

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65
1222
Jakes

RECEIVED

Type Test ☒ Initial ☐ Annual ☐ Special					Test Date 1-11-77		MAR 17 1977	
Company Yates Petroleum Corp.				Connection Transwestern Pipeline Co.				
Pool Cagle Creek Strawn Undesignated				Formation Strawn		Unit O.C.C. ARTESIA, OFFICE		
Completion Date 10-8-75		Total Depth 8640'		Plug Back TD 8080'		Elevation 3459'KB		Farm or Lease Name Patterson "EL"
Csq. Size 4 1/2"	Wt. 11.6#	d 4.000	Set At 8590'	Perforations: From 8002' To 8030'		Well No. 1		
Tbg. Size 2-3/8"	Wt. 4.7#	d 1.995	Set At 7920'	Perforations: From To		Unit Sec. Twp. Rye. M 31 - 17S-26E		
Type Well - Single - Bradenhead - G.C. or G.O. Multiple Single				Packer Set At 7920'		County Eddy		
Producing Thru tubing		Reservoir Temp. °F 134		Mean Annual Temp. °F 62		Baro. Press. - P _a 13.2		State New Mexico
L 8016	H 8016	Gg 0.6432	% CO ₂ 0.76	% N ₂ 0.41	% H ₂ S Nil	Prover	Meter Run 2.067"	Tags Flange

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI							2409	46			Months
1.	2 X 0.875			272	18	51	2046	51			1 hr.
2.				272	38	52	1864	52			1 hr.
3.				272	58	53	1702	53			1 hr.
4.				272	78	54	1950	54			1 hr.
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	3.729	71.649	285.2	1.009	1.265	1.0281	351
2	3.729	104.104	285.2	1.008	1.265	1.0279	509
3	3.729	128.614	285.2	1.007	1.265	1.0277	628
4	3.729	149.150	285.2	1.006	1.265	1.0275	727
5							

NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1	.4225	511	1.396	.9461	162.4 Mcf/bbl.	56.5 Deg.	.625	XXXXXXX	675 P.S.I.A.	366 R
2	.4225	512	1.399	.9465				0.6432	672 P.S.I.A.	368 R
3	.4225	512	1.402	.9468						
4	.4225	513	1.404	.9471						
5										

P _c 3039.2 P _c ² 9237				(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.7192$		(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.6976$	
NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²	AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1234$		
1			6682	2555			
2			5548	3689			
3			4621	4616			
4			3864	5373			
5							

Absolute Open Flow		1234	Mcf/d @ 15.025	Angle of Slope	44.7	Slope, n	0.97663
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Remarks: Static BHP by Bennett Wireline prior to pipeline connection. 4-point computed from DWT data after putting well on sales line; C-122D attached.

Approved By Commission:	Conducted By: Don Weaver	Calculated By: Eddie Mahfood	Checked By:
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