

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

JAN 11 1980

Type Test ☒ Initial ☐ Annual ☐ Special		Test Date 12-21-79		RECEIVED DEC 29 1979	
Company MESA PETROLEUM Co.		Location ARTESIA, OFFICE			
Pool Diamond mound Atoka		Formation Atoka		Unit MESA-55D	
Completion Date 11-29-79		Total Depth 8794'		Plug Back TD 8666' 8667	
Elevation 3574. GL		Land or Lease Name COOK FED. COM.		Well No. # 1	
Csg. Size 4 1/2	Wt. 11.6/10.5	Set At 8793	Perforations: From 8570 To 8580	Unit Soc. Twp. Rge. H 10 16 27	
Tub. Size 2 3/8	Wt. 4.7	Set At 8492	Perforations: From To		
Type Well - Single - Prodenhead - G.G. or G.O. Multiple			Packer Set At 8465'		County EDDY
Producing Thru TBG...		Reservoir Temp. *F 125° PERFS.	Mean Annual Temp. *F 60	Baro. Press. - P _a 13.2	State NEW MEXICO
L 8492	H 8492	Gg .850	% CO ₂ 14.002	% N ₂ .805	% H ₂ S Prover Meter Run 4 Taps FLG.

FLOW DATA					TUBING DATA		CASING DATA		Duration of Flow		
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. *F	Press. p.s.i.g.	Temp. *F		Press. p.s.i.g.	Temp. *F
51							2320				72 HR.
1.	4 X 1.000			355	2.0	80	1820	70			1 HR.
2.	4 X 1.000			363	3.0	89	1485	70			1 HR.
3.	4 X 1.000			353	3.5	95	1290	68			1 HR.
4.	4 X 1.000			315	5.0	87	318	68			45 MIN.
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor Fpv	Rate of Flow Q, Mcfd
1	4.753	27.14	368.2	.9813	1.085	1.046	144
2	4.753	33.59	376.2	.9732	1.085	1.044	176
3	4.753	35.80	366.2	.9680	1.085	1.041	186
4	4.753	40.51	328.2	.9750	1.085	1.038	171
5							

NO.	P ₁	Temp. *R	T _r	Z	Gas Liquid Hydrocarbon Ratio	Mcf/bbl.
1.	.51	540	1.29	.914	dry	
2.	.52	549	1.32	.917	A.P.I. Gravity of Liquid Hydrocarbons	Deg.
3.	.51	555	1.33	.922	Specific Gravity Separator Gas .850	X X X X X X X X
4.	.45	547	1.31	.928	Specific Gravity Flowing Fluid X X X X X	
5.					Critical Pressure 725 P.S.I.A.	P.S.I.A.
					Critical Temperature 417 R	R

$P_c = 2333.2$ $P_c^2 = 5443.8$

NO.	P ₁ ²	P _w ²	P _c ² - P _w ²
1	1833.3	3361.1	2082.7
2	1498.5	2245.4	3198.4
3	1303.5	1699.2	3744.6
4	333.6	111.3	5332.5
5			

