

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST, OR GAS WELL

COPY 658
Form C-122
Revised 9-1-69
RECEIVED

Type Test ☒ Initial ☐ Annual ☐ Special					Test Date 12-10-75		DEC 15 1975		
Company Yates Petroleum Corp.				Connection Transwestern Pipeline Co.				O. C. C. ARTESIA, OFFICE	
Pool Kennedy Farms				Formation Morrow				Unit	
Completion Date 2-29-75		Total Depth 8830'		Plug Back TD 8656'		Elevation 3341 KB		Farm or Lease Name Tidwell "ED" Com	
Csg. Size 5 1/2"	Wt. 11.6	d 	Set At 8719	Perforations: From 8507 To 8526		Well No. 1			
Thq. Size 2-3/8	Wt. 4.6	d 1.995	Set At 8484	Perforations: From To		Unit Soc. Twp. Rge. P 22 17S 26E			
Type Well - Single - Bradenhead - G.C. or G.O. Multiple Dual gas-gas					Packer Set At 8485		County Eddy		
Producing Thru Tubing		Reservoir Temp. °F # 138		Mean Annual Temp. °F 62		Baro. Press. - P _g 13.2		State New Mexico	
L	H 8516	G _g 0.608	% CO ₂ 0.27	% N ₂ 0.38	% H ₂ S -	Prover	Meter Run 4"	Taps Flange	

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI							1966	60			24hrs.
1.	4 x 2.500			440	2	81	1679	65			1 hr.
2.				445	5	100	1553	73			1 hr.
3.				460	10	88	1290	75			1 hr.
4.				460	17	88	847	74			1 hr.
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	42.17	30.11	453.2	.9804	1.282	1.035	1650
2	42.17	47.86	458.2	.9636	1.282	1.031	2570
3	42.17	68.79	473.2	.9741	1.282	1.035	3750
4	42.17	89.69	473.2	.9741	1.202	1.035	4890
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1.	.67	541	1.503	.933	122	53.8	0.608	XXXXXX	672	360
2.	.68	560	1.556	.940				XXXXX		
3.	.70	548	1.522	.933						
4.	.70	548	1.522	.933						
5.										

P _c 2510.2 P _c ² 6301				$(1) \frac{P_c^2}{P_c^2 - P_w^2} = 1.465$		$(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.425$	
NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²	$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 6968$		
1		2167.2	4697	1604			
2		2037.2	4150	2151			
3		1762.2	3105	3196			
4		1414.2	2000	4301			
5							

Absolute Open Flow 6968 Mcfd @ 15.025		Angle of Slope θ		Slope, n 0.9278	
Remarks: BHP by Bennett Wireline - Tests witnessed by Transwestern Pipeline Co					
Approved By Commission:		Conducted By: Don Weaver		Calculated By: Eddie Mahfood	
				Checked By:	