

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form O-124
Revised 9-1-65

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Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 2-14-83		FEB 21 1983	
Company Dalport Oil Corp. ✓				Connection To Atmosphere		O. C. D.	
Pool Wildcat <i>Double Queen</i>				Formation Queen		WARTESIA, OFFICE	
Completion Date 2-4-83		Total Depth 1950'		Plug Back TD 1920'		Elevation 3863' @KB	
Casing Size 4 1/2"		Wt. 10.5#		Set At 1950'		Perforations: From 1811' To 1819'	
Tubing Size 2 3/8"		Wt. 4.6#		Set At 1803'		Perforations: From _____ To _____	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single				Packer Set At OPENENDED		County Chaves	
Producing Thru Tubing		Reservoir Temp. °F 78° @ 1815'		Mean Annual Temp. °F 60°		Baro. Press. - P _a 13.2	
L 1815'		H 1815'		C _g 9089		% CO ₂ .044	
				% N ₂ 65.429		% H ₂ S -0-	
				Prover 2.00"		Meter Run Taps	

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI									670#		48 Hours
1.	2.00"	x	.1250"	635#		54°	635#	60°	665		1 Hr.
2.	2.00	x	.2500	561		60	561	60	655		1 Hr.
3.	2.00	x	.3750	500		58	500	60	635		1 Hr.
4.	2.00	x	.5000	417		57	417	60	615		45 Min.
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor F _{pv}	Rate of Flow Q, Mcfd
1	.26480		648.2	1.006	1.049	1.028	186
2	1.087		574.2	1.000	1.049	1.025	671
3	2.378		513.2	1.002	1.049	1.022	1311
4	4.279		430.2	1.003	1.049	1.019	1974
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio TSTM	Mcf/bbl.
1	1.174	514	1.810	.946	A.P.I. Gravity of Liquid Hydrocarbons	Deq.
2	1.040	520	1.831	.951	Specific Gravity Separator Gas .9089	XXXXXXXXXX
3	.930	518	1.824	.957	Specific Gravity Flowing Fluid XXXXX	
4	.779	517	1.820	.963	Critical Pressure 552	P.S.I.A.
5					Critical Temperature 284	R

NO.	P _i ²	P _w ²	P _r ²	P _c ² - P _w ²
1	648.2	760.73	578.71	54.48
2	574.2	686.73	471.60	161.59
3	513.2	625.73	391.54	241.65
4	430.2	542.73	294.55	338.64
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = \frac{633.19}{633.19 - 578.71}$

(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \left[\frac{633.19}{54.48} \right]^{1.000}$

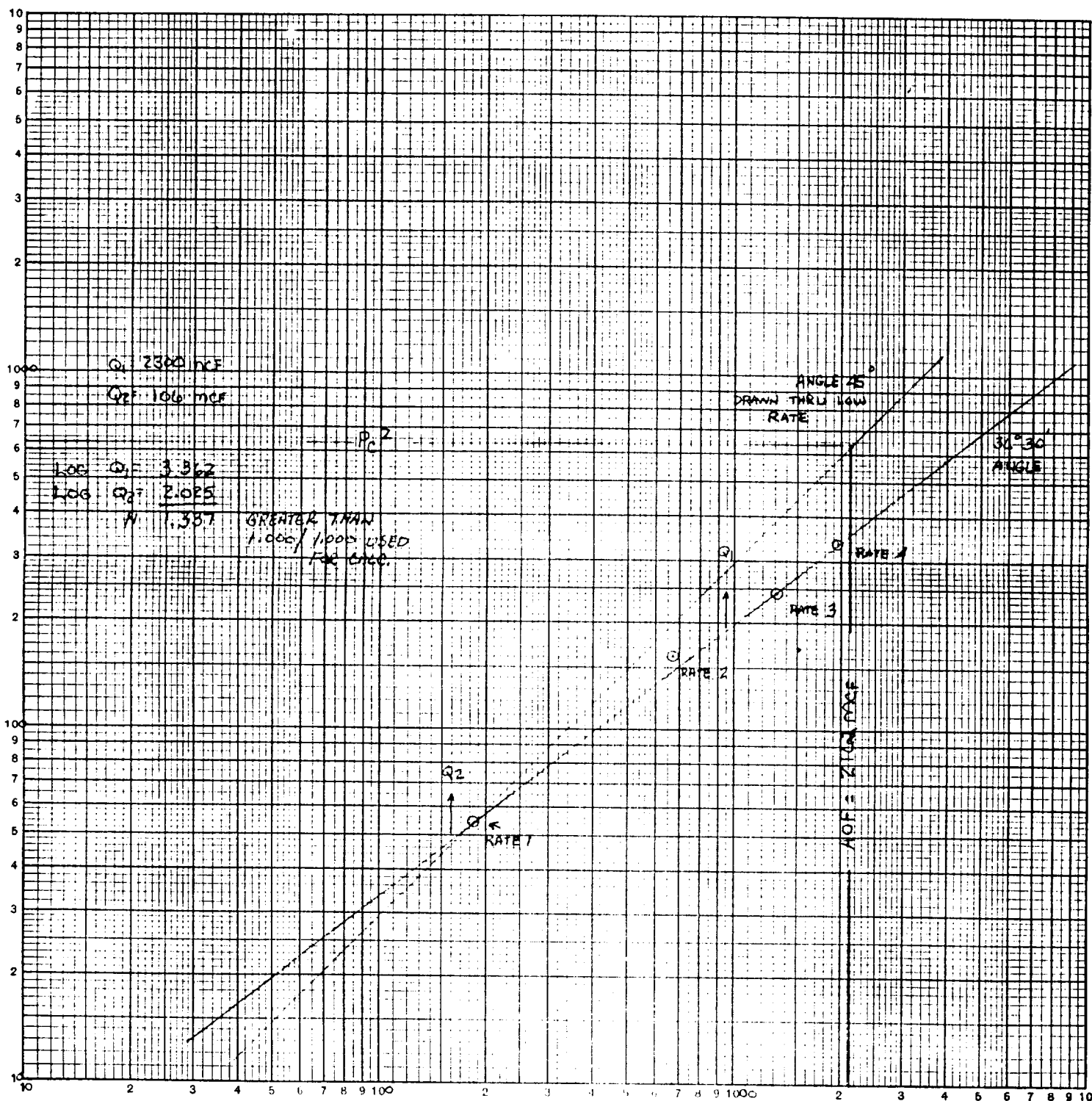
AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \frac{186 \times 2162}{633.19 - 578.71}$

186 = 2162 ID-2
Comp + BK
2-25-83

Absolute Open Flow	2162	Mcf/d @ 15.025	Angle of Slope	45°	Slope, n	1.000
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Remarks: Angle to flat to exponent greater than 1.00/a 45° angle was drawn thru low rate to exponent of 1.000 was used for all calculations

Approved By Commission:	Conducted By: W.S.	Calculated By: J.W.	Checked By: M.K.
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$$Q = \text{mcf}/D$$