

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT, AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

RECEIVED

Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 8/25/78		SEP - 6 1978	
Company Beard Oil Company ✓				Connection Air		O. C. C.	
Pool Undersigned <i>Atoka</i>				Formation Atoka		Unit JESIA, OFFICE	
Completion Date 8/4/78		Total Depth 7220		Plug Back TD 7210 7195		Elevation 3822 GL	
Casing Size 4 1/2		Wt. 10.5		Set At 7220		Perforations: From 7100 To 7116	
Tubing Size 2 3/8		Wt. J 55		Set At 7026		Perforations: From To	
Type Well - Single - Broadhead - G.G. or G.O. Multiple				Packer Set At 7026		County Eddy	
Producing Time Tbg.		Reservoir Temp. °F 146 @ 7108		Mean Annual Temp. °F 60		Baro. Press. - P _a 13.2	
L 7026		H 7026		G _q .617		% CO ₂ .53	
				% N ₂ 1.34		% H ₂ S	
				Prover		Meter Run 3"	
						Taps Flg.	

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI							1712				72 Hr.
1.	3 X 1.625			500	2.0	64	1530				1 Hr.
2.	3 X 1.625			500	4.0	77	1233				1 Hr.
3.	3 X 1.625			500	8.0	85	823				1 Hr.
4.	3 X 1.625			500	13.0	89	620				1 Hr.
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	13.24	32.04	513.2	.9962	1.273	1.047	563
2	13.24	45.31	513.2	.9810	1.273	1.044	734
3	13.24	64.07	513.2	.9763	1.273	1.041	1093
4	13.24	81.58	513.2	.9732	1.273	1.040	1393
5							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	Mcf/bbl.
1	.76	524	1.44	.913	Dry	
2	.76	537	1.47	.913	A.P.I. Gravity of Liquid Hydrocarbons	
3	.76	545	1.49	.922	Specific Gravity Separator Gas	.617
4	.76	542	1.50	.924	Specific Gravity Flowing Fluid	XXXXXX
5					Critical Pressure	671 P.S.I.A.
					Critical Temperature	365 °R

NO.	P _r	P _w	P _w ²	P _r ² - P _w ²	(1) $\frac{P_r^2}{P_r^2 - P_w^2} = 1.177$	(2) $\left[\frac{P_r^2}{P_r^2 - P_w^2} \right]^n = 1.173$
1	1725.2	1545.4	2388.4	587.9		
2	1725.2	1351.3	1566.9	1409.4		
3	1725.2	853.3	727.3	2248.5		
4	1725.2	669.5	448.2	2523.1		
5						

AGP = Q $\left[\frac{P_r^2}{P_r^2 - P_w^2} \right]^n = 1.635$

*Partial
AD-2 & back
9-22-78
ST*

Absolute Open Flow	1,635 Mcfd @ 15.025	Angle of Slope	45.5°	Slope, n	.980
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Remarks:

Approved by Commission	Conducted By: <i>John Davis</i>	Calculated By: <i>John Davis</i>	Checked By:
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