

RECEIVED

Type Test ☒ Initial ☐ Annual ☐ Special		Test Date 1-17-79		MAR 14 1979	
Company Yates Petroleum Corporation Transwestern Pipeline Co.				Connection O.C.C.	
Pool Eagle Creek Permo Penn				Formation Canyon-Cisco-Wolfcamp	
Completion Date 11-28-78		Total Depth 8180' KB		Plug Back TD 6896' KB	
				Elevation 3587' KB	
Csg. Size 4-1/2"	Wt. 10.5	d 4.000	Set At 7866' KB	Perforations: From 6392 To 6836'	
Tbg. Size 2-3/8"	Wt. 4.7	d 1.995	Set At 6367' KB	Perforations: From To	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple				Packer Set At 6367' KB	
Dual-Strawn blanked off - temp aband				Baro. Press. - P _g 13.2	
Producing Thru Tubing		Reservoir Temp. °F 123° 6615		Mean Annual Temp. °F 62	
L 6615		H 6615		G _g 678	
				% CO ₂ 2.46	
				% N ₂ 1.10	
				% H ₂ S Nil	
				Prover 2"	
				Meter Run Flange	
				Taps Flange	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow Days
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	
SI							1660	54		
1.	2.067 x 0.500			265	6	45	1505	55		
2.				265	13	45	1283	56.5		
3.				265	22	45	1006	57.5		
4.				265	33	45	583	59		
5.										

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	1.189	40.86	278.2	1.015	1.214	1.0322	62
2	1.189	60.14	278.2	1.015	1.214	1.0322	91
3	1.189	78.23	278.2	1.015	1.214	1.0322	119
4	1.189	95.82	278.2	1.015	1.214	1.0322	145
5							

NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1	0.410	505	1.340	.9385			.678	XXXXXX	678	377
2	0.410	505	1.340	.9385						
3	0.410	505	1.340	.9385						
4	0.410	505	1.340	.9385						
5										

NO.	P _t ²	P _w	R _w ²	P _c ² - R _w ²
1			3431	767
2			2471	1727
3			1501	2697
4			501	3697
5				

P_c 1994.2 P_c² 4198

(1) $\frac{P_c^2}{P_c^2 - R_w^2} = 1.1355$

(2) $\left[\frac{P_c^2}{P_c^2 - R_w^2} \right]^n = 1.0811$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - R_w^2} \right]^n = 157$

Absolute Open Flow 157 Mcfd @ 15.025

Angle of Slope 58.5 deg.

