

Federal GR Conty SW SW Sec 25-17S-24E Eddy Co
Eagle Creek Strawn;

Pf. 7404-7408 0.26 ft 0.78 Sg. $\beta_g = .006568$ $\mu_g = .019$ cp.

BHP = 2127 psi BHT = 129°F $P_c = 675$ $T_c = 366$ $Z = .826$ $\phi_{avg} = 6.5\%$

$K_{gh} = \frac{q \mu T_2 \ln \frac{r_e}{r_w}}{.703 \phi P_{avg}} = \frac{25000 (.006568) (.019) (539) (.826) (5.23)}{.703 (2140^2 - 43^2) / 1116.5} = \frac{3011.03}{4094.2} = 0.49 \text{ md ft}$ $h = 4 \text{ ft}$
 $k = 0.12 \text{ md}$

Most Probable Recovery Factor (After Craig & Buckley Statistics):

$= 0.11403 + .2719 \log k_e + .25569 S_w - .1355 \log \mu - 1.538 \phi - .00035 h$

$= 0.11403 - 0.25037 + 0.19944 + 0.23323 - 0.09997 - 0.00140$

$= 0.19496$

Then most probable reserves =

$43560 \text{ ft}^2/\text{ac} \times 320 \text{ ac} \times 0.19496 \left[\frac{0.26 \text{ ft} \times 0.78 S_g}{0.006568 \beta_g} \right] = 83930 \text{ mcf.}$

Eagle Creek Permian-Penn:

Pf 7248-7254, 0.68 ft 0.76 Sg $\beta_g = .006559$ $\mu_g = .019$ cp $\phi = 11.3\%$

BHP = 2115 psi BHT = 127°F $P_c = 675$ $T_c = 366$ $Z = .823$ $h = 6 \text{ ft}$

$K_{gh} = \frac{q \mu T_2 \ln \frac{r_e}{r_w}}{.703 \phi P_{avg}} = \frac{75000 (.006559) (.019) (539) (.823) (5.23)}{.703 (2128^2 - 43^2) / 1110.5} = \frac{5922.56}{4070} = 1.47 \text{ md ft}$
 $k_g = 2.45 \text{ md}$

Most Probable Recovery Factor (After Craig & Buckley Statistics)

$= 0.11403 - 0.16689 + 0.19432 + 0.23323 - 0.17687 - 0.00210 = 0.19652$

Pf 6214-6221, 0.477 ft 0.91 Sg $\beta_g = .006372$ $\mu_g = .019$ cp $\phi = 3.67\%$

BHP = 2032 psi BHT = 118°F $P_c = 673$ $T_c = 383$ $Z = .781$ $h = 13 \text{ ft}$

$K_{gh} = \frac{q \mu T_2 \ln \frac{r_e}{r_w}}{.703 \phi P_{avg}} = \frac{64000 (.006372) (.019) (578) (.781) (5.23)}{.703 (2045^2 - 147^2) / 1097} = \frac{41386.7}{3792} = 12.23 \text{ md ft}$
 $k = 0.94 \text{ md}$

Most Probable Recovery Factor (After Craig & Buckley Statistics):

$= 0.11403 - .00731 + .23268 + .23323 - 0.05644 - .00455 = 0.51164$

Then most probable reserves =

$43560 \text{ ft}^2/\text{ac} \times 320 \text{ ac} \times \left[.1965 (0.68 \text{ ft}) (.76 S_g) + .5116 (.477 \text{ ft}) (.91 S_g) \right]$
 $= 13939200 \text{ ft}^3 (15.483 + 34.818) = 701150 \text{ mcf.}$

We propose to commingle the Eagle Creek Strawn and the Eagle Creek Permian Penn, and to apportion production as follows:

Gas: Strawn — 83930 mcf = 10.69%

Permian Penn — $\frac{701150 \text{ mcf}}{785080} = 89.31\%$

Condensate: Strawn — $83930 / 4226 \text{ bbl/mcf} = 199 \text{ bbls} = 10.76\%$

Permian Penn — $701150 / 4256 \text{ mcf} = 1650 \text{ bbls} = 89.24\%$
 1849