UNITED BANK PLAZA 400 N. PENN, SUITE 1000

PRESIDENT

Read & Stevens, Inc. Oil Producers

Du Groducers P. O. Box 1518 Rosmell, New Mexico 88202

November 29, 1999

New Mexico Oil Conservation Division 811 South First Street Artesia, New Mexico 88210-2834

RE: Harris Federal #11 Section 26 T15S-R27E Chaves County, New Mexico De Novo Case #11514 Order #R10622

Ladies & Gentlemen:

Enclosed please find Form C-122-C for the subject well. Per the subject order number, Read & Stevens, Inc. is required to conduct a deliverability test into the pipeline on the subject well. The deliverability test was performed November 14, 1999 and the Artesia OCD office was advised of the date and time of the test.

Please note on the Form C-122-C that the stabilized test rate into the pipeline was 1,050 MCF, and the calculated deliverability at pipeline pressure using the "n" from the Multipoint Back Pressure Test was 1,646 MCFD. Taking the deliverability of 1,646 MCFD times fifty percent (50%) would yield an allowable of 823 MCFD for the subject well.

If you have any questions, please advise.

Sincerely,

**READ & STEVENS, INC.** 

John C Maxev/, Jr.

Operations Manager

JCM/sr/jcmltrs/ocdha11L4.wpd

Enclosure xc: File, Partners



STATE OF NEW MEXICO

ENERGY AND MINERALS DEPARTMENT

.

## - OIL CONSERVATION DIVISI ~ N P. O. BOX 2088 SANTA FE, NEW MEXICO 87501

Form C-122-C Revised 10-1-78

## DELIVERABILITY TEST REPORT

Type Test Test Date										<u> </u>						
			Initio	1 [	] A	Annual		Speci	al	11-14	4-99	.				
Company Connection CPM Cas Corporation																
Read & Stevens, Inc. GPM Gas Corporation Formation												Ún	iii iii			
Buffalo Valley Morrow												_				
Completion Total Depth						Plug Back TD Elevation						1	Farm or Lease Name			
	4-19-97			9050		<u> </u>	8998'			3492'GR			Harris Federal			
1	. Size	WI.				A1	Perforations: From 965/1 T						Well No. 11			
5 1/2" Tbg. Size		17# W1.		4.892 d Se		<u>9040'</u>	01	From 8654 T			• 8678 <b>'</b>			Sec.	Twp. Age.	
1		4.6#		1.995		8546'	From	From To			ò			26	55 2 <u>7E</u>	
TYP	c Well-Sing	ila – Bro	denhead	-G.G. or G.O			Packer Set At					60	County			
Single						854							Chaves			
Pro	ducing Thru			volt Temp. °F			d Tomp. °F	i		P <sub>a</sub>			Store			
	Tubing	157				60				3.2 %H <sub>2</sub> S Pro				Mexico r Run (Topa		
1	L 8666	н Q	666	Cq.		• co <sub>2</sub> 0.3	*N2 1.20	ו	7 123		PIOVE		Meter			
	8000	0		LOW DATA	<u> </u>	0.5			L UBING	DATA	1	CASI	ING D	ATA	Duration	
	Prover	Choke		Press.		Diff.	Temp.	Pre	65.	Temp.		Press.		Temp.	01	
ΝО.	Line Stze	X Orifice Size		p.s.i.g.		hw	•F	p.s.i.q.		°F		p. s. i.q.		•F	Flow	
SI	Total	Flow Mete		r			50	350						48 hrs		
1.			- <u>-</u>	<u> </u>	┸┯╾		64	20	0		<u> </u>			1	<u>  1 hr</u>	
	Coelli	cient				Pressure		Temp.		Gravity Factor		Super Compress.		Rate of Flow		
NO.	(2 <b>4-</b> H	our) —		√ <sup>h</sup> w <sup>p</sup> m		Pm		Ft		Fg		Factor Fpv		Q, Mcid		
1.							0.9	0.9962		1.256		1.0	1.020		1050	
	Pr Temp. R. Tr Z					Gau	Liquid Hydrocarbon Ratio Dry							Mcf/bbl.		
NO.	A.P.I. Gravity of Liquid Hydrocarbons Dry									Deg.						
l	0.413	•	cific Gravity Separator Gas0.63					• 6 3 4	4 xxxxxxxxx							
Pd 59.2 Specific Gravity Flowing Fluid XXXXX 670																
Pd <sup>2</sup> 3.50     Critical Pressure     670     p.e.i.a.       Pc     350.0     Pc <sup>2</sup> 131.9     Critical Temperature     370												p.s.i.d.				
Pc-		<sup>P</sup> c					Pf									
											1		1	2		
NQ	Pt	Pt <sup>2</sup>		$P_c - P_l^2$		Pw		°₩ <sup>2</sup>	Pc	$^2 - P_w^2$		P.		P. <sup>2</sup>	$P_1^2 - P_a^2$	
	213		45.	5 167.	5	282.	3	79.7	5	2.2	3	39.8	1_1	15.4		
$\left[P_{e^{2}}-P_{d^{2}}\right]$ $\left[1_{21}, q_{-3}\right]$ 50 0 (50 $\left[P_{e^{2}}-P_{d^{2}}\right]$ 0 0000																
-	$\begin{bmatrix} \frac{P_{c}^{2} - P_{d}^{2}}{P_{c}^{2} - P_{w}^{2}} \end{bmatrix} = \begin{bmatrix} 131.9 - 3.50 \\ 131.9 - 79 \end{bmatrix} = \underbrace{2.458}_{7} \qquad \text{Log} \begin{bmatrix} \frac{P_{c}^{2} - P_{d}^{2}}{P_{c}^{2} - P_{w}^{2}} \end{bmatrix} = \underbrace{0.3906}_{7}$															
$\left[P_{c}^{2}-P_{w}^{2}\right]$ $\left[131.9-79\right].7$																
~	-	1 n						~		-						
$\left[\frac{P_c^2 - P_d^2}{P_c^2 - P_w^2}\right]^n = \frac{1.568}{1.568} \qquad n \log \left[\frac{P_c^2 - P_d^2}{P_c^2 - P_w^2}\right] = \frac{0.195}{1.568}$																
	$P_c^2 - P_w^2$		<u> </u>	500			•	P	c <sup>2</sup> - P,	,2						
L	-	8						<b>6</b> .		<b>.</b>						
	[	Γ.,	 '	n												
D	eliv. = Q	Pe* - 1	24°													
$D_{\text{eliv.}} = Q \begin{bmatrix} \frac{P_c^2 - P_d^2}{P_c^2 - P_w^2} \end{bmatrix}^n$ Division																
	1	646		•			1	Compa	nv	Rea	ad &	Steve	ns, ]	[nc.		
<b>beliv.</b> MeldMeld																
	Multi	Point	Bacl	Pressure	e Te	est	(	Others								
	(Source o			<u>.</u>												