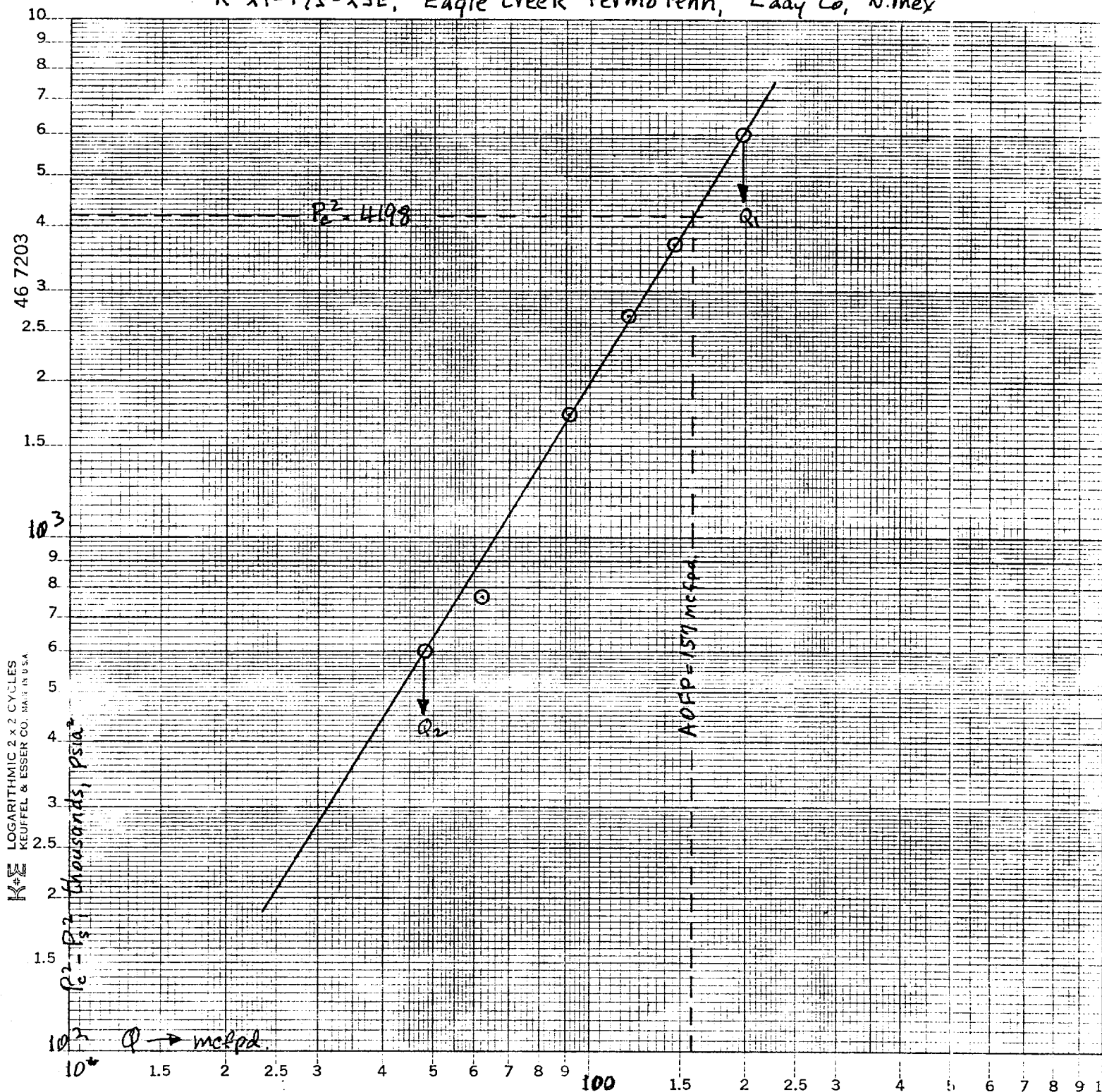
Slope, 0.6133

Remarks: Pressures by dead weight testers. Calculations worksheet C-122D attached.

Approved By Commission:	Conducted By: Hal Elless	Calculated By: Eddie Mahfood	Checked By:
-------------------------	-----------------------------	---------------------------------	-------------

YPC- Federal BZ Com No. 12

K-21-17s-2SE, Eagle Creek Permo Penn, Eddy Co, N.Mex



$$Q_1 = 197 \text{ mcfpd} \quad \log Q_1 = 2.2945$$

$$Q_2 = 48 \text{ mcfpd} \quad \log Q_2 = 1.6812$$

$$n = 0.6133$$

WORKSHEET FOR CALCULATION OF STATIC COLUMN WELLHEAD PRESSURE (P_w)

C-122D
Adapted 9-1-65

COMPANY

Yates Pats Corp

LEASE

Federal BZ Com

WELL NO. 12

DATE

1-17-79

LOCATION: Unit

K

Section

21

Township

17-S

Range

25-E

L

H

6615

L/H

1.000

G

0.678

%CO₂

2.46

%N₂

1.10

%H₂S

Nil

3/8" 6367(398) = 25340.7

248(16.00) = 3968.0

6615(4.4346) = 29308.7

D 2.1049

F_i .018568

GH 4485

P_{CT} 678

TABLE IX & X

T_{CT} 372

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

3/8" 6367(398) = 25340.7

248(16.00) = 3968.0

6615(4.4346) = 29308.7

D 2.1049

F_i .018568

GH 4485

P_{CT} 678

TABLE IX & X

T_{CT} 372

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

3/8" 6367(398) = 25340.7

248(16.00) = 3968.0

6615(4.4346) = 29308.7

D 2.1049

F_i .018568

GH 4485

P_{CT} 678

TABLE IX & X

T_{CT} 372

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

3/8" 6367(398) = 25340.7

248(16.00) = 3968.0

6615(4.4346) = 29308.7

D 2.1049

F_i .018568

GH 4485

P_{CT} 678

TABLE IX & X

T_{CT} 372

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

3/8" 6367(398) = 25340.7

248(16.00) = 3968.0

6615(4.4346) = 29308.7

D 2.1049

F_i .018568

GH 4485

P_{CT} 678

TABLE IX & X

T_{CT} 372

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

3/8" 6367(398) = 25340.7

248(16.00) = 3968.0

6615(4.4346) = 29308.7

D 2.1049

F_i .018568

GH 4485

P_{CT} 678

TABLE IX & X

T_{CT} 372

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

3/8" 6367(398) = 25340.7

248(16.00) = 3968.0

6615(4.4346) = 29308.7

D 2.1049

F_i .018568

GH 4485

P_{CT} 678

TABLE IX & X

T_{CT} 372

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

3/8" 6367(398) = 25340.7

248(16.00) = 3968.0

6615(4.4346) = 29308.7

D 2.1049

F_i .018568

GH 4485

P_{CT} 678

TABLE IX & X

T_{CT} 372

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X

TABLE IX & X