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.702$

(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.305$

ADP = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = .230$

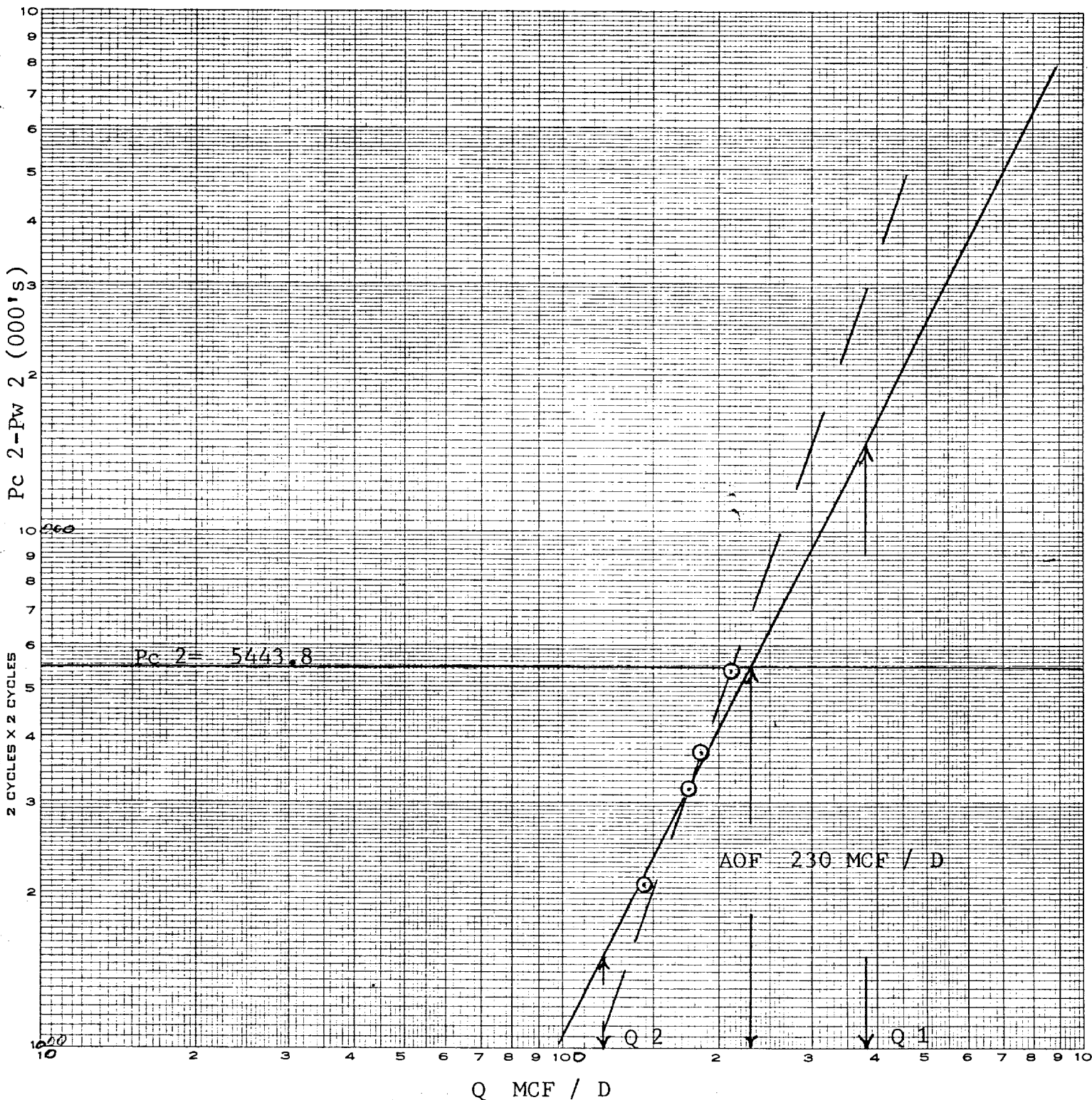
Absolute Open Flow 230 Mcfd @ 15.025 Angle of Slope 63.5 Slope, n .500

Remarks:

Approved By Commission:	Conducted By: JOHN DAVIS	Calculated By: LARRY DAVIS	Checked By:
-------------------------	-----------------------------	-------------------------------	-------------

COMPANY : MESA PETROLEUM
 LEASE : COOK FED. M.
 WELL NO. : # 1
 UNIT : 10/16/27
 COUNTY : EDDY
 STATE : NEW MEXICO
 DATE : DECEMBER 21, 1979

DIEZELER CORPORATION
 MADE IN U.S.A.
 LOGARITHMIC
 2 CYCLES X 2 CYCLES



Q 1 = 380; LOG OF Q 1 = 2.579784
 Q 2 = 120; LOG OF Q 2 = 2.079181
 N = .500

NEW-TEX LAB

P. O. BOX 1181
HOBBS, N.M. 88240

CERTIFICATE OF ANALYSIS

No. 2005
Run No. _____
Date of Run 12-26-79
Date Secured 12-21-79

A Sample of Mesa Petroleum Co. Cook Federal Comm #1
Secured from Davis Services
At Box 2033 Secured by _____
Hobbs, NM 88240 Time _____ Date _____
Sampling conditions _____ Press _____
Temp. _____

FRACTIONAL ANALYSIS

Percentage Composition

	MOL %	LIQ. %	G.P.M.
Carbon Dioxide	14.002		
Air			
Nitrogen	.805		
Oxygen			
Hydrogen sulfide			
Hydrogen			
Methane	67.048		
Ethane	9.248	2.466	
Propane	5.337	1.470	
Butanes			
Iso-Butane	.784	.256	
N-Butane	1.440	.453	
Pentanes			
Iso-Pentane	.439	.160	
N-Pentane	.418	.151	
Hexanes	.214	.088	
Heptanes	.265	.113	
Octanes			
TOTAL	100.000	5.157	

Calc. Sp. Gr. 0.8499
Calc. A.P.I. _____
Calc. Vapor Press. _____ PSIA
Sp. Gr. _____
Mol. Wt. 24.65

