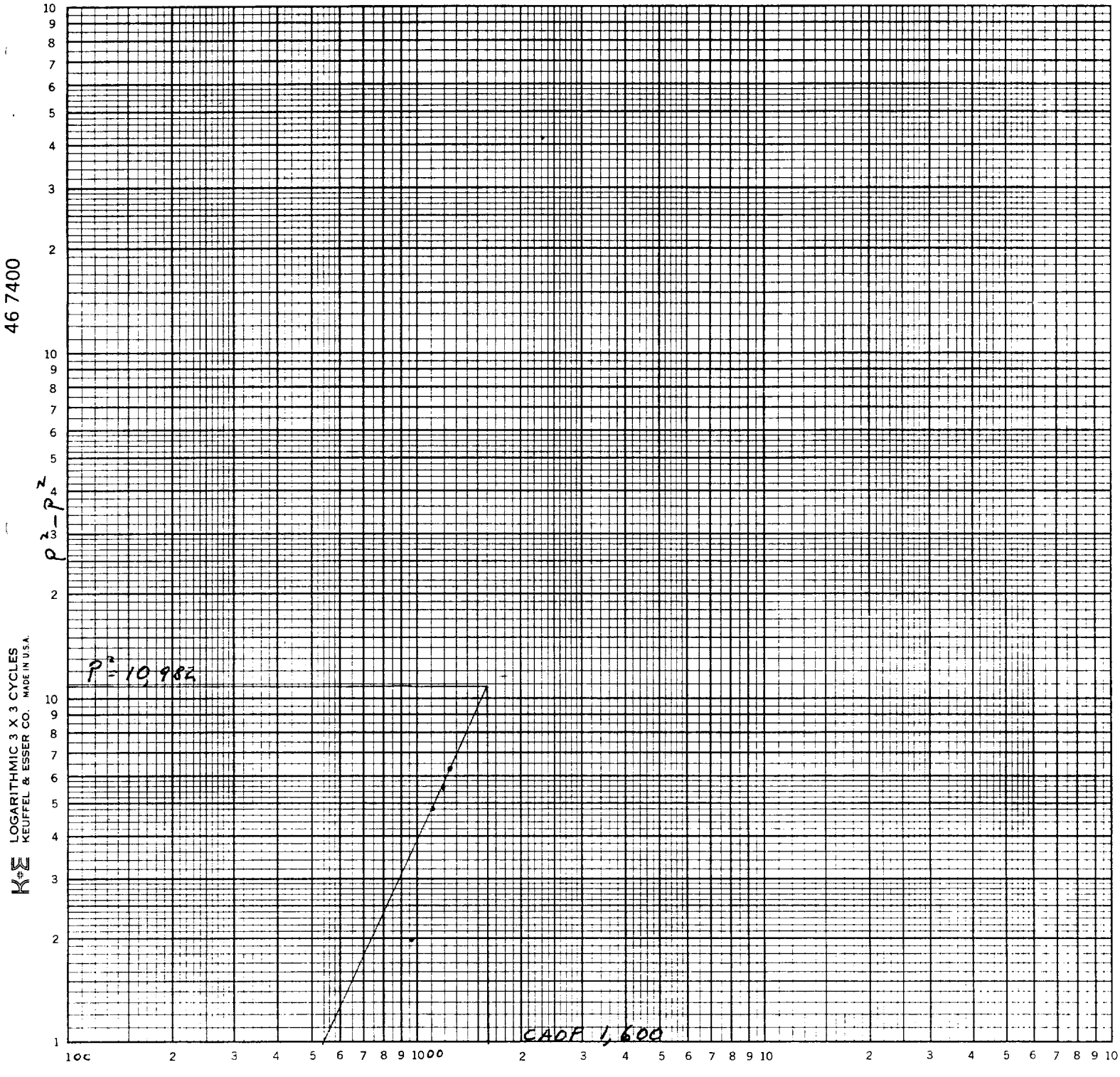
Absolute Open Flow 1580 Mcfd @ 15.025 Angle of Slope θ 33 Slope, n .445

Remarks: Calculated with know bottom hole pressures taken with an Amerada type gauge

Approved By Commission:	Conducted By:	Calculated By:	Checked By:
		M. Kelly	

READ & STEVENS

Harris Fed #6



Q
MSCFPD