

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

RECEIVED

Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 7-23-80		AUG 4 1980	
Company AMOCO PRODUCTION COMPANY				Connection LLANO		O. C. D. ARTESIA, OFFICE	
Pool LOGAN DRAW <i>Morrow</i>				Formation MORROW		Unit	
Completion Date 01-07-80		Total Depth 9910.		Plug Back TD 9395.		Elevation 3482.	
Form or Lease Name FEDERAL Z COM		Well No. 1		Perforations: From 9330. To 9338.		Unit Sec. Twp. Rge. H 33 17S 27E	
Csg. Size 5.500	Wt. 15.5	d 4.950	Set At 9910.	Perforations: From 0. To 0.		County EDDY	
Tbg. Size 2.375	Wt. 4.7	d 1.995	Set At 9272.	Perforations: From 0. To 0.		State NEW MEXICO	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple SINGLE				Packer Set At 9200.		County EDDY	
Producing Thru TUBING		Reservoir Temp. °F 153. @ 9334.		Mean Annual Temp. °F 60.0		Baro. Press. - P _a 13.2	
L 9334.	H 9334.	Gg 0.635	% CO ₂ 0.74	% N ₂ 0.41	% H ₂ S 0.	Prover 0.	Meter Run 3.0 FLANGE

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							1062.	82.			46.0
1.	3.00 X 1.250			490.	3.0	59.	904.	83.	0.	0.	0.7
2.	3.00 X 1.250			490.	10.0	53.	775.	92.	0.	0.	1.0
3.	3.00 X 1.250			490.	17.0	52.	672.	91.	0.	0.	1.0
4.	3.00 X 1.250			490.	21.0	52.	613.	90.	0.	0.	0.5
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	7.59	38.85	503.2	1.0010	1.2547	1.0492	389.
2	7.59	70.94	503.2	1.0068	1.2547	1.0511	715.
3	7.59	92.49	503.2	1.0078	1.2547	1.0516	934.
4	7.59	102.80	503.2	1.0078	1.2547	1.0516	1038.
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1.	0.75	519.	1.41	0.908	0.	0.	0.635	X X X X X X X X	673.	367.
2.	0.75	513.	1.40	0.905						
3.	0.75	512.	1.39	0.904						
4.	0.75	512.	1.39	0.904						
5.										

P _r 1066.9 P _c ² 1138.				(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.5771$		(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.5771$	
NO	P _r ²	P _w	P _w ²	P _c ² - P _w ²			
1	841.	913.	833.	306.			
2	621.	790.	624.	515.			
3	469.	697.	486.	652.			
4	392.	645.	417.	722.			
5							

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1636.$			
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Absolute Open Flow	1636	Mcfd @ 15.025	Angle of Slope @	45.0	Slope, n	1.000
Remarks:						

Approved By Commission:	Conducted By: John West Engineering	Calculated By: Chris Van Dooren	Checked By: L. W. Sheppard
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3 - NMOC D - A 1 - Hou 1 - Susp 1 - DLB 1 - LWS