

Federal CR Com # SW SW Sec 25-17S-24E Eddy Co

Eagle Creek Strawn;

Pf. 7404-7408 0.26 ft 0.78 S_g β_g = .006568 μ_g = .019 cp.

BHP = 2127 psi BHT = 129°F P_c = 675 T_c = 366 Z = .826 φ_{ay} = 65%

$$K_{gh} = \frac{q \mu T_2 h_{f_w}}{703 \Delta P P_{avg}} = \frac{25000 (.006568) (.019) (589) (.826) (5.23)}{5.615 (.703) (2140^2 - 93^2) / 110.5} = \frac{2011.23}{4094.2} = 0.49 \text{ mD ft} \quad h = 4 \text{ ft} \quad k = 0.12 \text{ md.}$$

Most Probable Recovery Factor (After Craig & Buckley Statistics):

$$= 0.11403 + .2719 \log k_e + .25569 S_w - .1355 \log \mu - 1.538 \phi - .00035 h$$

$$= 0.11403 - 0.25037 + 0.19914 + 0.23323 - 0.09997 - 0.00140$$

$$= 0.29496$$

Then most probable reserves =

$$43560 \text{ ft}^3/\text{ac} \times 320 \text{ ac} \times 0.195 \text{ RF} \left[\frac{0.26 \text{ ft} \times 0.78 S_g}{0.006568 \beta_g} \right] = 83930 \text{ mcf.}$$

Eagle Creek Permian-Penn:

Pf 7248-7254, 0.68 ft 0.76 S_g β_g = .006559 μ_g = .019 cp φ = 11.3%

BHP = 2115 psi BHT = 127°F P_c = 675 T_c = 366 Z = .823 h = 6 ft

$$K_{gh} = \frac{q \mu T_2 h_{f_w}}{703 \Delta P P_{avg}} = \frac{75000 (.006559) (.019) (589) (.823) (5.23)}{5.615 (.703) (2122^2 - 93^2) / 110.5} = \frac{5782.56}{4070} = 1.42 \text{ mD ft} \quad k_g = 2.4 \text{ md.}$$

Most Probable Recovery Factor (After Craig & Buckley Statistics)

$$= 0.11403 - 0.16609 + 0.19432 + 0.23323 - 0.17627 - 0.00210 = 0.19652$$

Pf 6214-6221, 0.477 ft 0.91 S_g β_g = .006372 μ_g = .019 cp φ = 3.67%

BHP = 2032 psi BHT = 112°F P_c = 673 T_c = 383 Z = .781 h = 13 ft

$$K_{gh} = \frac{q \mu T_2 h_{f_w}}{703 \Delta P P_{avg}} = \frac{64000 (.006372) (.019) (578) (.781) (5.23)}{5.615 (.703) (2045^2 - 149^2) / 109.7} = \frac{46386.7}{3792} = 12.23 \text{ mD ft} \quad k = 0.94 \text{ md.}$$

Most Probable Recovery Factor (After Craig & Buckley Statistics):

$$= 0.11403 - .00731 + .23212 + .23323 - 0.05644 - .00455 = 0.51164$$

Then most probable reserves =

$$43560 \text{ ft}^3/\text{ac} \times 320 \text{ ac} \times \left[\frac{.1965 (.68 \text{ ft}) (.76 S_g)}{.006559 \beta_g} + \frac{.5116 (.477 \text{ ft}) (.91 S_g)}{.006372} \right]$$

$$= 13939200 \text{ ft}^3 (15.483 + 34.818) = 701150 \text{ mcf.}$$

We propose to commingle the Eagle Creek Strawn and the Eagle Creek Permian Penn, and to apportion production as follows:

Gas: Strawn — 83930 mcf = 10.69%

Permian Penn — $\frac{701150 \text{ mcf}}{785080} = 89.31\%$

Condensate: Strawn — $\frac{83930}{4226 \text{ mcf}} = 199 \text{ bbls} = 10.76\%$

Permian Penn — $\frac{701150}{4256 \text{ mcf}} = 1650 \text{ bbls} = 89.24\%$

Oil: 1249