LIQUID CONTENT (GAL./MCF)

Propane Calc. G.P.M. 1.470
Butanes Calc. G.P.M. .709
Pentanes Plus. G.P.M. .512
Ethane Calc. G.P.M. 2.466
RVP Gasoline G.P.M. _____
B.T.U./Cu. Ft. @ 14.696 P.S.I.A.
Dry Basis 1105
Wet Basis 1086
Sulfur Analysis by Titration
Gr./100 Cu. Ft. _____
Hydrogen Sulfide _____
Mercaptans _____
Sulfides _____
Residual Sulfur _____
Total Sulfur _____

Run by Deane Simpson Checked by _____ Approved by Deane Simpson

Additional Data and Remarks

WORKSHEET FOR CALCULATION OF STATIC COLUMN WELLHEAD PRESSURE (P_w)

Form C-122D
Adopted 9-1-65

COMPANY MESA PETROLEUM LEASE COOK FED. COM. WELL NO. #1 DATE 12-21-79

LOCATION: Unit Section 10 Township 16 Range 27

L 8492 H 8492 L/H 1.000 G .850 % CO₂ 14.002 % N₂ .805 % H₂S 0

d 1.995 F_r .018231 GH 7218. P_{CT} 725 T_{CT} 417

LINE	1 st			2 nd			3 rd			4 th		
	1 st	2 nd	1 st	2 nd	1 st	2 nd	1 st	2 nd	1 st	2 nd	1 st	2 nd
1 Q _m	.144	.144	.176	.176	.186	.186	.211	.211	.211	.211		
2 T _w (W.H. °R)	534	534	534	534	534	534	534	534	534	534		
3 T _s (B.H. °R)	585	585	585	585	585	585	585	585	585	585		
4 T = ($\frac{1}{2}T_w + T_s$)	559.5	559.5	559.5	559.5	559.5	559.5	559.5	559.5	559.5	559.5		
5 Z (Est.)	.686	.669	.725	.690	.755	.717	.932	.922	.922	.922		
6 TZ	383.8	374.3	405.6	386.1	422.4	401.2	521.5	515.9	515.9	515.9		
7 GH/TZ	18.806	19.284	17.794	18.697	17.087	17.993	13.842	13.992	13.992	13.992		
8 e ^s (Table XIV)	2.024	2.061	1.949	2.016	1.898	1.963	1.680	1.690	1.690	1.690		
9 1-e ^s (Table XIV)	.506	.515	.487	.504	.473	.491	.405	.408	.408	.408		
10 P _t	1833.2	1833.2	1498.2	1498.2	1303.2	1303.2	331.2	331.2	331.2	331.2		
11 P _t ² /1000	3360.6	3360.6	2244.6	2244.6	1698.3	1698.3	109.7	109.7	109.7	109.7		
12 F _r (Table XV)	.018231	.018231	.018231	.018231	.018231	.018231	.018231	.018231	.018231	.018231		
13 F _c = F _r TZ	6.9974	6.8240	7.3952	7.0382	7.7012	7.3136	9.5066	9.4046	9.4046	9.4046		
14 F _c Q _m	1.008	.983	1.302	1.239	1.432	1.360	2.006	1.984	1.984	1.984		
15 L/H (F _c Q _m) ²	1.015	.966	1.694	1.534	2.052	1.850	4.024	3.938	3.938	3.938		
16 F _w = L/H (F _c Q _m) ² (1-e ^s)	.514	.497	.825	.773	.971	.908	1.629	1.608	1.608	1.608		
17 P _w ² = P _t ² + F _w	3361.1	3361.1	2245.4	2245.4	1699.2	1699.2	111.3	111.3	111.3	111.3		
18 P _s ² = e ^s P _w ²	6803.9	6926.9	4376.2	4526.7	3225.2	3336.5	187.1	188.1	188.1	188.1		
19 P _s	2608.4	2631.9	2091.9	2127.6	1795.9	1826.6	432.5	433.7	433.7	433.7		
20 P = ($\frac{P_t + P_s}{2}$)	2220.8	2232.6	1795.1	1812.9	1549.5	1564.9	381.9	382.4	382.4	382.4		
21 P _r = (P/P _{cr})	3.06	3.08	2.48	2.50	2.14	2.16	.53	.53	.53	.53		
22 T _r = (T/T _{cr})	1.34	1.34	1.34	1.34	1.34	1.34	1.34	1.34	1.34	1.34		
23 Z (Table XI)	.669	.668	.690	.688	.717	.715	.922	.922	.922	.922		